

# Massachusetts Institute of Technology Department of Aeronautics and Astronautics <br> Cambridge, MA 02139 

16.003/16.003 Unified Engineering III, IV Spring 2009

## Problem Set 6

Name: $\qquad$

Due Date: 3/20/2009

|  | Time Spent <br> (min) |
| :--- | :---: |
| T12 |  |
| T13-14 |  |
| S1 |  |
| Study <br> Time |  |

[^0]
## Unified Engineering <br> Thermodynamics \& Propulsion

Spring 2009
(Add a short summary of the concepts you are using to solve the problem)

## Problem T12

Consider the following Rankine cycles. Steam at 20 bar, $360^{\circ} \mathrm{C}$ is expanded in a steam turbine to 0.08 bar. It then enters a condenser, where it is condensed to saturated liquid water. The pump feeds back the water into the boiler.
a) Assuming ideal processes, sketch the cycle in a T-s diagram and find the net work and the cycle efficiency per kg of steam.
b) If the turbine and the pump each have $80 \%$ efficiency, find the percentage reduction in the net work and cycle efficiency. Sketch the non-ideal cycle in the same T-s diagram.

# Unified Engineering <br> Thermodynamics \& Propulsion 

Spring 2009
Z. S. Spakovszky
(Add a short summary of the concepts you are using to solve the problem)

## Problem T13-T14

One method of producing liquid nitrogen is to use the system shown below. Nitrogen gas at a pressure of 100 bar and a temperature of 300 K flows at a rate of $10 \mathrm{~m}^{3} / \mathrm{min}$ (measured at 1 bar ) through the heat exchanger, thereby decreasing in temperature. As it flows through the Joule-Thomson valve, its pressure is reduced from 100 bar to 1 bar and in the process some liquid is formed. The gas which is not liquefied, but has a reduced temperature, flows out through the counter-flow heat exchanger. The temperature of this discharge stream is 297 K . Assume that the heat exchange is externally adiabatic.
a) Sketch the process in a T-s diagram and label all states.
b) Find the mass flow into the heat exchanger.
c) Determine the heat transferred in the heat exchanger.
d) Determine the rate at which liquid nitrogen is delivered by this system.
e) Sketch the temperature difference in the heat exchanger versus the temperature of the low-pressure stream. Is the heat transfer process in the heat exchanger reversible? Why or why not? (No calculation is needed here, an explanation in a few sentences is expected)


