

16.31 Fall 2005, Homework 4

1) u is input for both systems $\Rightarrow \beta = \begin{bmatrix} b_1 \\ b_2 \end{bmatrix}$

y is sum of subsystem outputs $\Rightarrow C = \begin{bmatrix} c_1 & c_2 \end{bmatrix}$
 $D = [D_1 + D_2]$
final system

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} A_1 & 0 \\ 0 & A_2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} b_1 \\ b_2 \end{bmatrix} u$$

$$y = [c_1 \ c_2] \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + [D_1 + D_2] u_2$$

$$y = [D_2 C_1 \ C_2] \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + D_2 D_1 u_1$$

check dimensions match ✓

2) from figure 2.17:

$$u = u_1, \quad u_2 = u_1, \quad y = y_2$$

$$u_2 = y \Rightarrow u_2 = C_2 x_2 + D_2 u_1$$

$$\therefore \dot{x}_2 = A_2 x_2 + B_2 (C_2 x_2 + D_2 u_1)$$

Substitute and stack into matrices

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} A_1 & 0 \\ B_2 C_1 & A_2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} B_1 \\ B_2 D_1 \end{bmatrix} u$$

$$y = [0 \ C_2] \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + D_2 u$$

note that if original systems are controllable and observable, so is the series interconnection

3) From Figure 2.18:

$$y = y_1 \Rightarrow u_1 = u - y_2, \quad u_2 = y_1$$

The trick to this problem is to solve for y first, to get the effect of the "algebraic feedback loop" out of the way =

$$y = C_1 x_1 + D_1 u_1$$

$$= C_1 x_1 + D_1 (u - y_2)$$

$$= C_1 x_1 + D_1 u - D_1 (C_2 x_2 + D_2 y)$$

This is what happens when you have algebraic feedback! Solve for y :

$$(I + D_1 D_2) y = C_1 x_1 + D_1 u - D_1 C_2 x_2$$

$$y = (I + D_1 D_2)^{-1} [C_1 x_1 + D_1 u - D_1 C_2 x_2]$$

$$\triangleq \Delta^1 C_1 x_1 + \Delta^1 D_1 u + \Delta^1 D_1 C_2 x_2$$

Now that we have y , we can proceed.

$$\dot{x}_1 = A_1 x_1 + B_1 u - B_1 (\Delta^1 C_2 x_2 + \Delta^1 D_1 y)$$

$$\dot{x}_2 = A_2 x_2 + B_2 y$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} A_1 - B_1 D_2 \Delta^1 C_2 & -B_1 C_2 + B_1 D_2 \Delta^1 D_1 \\ A_2 & B_2 \Delta^1 D_1 C_2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$+ \begin{bmatrix} B_1 - B_1 D_2 \Delta^1 D_1 \\ B_2 \Delta^1 D_1 \end{bmatrix} u$$

$$y = [\Delta^1 C_1 \ -\Delta^1 D_1 C_2] \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \Delta^1 D_1 u$$

4 Substituting into given eqns:

$$\frac{d}{dt}(x^* + \Delta x) = f(x^* + \Delta x, u^* + \Delta u)$$

using first-order Taylor series:

$$\dot{x}^* + \Delta \dot{x} = f(x^*, u^*) + \left. \frac{\partial f}{\partial x} \right|_{\substack{x=x^* \\ u=u^*}} \Delta x + \left. \frac{\partial f}{\partial u} \right|_{\substack{x=x^* \\ u=u^*}} \Delta u$$

since the nominal traj satisfies:

$$\dot{x}^* = f(x^*, u^*) + \dots$$

we have

$$\Delta \dot{x} = \left. \frac{\partial f}{\partial x} \right|_{\substack{x=x^* \\ u=u^*}} \Delta x + \left. \frac{\partial f}{\partial u} \right|_{\substack{x=x^* \\ u=u^*}} \Delta u$$

and, by similar arguments

$$\Delta y = \left. \frac{\partial h}{\partial x} \right|_{\substack{x=x^* \\ u=u^*}} \Delta x + \left. \frac{\partial h}{\partial u} \right|_{\substack{x=x^* \\ u=u^*}} \Delta u$$

note that the derivative of a vector w/ respect to a scalar is

$$\frac{\partial a}{\partial x} = \begin{bmatrix} \frac{\partial f_1}{\partial x} \\ \frac{\partial f_2}{\partial x} \\ \vdots \end{bmatrix} \text{ by definition...}$$

to maintain consistency of the vector-matrix operations, we define the derivative of a scalar w/ respect to a vector as a row vector:

$$\frac{\partial a}{\partial x} = \left[\frac{\partial a}{\partial x_1}, \frac{\partial a}{\partial x_2}, \dots \right]$$

