# Fluids – Lecture 15 Notes

- 1. Mach Number Relations
- 2. Normal-Shock Properties

Reading: Anderson 8.4, 8.6

## Mach Number Relations

#### Local Mach number

For a perfect gas, the speed of sound can be given in a number of ways.

$$a = \sqrt{\gamma RT} = \sqrt{\frac{\gamma p}{\rho}} = \sqrt{(\gamma - 1)h}$$
(1)

The dimensionless *local Mach number* can then be defined.

$$M \equiv \frac{V}{a} = \sqrt{\frac{\rho(u^2 + v^2 + w^2)}{\gamma p}} = \sqrt{\frac{u^2 + v^2 + w^2}{(\gamma - 1)h}}$$

It's important to note that this is a field variable M(x, y, z), and is distinct from the freestream Mach number  $M_{\infty}$ . Likewise for V and a.



The local stagnation enthalpy can be given in terms of the static enthalpy and the Mach number, or in terms of the speed of sound and the Mach number.

$$h_o = h + \frac{1}{2}V^2 = h\left(1 + \frac{1}{2}\frac{V^2}{h}\right) = h\left(1 + \frac{\gamma - 1}{2}M^2\right) = \frac{a^2}{\gamma - 1}\left(1 + \frac{\gamma - 1}{2}M^2\right)$$
(2)

This now allows the isentropic relations

$$\frac{p_o}{p} = \left(\frac{\rho_o}{\rho}\right)^{\gamma} = \left(\frac{h_o}{h}\right)^{\gamma/(\gamma-1)}$$

to be put in terms of the Mach number rather than the speed as before.

$$\frac{\rho_o}{\rho} = \left(1 + \frac{\gamma - 1}{2}M^2\right)^{1/(\gamma - 1)}$$
$$\frac{p_o}{p} = \left(1 + \frac{\gamma - 1}{2}M^2\right)^{\gamma/(\gamma - 1)}$$

The following relation is also sometimes useful.

$$1 - \frac{V^2}{2h_o} = \left(1 + \frac{\gamma - 1}{2}M^2\right)^{-1}$$

### **Normal-Shock Properties**

#### Mach jump relations

We now seek to determine the properties  $\rho_2, u_2, p_2, h_2$  downstream of the shock, as functions of the known upstream properties  $\rho_1, u_1, p_1, h_1$ . In practice, it is sufficient and much more convenient to merely determine the downstream Mach number  $M_2$  and the variable <u>ratios</u>, since these are strictly functions of the upstream Mach number  $M_1$ .

$$\begin{array}{c|c} \rho_1 & & & \rho_2 = ? \\ u_1 & & & u_2 = ? \\ p_1 & & & p_2 = ? \\ h_1 & & & h_2 = ? \end{array} \end{array} \xrightarrow{} \begin{array}{c} M_2 = f(M_1) \\ \rho_2 / \rho_1 = f(M_1) \\ p_2 / p_1 = f(M_1) \\ h_2 / h_1 = f(M_1) \end{array}$$

The starting point is the normal shock equations obtained earlier, with V = u for this 1-D case. They are also known as the *Rankine-Hugoniot* shock equations.

$$\rho_1 u_1 = \rho_2 u_2 \tag{3}$$

$$\rho_1 u_1^2 + p_1 = \rho_2 u_2^2 + p_2 \tag{4}$$

$$h_1 + \frac{1}{2}u_1^2 = h_2 + \frac{1}{2}u_2^2 \tag{5}$$

$$p_2 = \frac{\gamma - 1}{\gamma} \rho_2 h_2 \tag{6}$$

Dividing the momentum equation (4) by the continuity equation (3) gives

or 
$$u_1 + \frac{p_1}{\rho_1 u_1} = u_2 + \frac{p_2}{\rho_2 u_2}$$
  
 $u_1 - u_2 = \frac{1}{\gamma} \left( \frac{a_2^2}{u_2} - \frac{a_1^2}{u_1} \right)$  (7)

where we have substituted  $p/\rho=a^2/\gamma$  and rearranged the terms.

