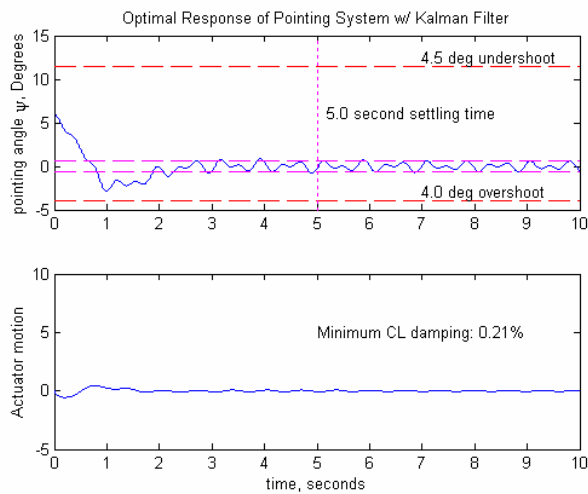


$W=10000*\text{diag}([1 \ 1 \ 1]);$   
 $V=1;$   
 $Q=1*\text{diag}([1 \ 1 \ 1 \ 1 \ 1 \ 1]);$   
 $R=.010;$

**Wow! Great performance with scaled identity matrices!**

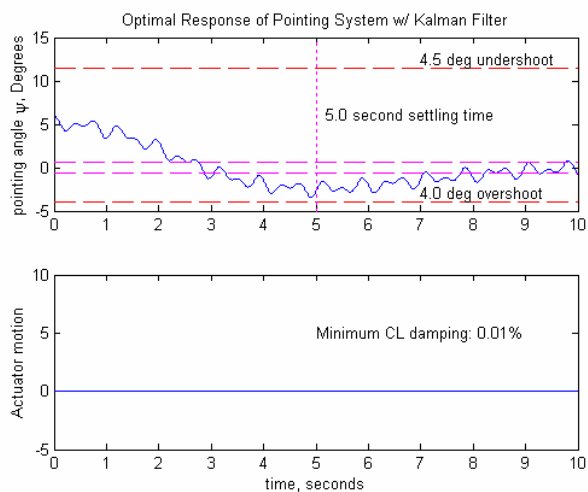
Base Score: 88 (Meets all specs)  
 Improved undershoot: +4  
 Improved settling time: +4  
 Improved actuator usage: +4  
 Total Score: 100



$q = 500; \ Q = \text{transpose}(C)*q*C;$   
 $R = 1;$   
 $V=10;$   
 $W=200*\text{eye}(3);$

**This one needs a lot more control effort – does not damp the structural modes**

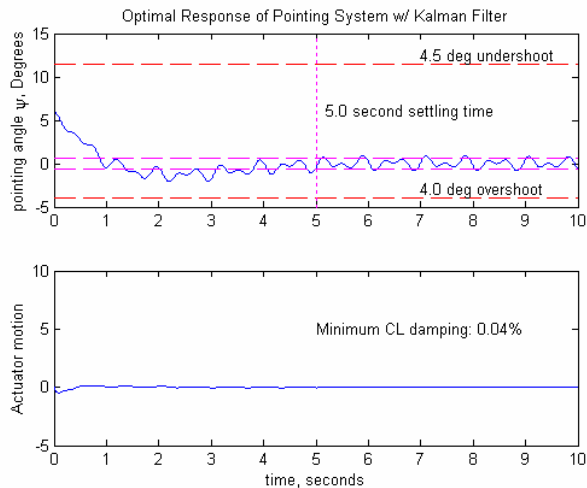
Base Score: 84 (Does not meet damping spec)  
 Improved undershoot: +4  
 Does not meet settling time: -4  
 Actuator usage: should have used more!  
 Total Score: 84



$q = \text{transpose}(C)*C;$   
 $r = 1;$   
 $w = [0.1,0,0;0,0.1,0;0,0,0.1];$   
 $v = 1;$