Combining these, $\frac{\partial a}{\partial x}$ is a matrix, in this case the Jacobian

4 (b)

Computed trajectory - see attached. use rk45 or Simulink

Linearized system

$$\Delta \dot{x}_1 = \Delta x_2$$

$$\Delta \dot{x}_2 = -4\Delta x_1 - 3(x_2^*)^2 \Delta x_2 \\ + x_2^* \Delta u + u^* \Delta \dot{x}_2$$

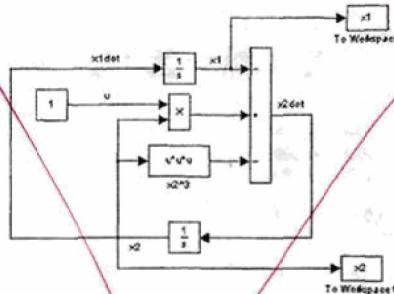
$$\Delta y = \Delta x_1$$

or

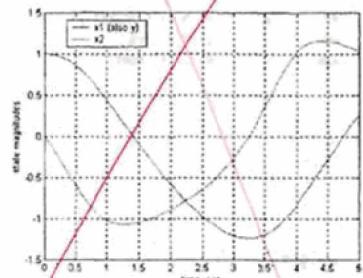
$$\begin{bmatrix} \Delta x_1 \\ \Delta x_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -1 & -3x_2^{*2} + 1u^* \end{bmatrix} \begin{bmatrix} \Delta x_1 \\ \Delta x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ x_2^* \end{bmatrix} \Delta u$$

Some of the coefficients of this system are time-varying. Plots of these coefficients are attached.

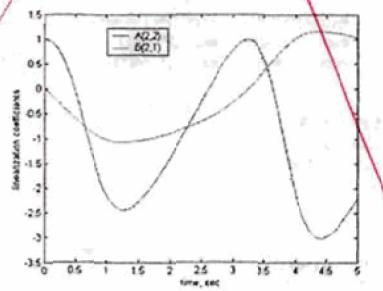
Problem 2, Part (b)



Here's the Simulink block diagram I used to compute the response – check it!



Here's the trajectories of x1 (which is y) and x2.



Here's the time histories of the coefficients of the A and B matrices
(the ones that aren't constant with time)

Problem 5. Parts (b) and (c)

```
>> t=1;
>> eAt=[exp(-t) exp(-t)*sin(t) exp(-t)*(1-cos(t))
0 exp(-t)*cos(t) -exp(-t)*sin(t)
0 exp(-t)*sin(t) exp(-t)*cos(t)]
```

```
eAt =
0.3679 0.3096 0.1691
0 0.1988 -0.3096
0 0.3096 0.1988
```

```
>> A=[-1 1 0;0 -1 -1;0 1 -1];
>> expm(A*t)
```

```
ans =
0.3679 0.3096 -0.1691
0 0.1988 -0.3096
0 0.3096 0.1988
```

```
>> t=2;
>> eAt=[exp(-t) exp(-t)*sin(t) exp(-t)*(1-cos(t))
0 exp(-t)*cos(t) -exp(-t)*sin(t)
0 exp(-t)*sin(t) exp(-t)*cos(t)]
```

```
eAt =
0.1353 0.1231 0.1917
0 -0.0563 -0.1231
0 0.1231 -0.0563
```

```
>> expm(A*t)
```

```
ans =
0.1353 0.1231 -0.1917
0 -0.0563 -0.1231
0 0.1231 -0.0563
```

```
>> t=4;
>> eAt=[exp(-t) exp(-t)*sin(t) exp(-t)*(1-cos(t))
0 exp(-t)*cos(t) -exp(-t)*sin(t)
0 exp(-t)*sin(t) exp(-t)*cos(t)]
```

```
eAt =
0.0183 -0.0139 0.0303
0 -0.0120 0.0139
0 -0.0139 -0.0120
```

```
>> expm(A*t)
```

```
ans =
0.0183 -0.0139 -0.0303
0 -0.0120 0.0139
0 -0.0139 -0.0120
```