Now we make use of the energy equation (5). For algebraic convenience we first define the constant total enthalpy in terms of the known upstream quantities

$$h_1 + \frac{1}{2}u_1^2 \equiv h_o = h_2 + \frac{1}{2}u_2^2$$

which then gives  $a_1^2$  and  $a_2^2$  in terms of  $u_1$  and  $u_2$ , respectively.

$$a_1^2 = (\gamma - 1)h_1 = (\gamma - 1)\left(h_o - \frac{1}{2}u_1^2\right)$$
  
$$a_2^2 = (\gamma - 1)h_2 = (\gamma - 1)\left(h_o - \frac{1}{2}u_2^2\right)$$

Substituting these energy relations into the combined momentum/mass relation (7) gives, after some further manipulation

$$u_1 - u_2 = \frac{\gamma - 1}{\gamma} \left( \frac{h_o}{u_2} - \frac{h_o}{u_1} + \frac{1}{2} (u_1 - u_2) \right)$$

Dividing by  $u_1 - u_2$  produces

$$1 = \frac{\gamma - 1}{\gamma} \left( \frac{h_o}{u_1 u_2} + \frac{1}{2} \right) \tag{8}$$

(10)

$$\frac{(\gamma - 1)h_o}{u_1 u_2} = \frac{\gamma + 1}{2} \\ \frac{(\gamma - 1)^2 h_o^2}{u_1^2 u_2^2} = \left(\frac{\gamma + 1}{2}\right)^2$$
(9)

Since  $h_o = h_{o_1} = h_{o_2}$ , we can write

$$(\gamma - 1)^2 h_o^2 = (\gamma - 1) h_{o_1} (\gamma - 1) h_{o_2} = a_1^2 \left( 1 + \frac{\gamma - 1}{2} M_1^2 \right) a_2^2 \left( 1 + \frac{\gamma - 1}{2} M_2^2 \right)$$

and using this to eliminate  $h_o^2$  from equation (9), and solving for  $M_2$ , yields the desired  $M_2(M_1)$  function. This is shown plotted for  $\gamma = 1.4$ .



The  $M_1 \rightarrow 1^+$ ,  $M_2 \rightarrow 1^-$  limit corresponds to infinitesimal shock, or a sound wave. The

 $M_2(M_1)$  function is not shown for  $M_1 < 1$ , since this would correspond to an "expansion"

shock" which is physically impossible based on irreversibility considerations.

#### Static jump relations

The jumps in the static flow variables are now readily determined as ratios using the known  $M_2$ . From the mass equation (3) we have

$$\frac{\rho_2}{\rho_1} = \frac{u_1}{u_2} = \frac{u_1^2}{u_1 u_2}$$

From the Mach definition we have

$$u_1^2 = M_1^2 a_1^2 = M_1^2 \frac{(\gamma - 1)h_o}{1 + \frac{\gamma - 1}{2}M_1^2}$$

and from equation (8) we have

$$\frac{1}{u_1 u_2} = \frac{1}{(\gamma - 1)h_o} \frac{\gamma + 1}{2}$$

Combining these gives the shock density ratio in terms of  $M_1$  alone.

$$\frac{\rho_2}{\rho_1} = \frac{(\gamma+1)M_1^2}{2+(\gamma-1)M_1^2} \tag{11}$$

The combination of the momentum equation (4) and mass equation (3) gives

$$p_2 - p_1 = \rho_1 u_1^2 - \rho_2 u_2^2 = \rho_1 u_1^2 \left( 1 - \frac{u_2}{u_1} \right) = \rho_1 u_1^2 \left( 1 - \frac{\rho_1}{\rho_2} \right)$$

which can be further simplified by using the general relation  $\rho u^2 = \gamma p M^2$ , dividing by  $p_1$ , and then using (11) to eliminate  $\rho_2/\rho_1$  in terms of  $M_1$ . The final result for the shock static pressure ratio is

$$\frac{p_2}{p_1} = 1 + \frac{2\gamma}{\gamma+1} \left( M_1^2 - 1 \right) \tag{12}$$

The static temperature or enthalpy ratio is now readily obtained from the pressure and density ratios via the state equation.

$$\frac{T_2}{T_1} = \frac{p_2}{p_1} \frac{\rho_1}{\rho_2}$$

The result is

$$\frac{T_2}{T_1} = \frac{h_2}{h_1} = \left[1 + \frac{2\gamma}{\gamma+1} \left(M_1^2 - 1\right)\right] \frac{2 + (\gamma-1)M_1^2}{(\gamma+1)M_1^2}$$
(13)

The three static quantity ratios (11), (12), (13), are shown plotted versus  $M_1$ .