Thermodynamic Properties of Nitrogen

| Temp. <br> K <br> $T$ | Press.$\mathrm{kPa}$$P$ | Specific Volume, $\mathrm{m}^{3} / \mathrm{kg}$ |  |  | Internal Energy, kJ/kg |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Sat. Liquid $v_{r}$ | Evap. <br> v/k | Sat. Vapor $v_{k}$ | Sat. Liquid ${ }^{\prime \prime}$ | Evap. $u_{f s}$ | $\begin{gathered} \text { Sat. Vaper } \\ u_{\pi} \\ \hline \end{gathered}$ |
| 63.1 | 12.5 | 0.001150 | 1.48074 | 1.48189 | -150.92 | 196.86 | 45.94 |
| 65 | 17.4 | 0.001160 | 1.09231 | 1.09347 | -147.19 | 194.37 | 47.17 |
| 70 | 38.6 | 0.001191 | 0.52513 | 0.52632 | -137.13 | 187.54 | 50.40 |
| 75 | 76.1 | 0.001223 | 0.28052 | 0.28174 | -127.04 | 180.47 | 53.43 |
| 77.3 | 101.3 | 0.001240 | 0.21515 | 0.21639 | -122.27 | 177.04 | 54.76 |
| 80 | 137.0 | 0.001259 | 0.16249 | 0.16375 | -116.86 | 173.06 | 56.20 |
| 85 | 229.1 | 0.001299 | 0.10018 | 0.10148 | -106.55 | 165.20 | 58.65 |
| 90 | 360.8 | 0.001343 | 0.06477 | 0.06611 | -96,06 | 156.76 | 60.70 |
| 95 | 541.1 | 0.001393 | 0.04337 | 0.04476 | -85.35 | 147.60 | 62.25 |
| 100 | 779.2 | 0.001452 | 0.02975 | 0.03120 | -74.33 | 137.50 | 63.17 |
| 105 | 1084.6 | 0.001522 | 0.02066 | 0.02218 | -62.89 | 126.18 | 63.29 |
| 110 | 1467.6 | 0.001610 | 0.01434 | 0.01595 | -50.81 | 113.11 | 62.31 |
| 115 | 1939.3 | 0.001729 | 0.00971 | 0.01144 | -37.66 | 97.36 | 59.70 |
| 120 | 2513.0 | 0.001915 | 0.00608 | 0.00799 | -22.42 | 76.63 | 54.21 |
| 125 | 3208.0 | 0.002355 | 0.00254 | 0.00490 | -0.83 | 40.73 | 39.90 |
| 126.2 | 3397.8 | 0.003194 | 0 | 0.00319 | 18.94 | 0 | 18.94 |
| TABLE B.6.2 SI Superteated Narogen |  |  |  |  |  |  |  |
| Temp. <br> K | $\mathrm{m}^{3} / \mathrm{kg}$ | $\begin{array}{cc} h & s \\ \mathrm{~kJ} / \mathrm{kg} & \mathrm{~kJ} / \mathrm{kg} \mathrm{~K} \end{array}$ | $\begin{array}{ll} \mathrm{K} & \mathrm{v} \\ \mathrm{~m}^{3} / \mathrm{kg} \end{array}$ | $\begin{array}{r} \mathrm{h} \\ \mathrm{~kJ} / \mathrm{kg} \end{array}$ | kJ/kg K | $\begin{array}{cc} v & h \\ \mathrm{~m}^{3} / \mathrm{kg} & \mathrm{~kJ} / / \mathrm{kg} \end{array}$ | kJ/kg K |
|  | $100 \mathrm{kPa}(77.24)$ |  | $200 \mathrm{kPa}(83.62)$ |  |  | $500 \mathrm{kPa}(93.98)$ |  |
| Sat. | 0.21903 | $76.61 \quad 5.4059$ | 0.11520 | - 81.05 | 5.2673 | $0.04834 \quad 86.15$ | 5.0802 |
| 100 | 0.29103 | 101.945 .6944 | 0.14252 | 2100.24 | 5.4775 | $0.05306 \quad 94.46$ | 5.1660 |
| 120 | 0.35208 | $123.15 \quad 5.8878$ | 0.17397 | - 121.93 | 5.6753 | $0.06701 \quad 118.12$ | 2 5,3821 |