**Honorable mention for least control effort used...**

Base Score: 84 (Does not meet damping spec)  
 Improved undershoot: +4  
 Does not meet settling time: -4  
 Actuator usage: should have used more!  
 Total Score: 84



```
temp = 10000;
Q = C'*temp*C;
W = diag([.1 .1 .1]);
v = 0.1;
```

***Needs more control effort!***

Base Score: 84 (Does not meet damping spec)

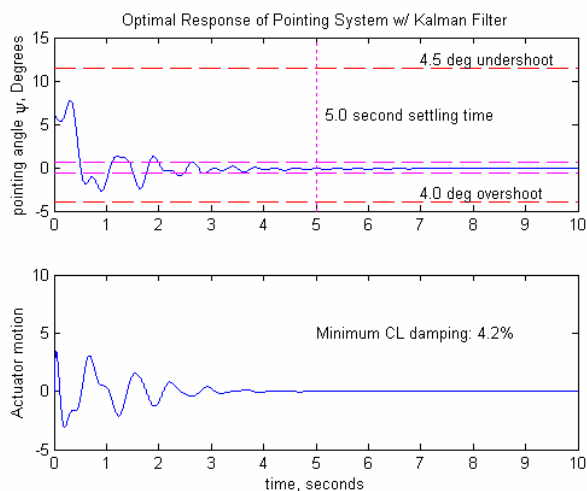
Improved undershoot: +4

Improved overshoot: +4

Does not meet settling time: -4

Actuator usage: should have used more!

Total Score: 88



% Q & R matrices

```
Q(6,6) = 100000; Q(5,5) = 5000;
```

```
Q(4,4) = 5000000; Q(2,2) = 1000000;
```

```
Q(3,3) = 10000; Q(1,1) = 10000;
```

```
R = 1;
```

```
W=10*eye(3),V=.001;
```

***Nice result after what appears to be some heavy iteration.***

Base Score: 88 (Meets all specs)

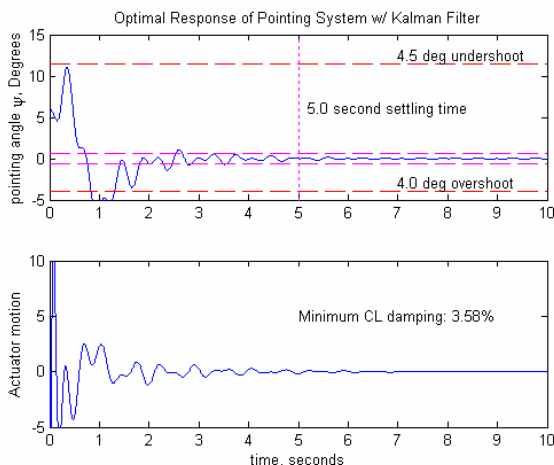
Improved undershoot: +4

Improved overshoot: +4

Improved settling time: +4

Actuator usage: Ok, I'll give you +2 (but 100 is the max)

Total Score: 102



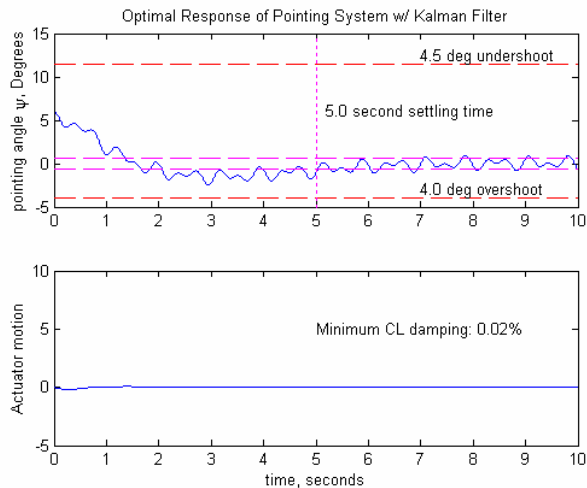
***This student used a pole placement approach – strangely enough, the damping requirements aren't quite met, which should be the first thing you get right when placing poles...***

