

PART A -

①

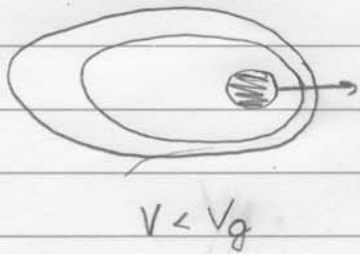
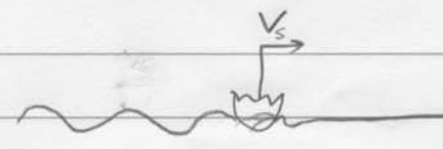
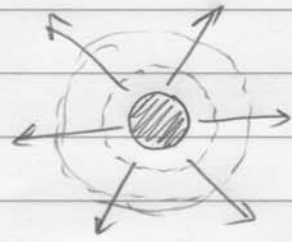
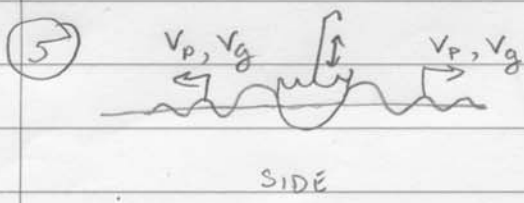
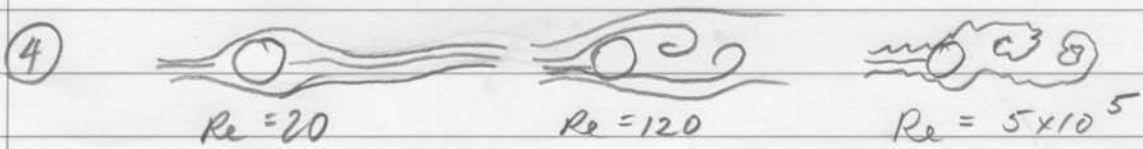
X	0	0	0	0	X
0	X	0	0	0	0
0	0	X	X	0	0
0	0	X	X	0	0
0	0	0	0	0	0
X	0	0	0	0	X

③

-X	0	0	0	0	-X
0	-X	0	0	0	-X
0	0	+X	+X	+X	0
0	0	+X	-X	0	0
0	0	+X	0	-X	0
-X	-X	0	0	0	-X

②  $\underline{\omega_s} = 16.75 \text{ rad/s}$  ,  $(f_s = 2.67 \text{ Hz})$

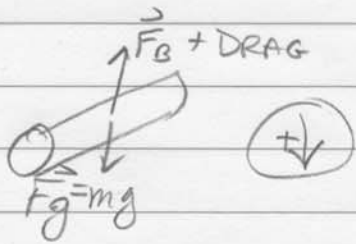
$\omega_s = \omega_n = \sqrt{\frac{k}{M+Ma}}$  lock in -



↑  
there is always some form of bow wave...

PART B-

(1) a) Terminal Velocity



$$F_{\text{DRAG}} = \frac{1}{2} \rho U^2 C_D A$$

$$F_B = \rho g V$$

$$F_g = 1.5 \rho_w g V$$

$$A = dL$$

$$V = \frac{\pi d^2}{4} L$$

@ Terminal Vel  $\Sigma F = ma = 0$

$$\Sigma F = \vec{F}_g - \vec{F}_B - \vec{F}_D = 0$$

$$\vec{F}_D = \vec{F}_g - \vec{F}_B = \frac{1}{2} \rho_w g V = 157 \text{ N}$$

$$U^2 \left( \frac{1}{2} \rho C_D d \cdot V \right) = \frac{1}{2} \rho_w g \frac{\pi d^2}{4} V$$

$$U = \sqrt{\frac{\pi g d}{4 C_D}} = \sqrt{1.57 / C_D}$$

laminar  $C_D = 1.2$   $U = 1.14 \text{ m/s}$   $Re = 228,000$

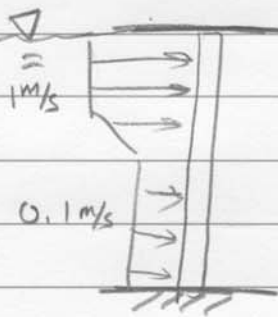
turb  $C_D = 0.6$   $U = 1.62 \text{ m/s}$   $Re = 324,000$

wow! v. close could be either so it ultimately depends on cylinder roughness - either answer gets credit-

b) @  $U = 1.14 \text{ m/s}$   $f = 1.14 \text{ Hz}$  ;  $f = \frac{U}{d} = \frac{0.2}{0.2} U$   
 $U = 1.62 \text{ m/s}$   $f = 1.62 \text{ Hz}$  ;

PART B

3



assume  $S = 0.2 = \frac{fd}{u}$

Top  
 $f = \frac{0.2 \cdot 1.0}{0.5}$

bottom  
 $f_{bot} = 0.1 * f_{top}$

$f_{top} = 0.4 \text{ Hz}$

$f_{bot} = 0.04 \text{ Hz}$

b) frequency of drag is 2. freq of vortex shedding

freq. of lift is = freq of vortex shedding

therefore it directly correlates w/ flow velocity.

c) the structure will tend to vibrate more at top exciting forced motion

@ bottom. In both cases frequency is low so it's not going to be too violent.

Shear will complicate shedding & make flow more 3 dimensional

d) Flexible cylinder

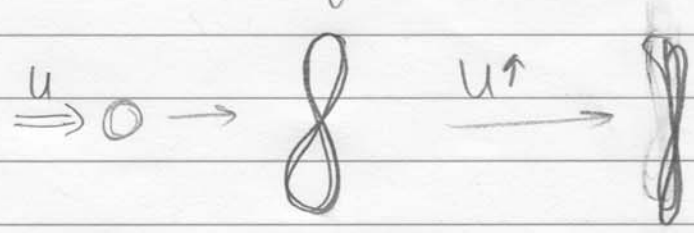


figure "8" motion

high vel, tension ↑ and inline vibs ↓