| 140 | 0.41253 | $144.20 \quad 6.0501$ | 0.20476 | - 143.28 | 5.8399 | $0.08007 \quad 140.44$ | 4.5541 |
| 160 | $0.47263$ | $165.17 \quad 6.1901$ | 0.23519 | 164,44 | 5.9812 | $0.09272 \quad 162.22$ | $2 \quad 5.6996$ |
| 180 | 0.53254 | $186.09 \quad 6.3132$ | $0.26542$ | 185.49 | $6.1052$ | $0.10515 \quad 183.70$ | $\begin{array}{ll} 0 & 5.8261 \end{array}$ |
| 200 | 0.59231 | $206.97 \quad 6.4232$ | 0.29551 | 206.48 | 6.2157 | $0.11744 \quad 205.00$ | O 5.9383 |
| 220 | 0.65199 | $227.83 \quad 6.5227$ | 0.32552 | 2227.41 | 6.3155 | $0.12964 \quad 226.18$ | 8.8 .0392 |
| 240 | 0.71161 | $248.67 \quad 6.6133$ | 0.35546 | 248.32 | 6.4064 | $0.14177 \quad 247.27$ | $7 \quad 6.1310$ |
| 260 | 0.77118 | 269.51 6.6967 | 0.38535 | 269.21 | 6.4900 | $0.15385 \quad 268.31$ | 16.2152 |
| 280 | 0.83072 | $290.33 \quad 6.7739$ | 0.41520 | - 290.08 | 6.5674 | $0.16590 \quad 289.31$ | 16.2930 |
| TABLE B.6.I SI (Continued) Saturated Nïrogen |  |  |  |  |  |  |  |
| Temp. <br> K <br> $T$ | Press. <br> kPa $P$ | Enthalpy, kJ/kg |  |  | Entropy, kJ/kg K |  |  |
|  |  | Sat. Liquid $h_{f}$ | Evap. $h_{\text {fo }}$ | $\begin{gathered} \text { Sat. Vapor } \\ h_{s} \end{gathered}$ | Sat. Liquid ${ }_{5 f}$ | Evap. <br> $s_{f i r}$ | $\begin{aligned} & \text { Sat. Vapor } \\ & s_{s} \\ & \hline \end{aligned}$ |
| 63.1 | 12.5 | -150.91 2 | 215.39 | 64.48 | 2.4234 | 3.4109 | 5.8343 |
| 65 | 17.4 | -147.17 | 213.38 | 66.21 | 2.4816 | 3.2828 | 5.7645 |
| 70 | 38.6 | -137.09 207 | 207.79 | 70.70 | 2.6307 | 2.9684 | 5.5991 |
| 75 | 76.1 | -126.95 | 201.82 | 74.87 | 2.7700 | 2.6509 | 5.4609 |
| 77.3 | 101.3 | -122.15 | 198.84 | 76.69 | 2.8326 | 2.5707 | 5.4033 |
| 80 | 137.0 | -116.69 | 195.32 | 78.63 | 2.9014 | 2.4415 | 5.3429 |
| 85 | 229.1 | -106.25 | 188.15 | 81.90 | 3.0266 | 2.2135 | 5.2401 |
| 90 | 360.8 | -95.58 | 180.13 | 84.55 | 3.1466 | 2.0015 | 5.1480 |
| 95 | 541.1 | -84.59 | 171.07 | 86.47 | 3.2627 | 1.8007 | 5.0634 |
| 100 | 779.2 | .73.20 | 160.68 | 87.48 | 3.3761 | 1.6068 | 4.9829 |
| 105 | 1084.6 | -61.24 | 148.59 | 87.35 | 3.4883 | 1.4151 | 4.9034 |
| 110 | 1467.6 | -48,45 | 134.15 | 85.71 | 3.6017 | 1.2196 | 4.8213 |
| 115 | 1939.3 | -34.31 | 116.19 | 81.88 | 3.7204 | 1.0104 | 4.7307 |
| 120 | 2513.0 | -17.61 | 91.91 | 74.30 | 3.8536 | 0.7659 | 4.6195 |
| 125 | 3208.0 | 6.73 | 48.88 | 55.60 | 4.0399 | 0.3910 | 4.4309 |
| 126.2 | 3397.8 | 29.79 | 0 | 29.79 | 4.2193 | 0 | 4.2193 |