Base Score: 82 (Misses overshoot spec, ~damping spec)

Improved settling time: +4

Actuator usage: -4 (typical problem in pole placement)

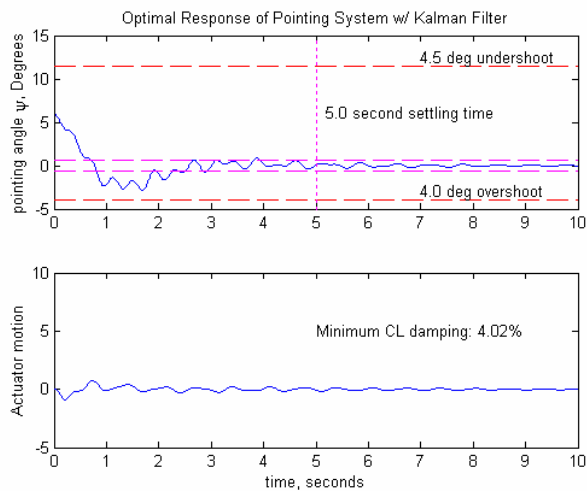
Total Score: 82



$W = [.3 \ 0 \ 0; 0 \ .3 \ 0; 0 \ 0 \ .3];$   
 $v = 1;$   
 $R = .05;$   
 $\text{var} = 10; Q = C' * \text{var} * C;$

**Another low-actuation usage case...**

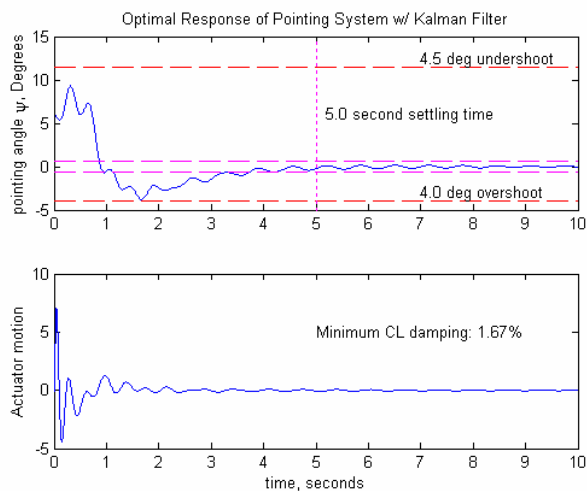
Base Score: 84 (Does not meet damping spec)  
 Improved undershoot: +4  
 Improved overshoot: +4  
 Does not meet settling time: -4  
 Actuator usage: should have used more!  
 Total Score: 88



$Q = [1 \ 0 \ 0 \ 0 \ 0; \ 0 \ 0.5 \ 0 \ 0 \ 0; \ 0 \ 0 \ 1 \ 0 \ 0$   
 $\quad \quad \quad 0 \ 0 \ 0 \ 10 \ 0; \ 0 \ 0 \ 0 \ 0 \ 1 \ 0; \ 0 \ 0 \ 0 \ 0 \ 0 \ 0.5];$   
 $R = 0.35;$   
 $W = [1 \ 0 \ 0; 0 \ 4.1; 0 \ 0 \ 300];$   
 $V = 0.04;$

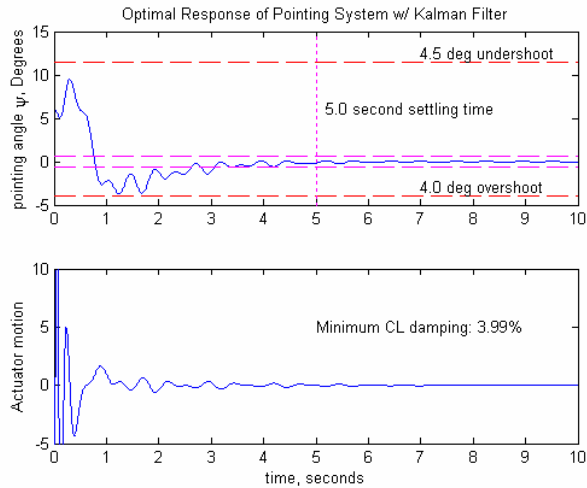
***This one gets the 'most bang for the buck' award – excellent response with very little control usage!***