5 (a) $\ddot{r} = r\dot{\theta} - \frac{k}{r^2} + u_1$ or $\ddot{r} = r\dot{\theta}^2 - \frac{k}{r^2} + u_1$
 $\ddot{\theta} = -2\frac{\dot{r}}{r}\dot{\theta} + \frac{1}{r}u_2$

(b) $\dot{r}_1 = r_2$
 $\dot{r}_2 = r_1\dot{\theta}_2 - \frac{k}{r_1^2} + u_1$ or $\dot{r}_2 = r_1\dot{\theta}_2^2 - \frac{k}{r_1^2} + u_1$
 $\dot{\theta}_1 = \dot{\theta}_2$
 $\dot{\theta}_2 = -2\frac{r_2}{r_1}\dot{\theta}_2 + \frac{1}{r_1}u_2$

(c) if $u_1 = u_2 = 0$ + $k \neq 0$,
and we see that $\eta = 0$ is not allowable,
we have

$$\dot{r}_2 = r_1\dot{\theta}_2 - \frac{k}{r_1^2} = 0 \Rightarrow \dot{\theta}_2 = \frac{k}{r_1^3} \quad \text{or} \quad \dot{r}_2 = 0 \Rightarrow \dot{\theta}_2^2 = \frac{k}{r_1^2}$$

$\Rightarrow \dot{\theta}_1 = \dot{\theta}_2 \neq 0$ No equilibrium for these states.

(d) $x_1 = r_1 - \sigma \quad x_2 = r_2 = r_1 = \dot{x}_1 + \frac{\sigma}{\dot{r}_1}$
 $x_3 = \dot{\theta}_1 - \omega t \quad x_4 = \dot{\theta}_2 - \omega$
 $\dot{x}_1 = x_2$
 $\dot{x}_2 = (x_1 + \sigma)(x_4 + \omega) - \frac{k}{(x_1 + \sigma)^2} + u_1$ or $\dot{x}_2 = (x_1 + \sigma)(x_4 + \omega) - \frac{k}{(x_1 + \sigma)^2} + u_1$
 $\dot{x}_3 = x_4$
 $\dot{x}_4 = -2\frac{x_2}{(x_1 + \sigma)}(x_4 + \omega) + \frac{1}{(x_1 + \sigma)}u_2$

(e) if $u_1 = u_2 = 0$:
 $\dot{x}_2 = (x_1 + \sigma)(x_4 + \omega) - \frac{k}{(x_1 + \sigma)^2} = 0$

$$\Rightarrow (x_4 + \omega) = \frac{k}{(x_1 + \sigma)^3}$$

$$\text{if } x_1 = g \text{, then } \omega = \frac{k}{\sigma^3} \triangleq \frac{\sigma^3 \omega^2}{\omega} \checkmark$$

$$x_1 = 0, x_2 \neq 0 \quad \text{(assumed)}$$

$$x_2 = 0 \quad \text{(from above)}$$

$$x_3 = 0, x_4 = 0 \quad \text{(assumed)}$$

$$\dot{x}_4 = -2\frac{\sigma}{\omega}(x_4 + \omega) = 0, \checkmark$$

(In ω 's this
is how ω 's
dependence on
 σ is found)

$\Rightarrow [x] = 0$ is a valid
equilibrium.

Linearize (drop Δ 's, too messy otherwise!)

$$\dot{x}_1 = x_2$$

$$\dot{x}_2 = \omega x_1 + \sigma x_4 + 2\frac{k}{\sigma^3}x_1 + u_1$$

$$= (\omega + 2\omega^2)x_1 + \sigma x_4 \quad \text{or} = 3\omega^2 x_1 + 2\omega x_4$$

$$\dot{x}_3 = x_4$$

$$\dot{x}_4 = -2\frac{\omega}{\sigma}x_2 \oplus \frac{1}{\sigma}u_2$$