TABLE B.6.2 SI (Continued) Superheated Nitrogen

| Temp. <br> K | $\mathrm{m}^{\mathrm{F}} / \mathrm{kg}$ | $\stackrel{h}{\mathrm{k} \cdot / / \mathrm{kg}}$ | $\mathrm{kJ} / \mathrm{kg} \mathrm{K}$ | $\stackrel{v}{\mathrm{~m}^{3} / \mathrm{kg}}$ | $\begin{gathered} h \\ \mathrm{~kJ} / \mathrm{kg} \end{gathered}$ | $\mathrm{kJ} / \mathrm{kg} \mathrm{K}$ | $\mathrm{m}^{3 / \mathrm{kg}}$ | $\stackrel{h}{\mathrm{k} \cdot \mathrm{~J} / \mathrm{kg}}$ | kJ/kg K |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $100 \mathrm{kPa}(77.24)$ |  |  | $200 \mathrm{kPa}(83.62)$ |  |  | $500 \mathrm{kPa}(93.98)$ |  |  |
| 300 | 0.89023 | 311.16 | 6.8457 | 0.44503 | 310.94 | 6.6393 | 0.17792 | 310.28 | 6.3653 |
| 350 | 1.03891 | 363.24 | 7.0063 | 0.51952 | 363.09 | 6.8001 | 0.20788 | 362.63 | 6.5267 |
| 400 | 1.18752 | 415.41 | 7.1456 | 0.59392 | 415.31 | 6.9396 | 0.23777 | 414.99 | 6.6666 |
| 450 | 1.33607 | 467.77 | 7.2690 | 0.66827 | 467.70 | 7.0630 | 0.26759 | 467.49 | 6.7902 |
| 500 | 1.48488 | 520.41 | 7.3799 | 0.74258 | 520.37 | 7.1740 | 0.29739 | 520.24 | 6.9014 |
| 600 | 1.78154 | 626.94 | 7.5741 | 0.89114 | 626.94 | 7.3682 | 0.35691 | 626.93 | 7.0959 |
| 700 | 2.07845 | 735.58 | 7.7415 | 1.03965 | 735.61 | 7.5357 | 0.41637 | 735.68 | 7.2635 |
| 800 | 2.37532 | 846.60 | 7.8897 | 1.18812 | 846.64 | 7.6839 | 0.47581 | 846.78 | 7.4118 |
| 900 | 2.67217 | 960.01 | 8.0232 | 1.33657 | 960.07 | 7.8175 | 0.53522 | 960.24 | 7.5454 |
| 1000 | 2.96900 | 1075.68 | 8.1451 | 1.48501 | 1075.75 | 7.9393 | 0.59462 | 1075.96 | 7.6673 |

