

Unit M1.5-*Example*

Statically Indeterminate Systems-- AN EXAMPLE (Handout - #M-3)

Readings:

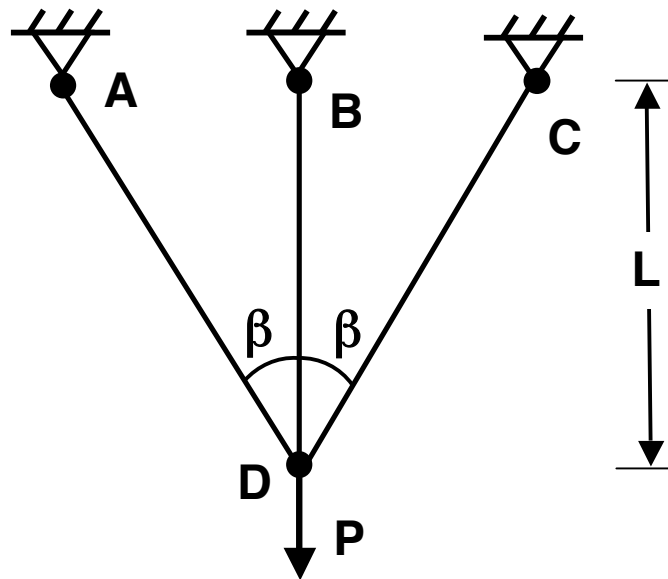
CDL 2.1, 2.3, 2.4, 2.7

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Look at another example and consider, more generally.....

Deflection of Trusses:

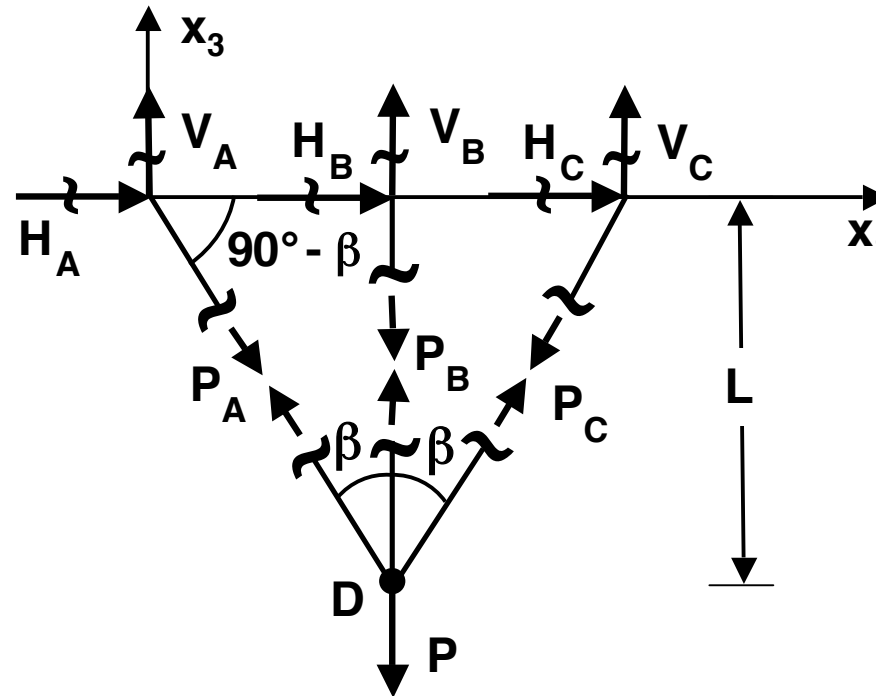
Figure M1.5-13 Example of three-bar truss



All bars are of same material (E) and area (A)

First.....

Figure M1.5-14 Draw the Free Body Diagram for the truss



Now apply the approach

--> Step 1: Apply equilibrium

At all the support points:

at A:

$$\begin{aligned}\sum F_H &= 0 \xrightarrow{+} \Rightarrow H_A + P_A \cos (90 - \beta) = 0 \\ &\Rightarrow H_A = -P_A \cos (90 - \beta)\end{aligned}$$

$$\begin{aligned}\sum F_V &= 0 \uparrow + \Rightarrow V_A - P_A \sin (90 - \beta) = 0 \\ &\Rightarrow V_A = P_A \sin (90 - \beta)\end{aligned}$$

at B:

$$\begin{aligned}\sum F_H &= 0 \xrightarrow{+} \Rightarrow H_B = 0 \\ \sum F_V &= 0 \uparrow + \Rightarrow V_B - P_B = 0 \\ &\Rightarrow V_B = P_B\end{aligned}$$

at C:

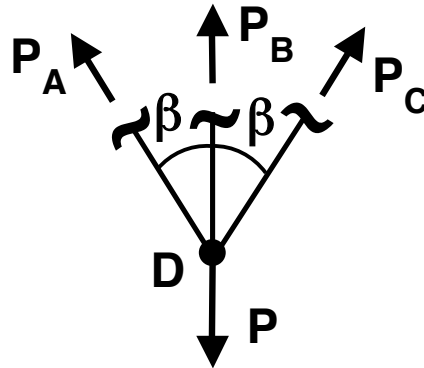
$$\begin{aligned}\sum F_H &= 0 \xrightarrow{+} \Rightarrow H_C - P_C \cos (90 - \beta) = 0 \\ &\Rightarrow H_C = P_C \cos (90 - \beta) \\ \sum F_V &= 0 \uparrow + \Rightarrow V_C - P_C \sin (90 - \beta) = 0 \\ &\Rightarrow V_C = P_C \sin (90 - \beta)\end{aligned}$$

--> We get all reactions once we know the loads
in the bars (P_A , P_B , P_C)

