SOLUTIONS

Unified Quiz TMS4

November 19, 2008

M - PORTION

- · Put your name on each page of the exam.
- Read all questions carefully.
- Do all work on that question on the page(s) provided. Use back of the page(s) if necessary.
- Show all your work, especially intermediate results. Partial credit cannot be given without intermediate results.
- Show the logical path of your work. Explain <u>clearly</u> your reasoning and what you are doing. *In some cases, the reasoning is worth as much (or more) than the final answers.*
- Please be neat. It will be easier to identify correct or partially correct responses when the response is neat.
- Be sure to show the appropriate units throughout. Answers are not correct without the units.
- Report significant digits only.
- Box your final answers.
- · Calculators are allowed.
- Print-outs of Handout "HO-M-7" along with 2 sides of pages of handwritten material are allowed.

EXAM SCORING

#1M = FINAL SCORE	

A large slab of a relatively compliant material is in the x_2 - x_3 plane. This slab is outfitted with strain gages and the slab is loaded by stresses along multiple axes. While undergoing this multiaxial stress state, it is determined that the strain gages show that the strains are:

$$\varepsilon_{22} = -4000 \,\mu$$
strain $\varepsilon_{33} = +8000 \,\mu$ strain $\gamma_{23} = +10,000 \,\mu$ strain

where the shear strain is engineering shear strain. It is furthermore known that the strain does not vary through the thickness of the slab, i.e. with x_1 , and any strains involving the x_1 -direction are equal to zero.

- (a) Can one draw a rectangle on the slab of material that will maintain its shape as a rectangle? If not, why not? If so, what is its orientation? How will its rectangular aspect ratio change in that case, if at all? Clearly explain your reasoning.
- -> A rectangle will maintain its rectangular shape in a direction where there is no shear stoir, and thus no angular determation/change.
 - -> Thus it is the principal axis system of the strains where this will occur.
 - -> Foran in-plane strain system, the principal strains are the voicts of the equation:

 \(\tau \) = \(\tau \) \(\tau
- -> No to in this case the sheer strain is engineering sheerstrain, so this must be converted to tensorial shear street to 23 2

Fo have: €22= -4000 MS €33= +8000 MS

E23 =+2000 m

-> Proceed withthe equation for the moto.

(sw jurkoun)

72-τ(4×10 3 μs) + (-32×106-25×10 tus)²=0

βiving: τ²-τ(4×10 3 μs) - 57×10 (μs)²=0

-> Solve via the factoratic formula: τ= 5±1/5²-4ac

2 a

here: A = 1 $C = -4 \times 10^{3} \text{ ms}$ $C = -57 \times 10^{6} \text{ (ms)}^{2}$

=) $T = \frac{4 \times 10^{-3} \pm \sqrt{(16 \times 10^{-6}) - 4(1)(-57 \times 10^{-6})}}{2}$

 $= \frac{4 \pm \sqrt{16 + 228} \times 10^3 \, \text{ms}}{2}$

 $= \frac{4 \pm \sqrt{244}}{2} \times 10^{3} \text{ Ms} = \frac{4 \pm 75.6}{2} \times 10^{3} \text{ Ms}$

Frally: 7 = 9800 ustan, - 5500 ustrain

So: Principal straw: E, FI = 9500 postour, -5800

Note: Check in Extensional = content = 400 pustam V

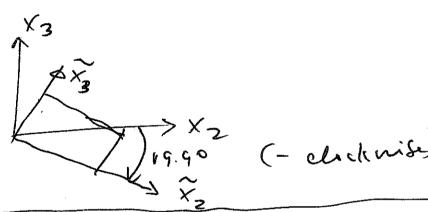
-> get the avection associated with this via:

$$\theta_p = \frac{1}{2} \tan^{-1} \left(\frac{2 + 23}{522 + 633} \right)$$

$$= \frac{1}{2} \tan^{-1} \left(\frac{10 \times 10^3 \text{ nothern}}{-12 \times 10^3 \text{ nothern}} \right)$$

Op = \frac{1}{2} tan (-5) = = (-39.f°)

=> [Principal direction: Op = -19.90]



Rectargle in X X3 Syrtem, -19.9° knu X2, X3 will otay a rectangle

Its expect ratio will change via

BUZ = E22 ; BUZ = 533

for constant other as is the case, the diturnation

chaperato is:

$$\left|\frac{\Delta U_3}{\Delta U_2}\right|^2 \left|\frac{\xi_{33}}{\xi_{22}}\right|$$

| DU3 | = | \frac{\xi33}{\xi22|} rant look at this in (xxxxyrtem of rectangle (xx, x3)

(b) The stresses are altered along the various axes, but this does not result in a change in the strains measured by the strain gages, or any in the x₁-direction. Will this change the deformation of the slab? Clearly explain your reasoning.

If the strain does not change, the deformation will not change. The deformation is directly related to the strain and is not directly affected by the otherses. The deformation is affected by the stresses. The deformation is affected by the stresses only if it were to affect the stains.

(c) The loading is now changed so that the deformations are increased by a factor of thirty. How will this affect the values of the in-plane strains? **Clearly explain your reasoning.**

The key issue here is whether all remains "Somall and linear "such that thestrains increase linearly by the same factor of 30 as the deformation. This would give F22 = 120, 000 ustain and €33 = + 240,000 tustain. There are rather large, but it becomes clearer whether the assumption of small displacements and small angles is breaking down by looking at the shear strain and the arrociated angle change, i. e. ozs. If this neverses linearly by a factor of 30, this fiver: 823: +300,000 usthain. Recalling trut the total angle hange is liqual to the engineery stain, this fires a change in radians of 0.30. This is 17.20 and fives cop 0 of 0.955. So this is 4.5% off cop 0=1. Thus, there is expling to the en extention and rhear that needs to be taken into account. Therefore I say my simply that the strains were ase by a linear factor of 30 would be using an approximation that is breaking down!