TABLE B. 6.2 SI (Continued) Superheated Nïrogen


| Sat. | $600 \mathrm{kPa}(96.37)$ |  |  | $800 \mathrm{kPa}(100.38)$ |  |  | $1000 \mathrm{kPa}(103.73)$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.04046 | 86.85 | 5.0411 | 0.03038 | 87.52 | 4.9768 | 0.02416 | 87.51 | 4.9237 |
| 120 | 0.05510 | 116.79 | 5.3204 | 0.04017 | 114.02 | 5.2191 | 0.03117 | 111.08 | 5.1357 |
| 140 | 0.06620 | 139.47 | 5.4953 | 0.04886 | 137.50 | 5,4002 | 0,03845 | 135.47 | 5.3239 |
| 160 | 0.07689 | 161.47 | 5.6422 | 0.05710 | 159.95 | 5.5501 | 0.04522 | 158.42 | 5.4772 |
| 180 | 0.08734 | 183.10 | 5.7696 | 0.06509 | 181.89 | 5.6793 | 0.05173 | 180.67 | 5.6082 |
| 200 | 0.09766 | 204.50 | 5.8823 | 0.07293 | 203.51 | 5.7933 | 0,05809 | 202.52 | 5.7234 |
| 220 | 0.10788 | 225.76 | 5.9837 | 0.08067 | 224.94 | 5.8954 | 0.06436 | 224.11 | 5.8263 |
| 240 | 0.11803 | 246.92 | 6.0757 | 0.08835 | 246.23 | 5.9880 | 0.07055 | 245.53 | 5.9194 |
| 260 | 0.12813 | 268.01 | 6.1601 | 0.09599 | 267.42 | 6.0728 | 0.07670 | 266.83 | 6.0047 |
| 280 | 0.13820 | 289.05 | 6.2381 | 0.10358 | 288.54 | 6.1511 | 0.08281 | 288.04 | 6.0833 |
| 300 | 0.14824 | 310.06 | 6.3105 | 0.11115 | 309.62 | 6.2238 | 0.08889 | 309.18 | 6.1562 |
| 350 | 0.17326 | 362.48 | 6.4722 | 0.12998 | 362.17 | 6.3858 | 0.10401 | 361.87 | 6.3187 |
| 400 | 0.19819 | 414.89 | 6.6121 | 0.14873 | 414.68 | 6.5260 | 0.11905 | 414.47 | 6.4591 |
| 450 | 0.22308 | 467.42 | 6.7359 | 0.16743 | 467.28 | 6.6500 | 0.13404 | 467.15 | 6.5832 |
| 500 | 0.24792 | 520.20 | 6.8471 | 0.18609 | 520.12 | 6.7613 | 0.14899 | 520.04 | 6.6947 |
| 600 | 0.29755 | 626.93 | 7.0416 | 0.22335 | 626.93 | 6.9560 | 0.17883 | 626.92 | 6.8895 |
| 700 | 0.34712 | 735.70 | 7.2093 | 0.26056 | 735.76 | 7.1237 | 0.20862 | 735.81 | 7.0573 |
| 800 | 0.39666 | 846.82 | 7.3576 | 0.29773 | 846.91 | 7.2721 | 0.23837 | 847.00 | 7.2057 |
| 900 | 0.44618 | 960.30 | 7.4912 | 0.33488 | 960.42 | 7.4058 | 0.26810 | 960.54 | 7.3394 |
| 1000 | 0.49568 | 1076.02 | 7.6131 | 0.37202 | 1076.16 | 7.5277 | 0.29782 | 1076.30 | 7.4614 |
|  | $1500 \mathrm{kPa}(110.38)$ |  |  | 2000 kPa ( 115.58 ) |  |  | $3000 \mathrm{kPa}(123.61)$ |  |  |
| Sat | 0.01555 | 85.51 | 4.8148 | 0.01100 | 81.25 | 4.7193 | 0.00582 | 63.47 | 4.5032 |
| 120 | 0.01899 | 102.75 | 4.9650 | 0.01260 | 92.10 | 4.8116 | - | - | - |
| 140 | 0.02452 | 130.15 | 5,1767 | 0.01752 | 124.40 | 5.0618 | 0.01038 | 111.13 | 4.8706 |
| 160 | 0.02937 | 154.50 | 5.3394 | 0.02144 | 150.43 | 5.2358 | 0.01350 | 141.85 | 5.0763 |
| 180 | 0.03393 | 177.60 | 5.4755 | 0.02503 | 174.48 | 5.3775 | 0.01614 | 168.09 | 5.2310 |
| 200 | 0.03832 | 200.03 | 5.5937 | 0.02844 | 197.53 | 5.4989 | 0.01857 | 192.49 | 5.3596 |
| 220 | 0.04260 | 222.05 | 5.6987 | 0.03174 | 219.99 | 5.6060 | 0.02088 | 215.88 | 5.4711 |
| 240 | 0.04682 | 243.80 | 5.7933 | 0.03496 | 242.08 | 5.7021 | 0.02312 | 238.66 | 5.5702 |
| 260 | 0.05099 | 265.36 | 5.8796 | 0.03814 | 263.90 | 5.7894 | 0.02531 | 261.02 | 5.6597 |
| 280 | 0.05512 | 286.78 | 5.9590 | 0.04128 | 285.53 | 5.8696 | 0.02746 | 283.09 | 5.7414 |
| 300 | 0.05922 | 308.10 | 6.0325 | 0.04440 | 307.03 | 5.9438 | 0.02958 | 304.94 | 5.8168 |
| 350 | 0.06940 | 361.13 | 6.1960 | 0.05209 | 360.39 | 6.1083 | 0.03480 | 358.96 | 5.9834 |
| 400 | 0.07949 | 413.96 | 6.3371 | 0.05971 | 413.47 | 6.2500 | 0.03993 | 412.50 | 6.1264 |
| 450 | 0.08953 | 466.82 | 6.4616 | 0.06727 | 466.49 | 6.3750 | 0.04502 | 465.87 | 6.2521 |
| 500 | 0.09953 | 519.84 | 6.5733 | 0.07480 | 519.65 | 6.4870 | 0.05008 | 519.29 | 6.3647 |
| 600 | 0.11948 | 626.92 | 6.7685 | 0.08980 | 626.93 | 6.6825 | 0.06013 | 626.95 | 6.5609 |
| 700 | 0.13937 | 735.94 | 6.9365 | 0.10474 | 736.07 | 6.8507 | 0.07012 | 736.35 | 6.7295 |
| 800 | 0.15923 | 847.22 | 7.0851 | 0.11965 | 847.45 | 6.9994 | 0.08008 | 847.92 | 6.8785 |
| 900 | 0.17906 | 960.83 | 7.2189 | 0.13454 | 961.13 | 7.1333 | 0.09003 | 961.73 | 7.0125 |
| 1000 | 0.19889 | 1076.65 | 7.3409 | 0.14942 | 1077.01 | 7.2553 | 0.09996 | 1077.72 | 7.1347 |