This tells us the reactions are equal to the loads in the bars (in magnitude and direction)

Proceed to consideration of the cut-off section

Figure M1.5-15 Free Body Diagram of cut-off section



Again apply equilibrium:

$$\sum F_H = 0 \xrightarrow{+} \Rightarrow -P_A \sin \beta + P_C \sin \beta = 0$$

$$\Rightarrow P_A = P_C \quad (1)$$

$$\sum F_V = 0 \uparrow + \Rightarrow P_A \cos \beta + P_B + P_C \cos \beta - P = 0 \quad (2)$$

using (1):

$$2P_C \cos \beta + P_B = P \quad (2^*)$$

We have 2 equations in 3 unknowns (P_A , P_B , P_C)

So go to:

--> Step 2: Determine constitutive relations

We have bars, so from before recall:

$$\delta = \frac{PL}{AE} + \alpha \Delta T L$$

$$\Delta T = 0 \text{ here so}$$

$$\Rightarrow \delta = \frac{PL}{AE}$$

$$\text{For bars A and C, length} = \frac{L}{\cos \beta}$$

The bars are of the same material and cross-sectional area, so AE is a constant.

Thus:

$$\delta_A = \frac{P_A L}{AE \cos \beta} \quad (3)$$

$$\delta_B = \frac{P_B L}{AE} \quad (4)$$

$$\delta_C = \frac{P_C L}{AE \cos \beta} \quad (5)$$

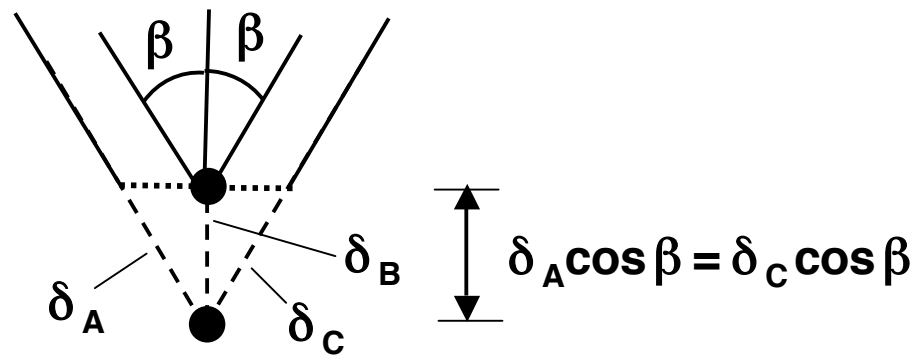
This gives us 5 equations in 6 unknowns (P_A , P_B , P_C , δ_A , δ_B , δ_C)

We now go to:

--> Step 3: Enforce compatibility of displacements

From the compatibility example done earlier..... (*zeroeth order solution*)

Figure M1.5-16 Illustration of displacement at point D (magnified)



We know:

$$\delta_A \cos \beta = \delta_B = \delta_C \cos \beta$$

This really represents two conditions:

$$\delta_A = \frac{\delta_B}{\cos \beta} \quad (6)$$

$$\delta_C = \frac{\delta_B}{\cos \beta} \quad (7)$$

With these two extra equations, we now have 7 equations in 6 unknowns (enough to solve, but one equation must be repetitive).

so finally....

--> Step 4: Solve the simultaneous equations

Equations (6) and (7) tell us:

$$\delta_A = \delta_C = \delta_B / \cos \beta$$

Using this in equations (3), (4) and (5) gives:

$$\delta_B / \cos \beta = \frac{P_A L}{AE \cos \beta} \quad (3^*)$$

$$\delta_B = \frac{P_B L}{AE} \quad (4^*)$$

$$\delta_B / \cos \beta = \frac{P_C L}{AE \cos \beta} \quad (5^*)$$

Note that equations (3*) and (5*) tell us $P_A = P_C$
(redundant from equation (1)!)

Now use equations (4*) and (5*) in these forms:

$$P_B = \frac{AE \delta_B}{L} = P_C = P_A$$

and in equation (2):

$$2AE \cos \beta \frac{\delta \beta}{L} + AE \frac{\delta \beta}{L} = P$$

$$\Rightarrow \boxed{\delta_B = \frac{PL}{AE} \frac{1}{1 + 2 \cos \beta}} \quad \text{deflection of point D}$$

Use this in equation (3*), (4*), and (5*) to get:

$$\begin{aligned} P_A &= P_C = \frac{P}{1 + 2\cos \beta} \\ P_B &= \frac{P}{1 + 2\cos \beta} \end{aligned}$$

Finally,

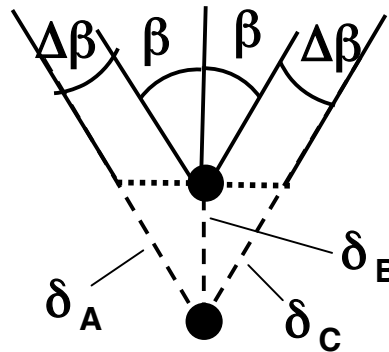
$$\delta_A = \delta_C = \frac{PL}{AE} \frac{1/\cos \beta}{1 + 2\cos \beta}$$

check units

$$\frac{\begin{bmatrix} N \end{bmatrix} \begin{bmatrix} m \end{bmatrix}}{\begin{bmatrix} m^2 \end{bmatrix} \begin{bmatrix} N / m^2 \end{bmatrix}} = \begin{bmatrix} m \end{bmatrix} \quad \checkmark \quad \text{units of deflection}$$

Final note of the deflection for this example (and truss in general)
Rotation is actually composed of extension and slight rotation.

Figure M1.5-17 Illustration of displacement at point D with magnified angle change noted



As before, must ignore small angle changes (assume deformations are small)

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