Base Score: 88 (Meets all specs)  
 Improved undershoot: +4  
 Improved settling time: +4  
 Improved actuator usage: +4  
 Overshoot: don't be greedy now...  
 Total Score: 100



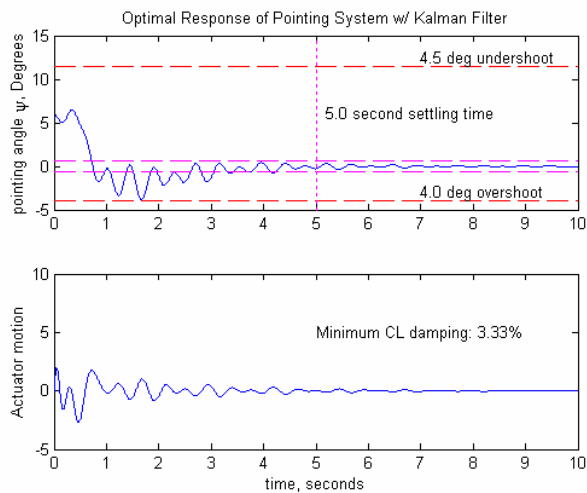
***This student used pole-placed eigenvalues for the observer, and an lqr controller. Again, there is a slight problem with damping but otherwise a respectable solution.***

Base Score: 84 (Misses the damping spec)  
 Improved settling time: Just sneaks in... +4  
 Total Score: 88



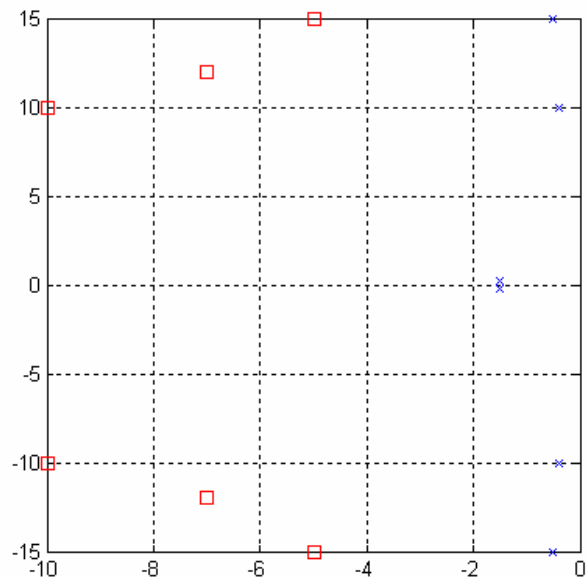
**Another pole placer... Here all the specs are met but at the price of high actuation levels, also fairly high frequency actuation.**

Base Score: 88 (meets all the specs)  
 Improved settling time: +4  
 Too much actuation: -4  
 Total Score: 88



**And finally! Proving it is possible to meet all of the specifications (almost) using pole placement, without using much actuation.**

Base Score: 86 (just misses the damping spec!)  
 Improved undershoot: +4  
 Improved settling time: +2 (peeks out at 4.2 sec)  
 Actuator usage: +4  
 Total Score: 96



Here are the poles that were used for this pole placement – the structural modes very judiciously placed along a 4% damping line, at about the same frequencies as the open loop poles – unfortunately numerical error pushed them slightly to the right, if my guess is right. Hence only 2 pts off for a near miss on this spec.

The observer poles are placed at somewhat higher frequencies, but not so high that they will pass a lot of noise. The roll-off characteristics (noise rejection) appear to be pretty good in the bode plot.