| Temp. K | $\stackrel{\nu}{\mathrm{m}^{3} / \mathrm{kg}}$ | h $\mathrm{k} . \mathrm{I} / \mathrm{kg}$ | $\mathrm{kJ} / \mathrm{kg} \mathrm{~K}$ | $\mathrm{m}^{3} / \mathrm{kg}$ | $\stackrel{h}{\mathrm{~kJ} / \mathrm{kg}}$ | $\stackrel{s}{\mathrm{kal} / \mathrm{kg} \mathrm{~K}}$ | $\mathrm{m}^{\frac{3}{3} / \mathrm{kg}}$ | h $\mathrm{k} / \mathrm{l} / \mathrm{kg}$ | $\mathrm{kJ} / \mathrm{kg}$ K |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 6000 kPa |  |  | 8000 kPa |  |  | 10000 kPa |  |  |
| 140 | 0.002941 | 47.44 | 4.2926 | 0.002224 | 27.78 | 4,1167 | 0.002003 | 20.87 | 4.0373 |
| 160 | 0.005556 | 112.16 | 4.7292 | 0.003748 | 91.80 | 4.5453 | 0.002908 | 76.52 | 4.4088 |
| 180 | 0.007309 | 148.02 | 4.9411 | 0.005193 | 134,69 | 4.7988 | 0.004021 | 122.65 | 4.6813 |
| 200 | 0.008771 | 177.29 | 5.0955 | 0.006387 | 167.47 | 4.9717 | 0.005014 | 158.35 | 4.8697 |
| 220 | 0,010095 | 203.77 | 5.2217 | 0.007449 | 196.07 | 5.1082 | 0.005902 | 188.88 | 5.0153 |
| 240 | 0.011337 | 228.73 | 5.3303 | 0.008433 | 222.48 | 5.2231 | 0.006721 | 216.64 | 5.1362 |
| 260 | 0.012526 | 252.73 | 5.4264 | 0.009367 | 247.55 | 5.3235 | 0.007495 | 242.72 | 5.2406 |
| 280 | 0.013678 | 276.09 | 5.5130 | 0.010264 | 271.74 | 5.4131 | 0.008215 | 267.69 | 5.3331 |
| 300 | 0.014803 | 298.99 | 5.5920 | 0.011135 | 295.32 | 5.4945 | 0.008952 | 291.90 | 5.4167 |
| 350 | 0.017532 | 354.95 | 5.7646 | 0.013236 | 352.51 | 5.6709 | 0.010670 | 350.26 | 5.5967 |
| 400 | 0.020187 | 409.83 | 5.9111 | 0.015264 | 408.24 | 5.8197 | 0.012320 | 406.79 | 5.7477 |
| 450 | 0.022794 | 464.19 | 6.0392 | 0.017248 | 463.22 | 5.9492 | 0.013927 | 462.36 | 5.8786 |
| 500 | 0.025370 | 518.37 | 6.1534 | 0.019202 | 517.88 | 6.0644 | 0.015507 | 517.48 | 5.9948 |
| 600 | 0.030463 | 627.12 | 6.3516 | 0.023053 | 627.32 | 6.2639 | 0.018611 | 627.58 | 6.1955 |
| 700 | 0.035506 | 737.27 | 6.5214 | 0.026856 | 737.94 | 6.4344 | 0.021669 | 738.65 | 6.3667 |
| 800 | 0.040519 | 849.37 | 6.6710 | 0.030631 | 850.38 | 6.5845 | 0.024700 | 851.43 | 6.5172 |
| 900 | 0.045514 | 963.59 | 6.8055 | 0.034388 | 964.86 | 6.7194 | 0.027714 | 966.15 | 6.6523 |
| 1000 | 0.050495 | 1079.88 | 6.9281 | 0.038132 | 1081.35 | 6.8421 | 0.030715 | 1082.84 | 6.7753 |
|  | 15000 kPPa |  |  | 20000 kPa |  |  | 50000 kPa |  |  |
| 140 | 0.001770 | 14.81 | 3.9273 | 0.001655 | 13.75 | 3.8587 | 0.001391 | 28.05 | 3.6405 |
| 160 | 0.002183 | 59.14 | 4.2232 | 0.001929 | 53.63 | 4.1250 | 0.001497 | 61.62 | 3.8647 |
| 180 | 0.002749 | 102.34 | 4.4778 | 0.002281 | 93.02 | 4.3570 | 0.001612 | 94.31 | 4.0573 |
| 200 | 0.003365 | 140.60 | 4.6796 | 0.002687 | 130.17 | 4.5529 | 0.001736 | 126.15 | 4.2250 |
| 220 | 0.003964 | 174.10 | 4.8394 | 0.003108 | 164.26 | 4.7154 | 0,001867 | 157.12 | 4.3726 |
| 240 | 0.004531 | 204.33 | 4.9710 | 0.003525 | 195.59 | 4.8518 | 0.002003 | 187.24 | 4.5037 |
| 260 | 0.005071 | 232.41 | 5.0834 | 0.003930 | 224.82 | 4.9689 | 0.002143 | 216.53 | 4.6209 |
| 280 | 0.005589 | 259.01 | 5,1820 | 0.004323 | 252.50 | 5.0714 | 0.002285 | 245.02 | 4.7266 |
| 300 | 0.006088 | 284,56 | 5.2702 | 0.004704 | 279.01 | 5.1629 | 0.002428 | 272.78 | 4.8223 |
| 350 | 0.007280 | 345.47 | 5.4581 | 0.005617 | 341.86 | 53568 | 0.002786 | 339.44 | 5.0280 |
| 400 | 0.008416 | 403.79 | 5.6139 | 0.006487 | 401.65 | 5.5166 | 0.003138 | 403.08 | 5.1980 |
| 450 | 0.009517 | 460.71 | 5.7480 | 0.007329 | 459.70 | 5.6534 | 0.003484 | 464.64 | 5.3431 |
| 500 | 0.010593 | 516.88 | 5.8664 | 0.008149 | 516.78 | 5.7737 | 0.003823 | 524.82 | 5.4699 |
| 600 | 0.012697 | 628,50 | 6,0699 | 0.009748 | 629.76 | 5.9797 | 0.004484 | 642.94 | 5.6853 |
| 700 | 0.014759 | 740.63 | 6.2427 | 0.011310 | 742.85 | 6.1540 | 0.005129 | 760.04 | 5.8658 |
| 800 | 0.016797 | 854.18 | 6.3943 | 0.012849 | 857.11 | 6.3065 | 0.005762 | 877.47 | 6.0226 |
| 900 | 0.018818 | 969.50 | 6.5301 | 0.014374 | 972.98 | 6.4430 | 0.006385 | 995.87 | 6.1621 |
| 1000 | 0.020828 | 1086.64 | 6.6535 | 0.015887 | 1090.55 | 6.5668 | 0.007001 | 1115.51 | 6.2881 |

## Signals and Systems 1:

Please do problems 1.21, 1.22, 1.25, and 1.26 from Oppenheim and Willsky.


[^0]:    Announcements:

