

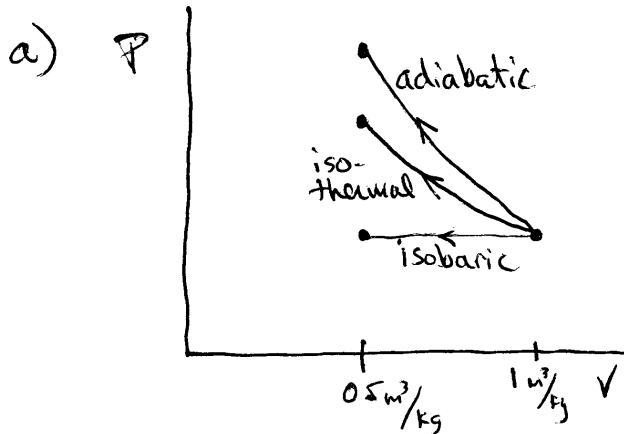


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Unified Engineering
Fall 2004

Problem Set #7
Solutions

SOLUTIONS TO T4 BY WAITZ



b) INITIAL CONDITIONS

$$v_1 = 1 \text{ m}^3/\text{kg}, \quad P_1 = 100 \text{ kPa} \quad \therefore T_1 = 348.4 \text{ K}$$

by ideal gas law

1) isobaric $P = \text{const.}$ $P_1 = P_2 = 100 \text{ kPa}$
 $v_2 = 0.5 \text{ m}^3/\text{kg}$

$$\therefore \boxed{T_2 = 174.2 \text{ K}} \text{ by ideal gas law}$$

2) isothermal $T = \text{const}$ $T_1 = T_2 = 348.4 \text{ K}$

$$v_2 = 0.5 \text{ m}^3/\text{kg}$$

$$\therefore \boxed{P_2 = 200 \text{ kPa}} \text{ by ideal gas law}$$

3) γ-s adiabatic $Pv^\gamma = \text{const}$ $\gamma = 1.4$

$$\frac{T_2}{T_1} = \left(\frac{v_1}{v_2}\right)^{\gamma-1} = (2)^{0.4} = 1.32 \Rightarrow \boxed{T_2 = 459.7 \text{ K}}$$

$$\frac{P_2}{P_1} = \left(\frac{T_2}{T_1}\right)^{\gamma/\gamma-1} = 2.64 \quad \therefore \boxed{P_2 = 264 \text{ kPa}}$$

c) FOR EACH PROCESS CALCULATE WORK DONE BY SYSTEM &
HEAT ADDED TO SYSTEM

1) ISOBARIC

$$w = p \Delta v$$

$$w = 100 \text{ kPa} (0.5 \text{ m}^3/\text{kg} - 1.0 \text{ m}^3/\text{kg}) = ?$$

$$w = -50 \text{ kJ/kg} \quad (\text{compression})$$

$$\text{1st Law: } \Delta u = q - w$$

$$\therefore q = \Delta u + w = C_v (T_2 - T_1) + w$$

$$= 716.5 (174.2 - 348.4) + (-50,000)$$

$$= -175 \text{ kJ/kg} \quad (\text{heat removal})$$

2) ISOTHERMAL

$$w = RT \ln \left(\frac{v_2}{v_1} \right) = 287 \cdot 348.4 \ln(0.5)$$

$$w = -69 \text{ kJ/kg} \quad (\text{compression})$$

$$\text{1st LAW} \quad \Delta u = q - w \quad \Delta u = C_v \Delta T = 0$$

$$\text{so } q = w$$

$$q = -69 \text{ kJ/kg} \quad (\text{heat removal})$$

3) ADABATIC

$$\Delta u = q - w \quad q = 0$$

$$\therefore w = -\Delta u = -C_v (T_2 - T_1) = 716.5 (459.7 - 348)$$

$$w = -80 \text{ kJ/kg} \quad (\text{compression})$$

d) ENTHALPY CHANGE FOR EACH PROCESS

$$\Delta h = C_p \Delta T = \Delta [u + pV] = \Delta [C_v T + pV]$$

* CAN CALC. EITHER WAY
BUT $C_p \Delta T$ IS EASIER

1) ISOBARIC

$$\Delta h = 1003.5 (174.2 - 348.4) = \boxed{-180 \text{ kJ/kg}}$$

2) ISOTHERMAL

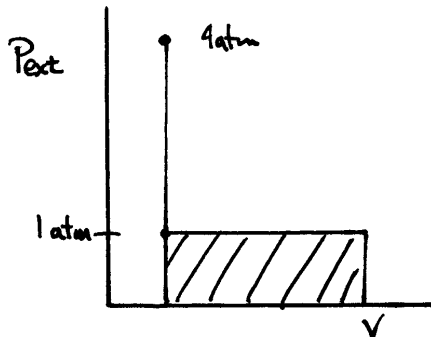
$$\boxed{\Delta h = 0}$$

3) ADIABATIC

$$\Delta h = 1003.5 (459.7 - 348.4) = \boxed{112 \text{ kJ/kg}}$$

SOLUTIONS TO T5 BY WAITZ

a) All weights removed instantaneously



$$P_{\text{initial}} = 4 \text{ atm}, T_i = 300 \text{ K}$$

$$V_i = \frac{287 \cdot 300}{405.3 \text{ kPa}} = 0.21 \text{ m}^3/\text{kg}$$

WE KNOW $P_{\text{final}} = 1 \text{ atm}$ BUT
WE DO NOT KNOW T_f OR V_f .

* NOTE THAT WE EXPECT $T_f < T_i$
SINCE IT IS A THERMALLY-INSULATED
(ADIABATIC) CYLINDER AND WE
ARE GETTING WORK OUT SO
 ΔU SHOULD BE NEGATIVE.

CONSIDER 1st LAW FOR ADIABATIC PROCESS:

$$\Delta u = \overset{+}{\cancel{q}} - w \quad \text{so} \quad C_v \Delta T = -P_{\text{ext}} \Delta V$$

$$C_v (T_f - T_i) = -P_{\text{ext}} (V_f - V_i)$$

$$\text{ideal gas: } P_f V_f = RT_f$$

} 2 eqns
2 unknowns
(V_f & T_f)

$$\text{LET } V_f = \frac{RT_f}{P_f} \quad C_v (T_f - T_i) = -P_{\text{ext}} \left(\frac{RT_f}{P_f} - V_i \right)$$

AT THE FINAL STATE $P_f = P_{\text{ext}}$ (it comes to thermodynamic equilibrium)
SO $C_v T_f - C_v T_i = -RT_f + P_{\text{ext}} V_i$

$$(C_v + R)T_f = P_{\text{ext}} V_i + C_v T_i$$

$$\boxed{T_f = \frac{P_{\text{ext}} V_i + C_v T_i}{C_v + R}} *$$

PLUG IN SOME NUMBERS

$$T_f = \frac{(101325)(0.21) + (716.5)(300)}{716.5 + 287} = 235.4 \text{ K}$$

$$P_f = P_{\text{ext}} = 101325 \text{ N/m}^2$$

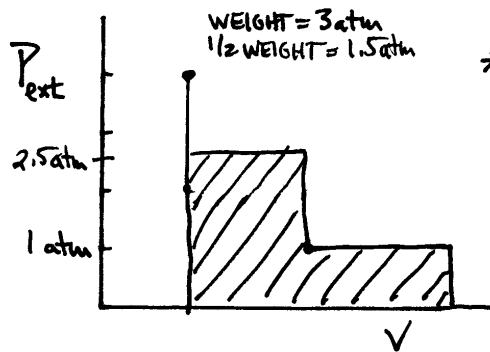
$$PV = RT \Rightarrow V_f = 0.67 \text{ m}^3/\text{kg}$$

$$\Delta u = -w$$

$$w = -C_v(235.4 - 300) = +46.3 \text{ kJ/kg}$$

work by system

b) Two step process (expect more work out of system!)



* Define subscript "m" as middle condition (1/2 weight removed)
USE SAME EQUATIONS

$$T_m = \frac{P_{\text{ext}} v_i + C_v T_i}{C_v + R} = \frac{253312 \cdot 0.21 + 716.5 \cdot 300}{716.5 + 287}$$

$$= 267.2 \text{ K}$$

$$P_m = 253312 \text{ N/m}^2$$

$$V_m = 0.30 \text{ m}^3/\text{kg}$$

$$W_{\text{①}} = 23.5 \text{ kJ/kg}$$

$$T_f = \frac{P_{\text{ext}} V_m + C_v T_m}{C_v + R} = \frac{101325 \cdot 0.30 + 716.5 \cdot 267.2}{716.5 + 287}$$

$$T_f = 221 \text{ K}, \quad p_f = 101325 \text{ Pa}, \quad v_f = 0.63 \text{ m}^3/\text{kg}$$

$$w_{\text{ext}} = -716.5 (221 - 267.2) = 33.1 \text{ kJ/kg}$$

$$w_{\text{total}} = w_{\text{int}} + w_{\text{ext}} = 56.6 \text{ kJ/kg}$$

c) (Quasi-static process (expect the most work)
adiabatic

$$p v^\gamma = \text{const.} \quad \frac{T_f}{T_i} = \left(\frac{p_f}{p_i} \right)^{\gamma-1/\gamma} = \left(\frac{1}{4} \right)^{0.4/1.4}$$

$$\therefore T_f = 202 \text{ K} \quad = 0.673$$

$$p_f = 101325 \text{ Pa}$$

$$v_f = 0.572 \text{ m}^3/\text{kg}$$

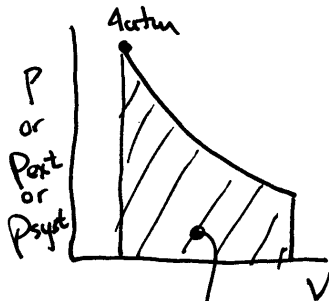
$$\Delta u = \int \delta q - w \quad C_v \Delta T = -w$$

$$w = -716.5 (202 - 300) = 70.2 \text{ kJ/kg}$$

MESSAGES: (1) THE AMOUNT OF WORK EXTRACTED DEPENDS ON PATH

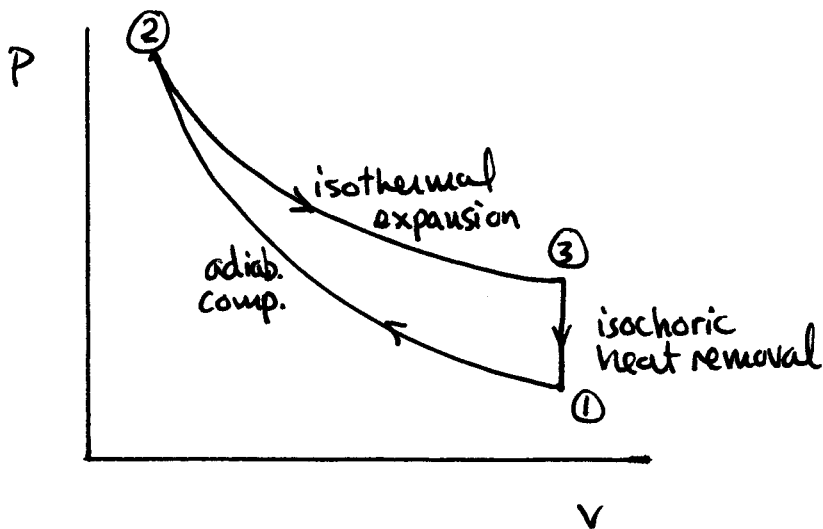
(2) IN CALCULATING WORK FOR NON-QUASI-STATIC PROCESSES, NEED TO USE point.

(3) THE CLOSER WE APPROACH A QUASI-STATIC PROCESS, THE MORE WORK WE GET OUT OF THE SYSTEM. THEREFORE IN DESIGNING AN ENGINE WE WANT TO LIMIT NON-QUASI-STATIC PROCESSES TO EVERY EXTENT POSSIBLE.



we get the most area under the curve

SOLUTIONS TO T5 BY WAITZ



a) LEG ①-②: ADIABATIC COMPRESSION $Q=0$ $W \neq 0$ (-)

LEG ②-③: ISOTHERMAL EXPANSION

$$\Delta U = Q - W \quad \text{SO } Q = W \quad W \Rightarrow (+)$$

$$\therefore Q \Rightarrow (+)$$

LEG ③-①: CONSTANT VOLUME
HEAT EXTRACTION

$$W=0, \quad Q \Rightarrow (-)$$

b) LEG ①-②

$$\Delta u = Q - W \quad C_v \Delta T = \Delta u = -W$$

$$\frac{T_2}{T_1} = \left(\frac{V_1}{V_2}\right)^{\gamma-1} = (8)^{0.4} = 2.3$$

$$T_1 = 300\text{K} \quad \text{so } T_2 = 690\text{K}$$

$$\left[\begin{array}{l} \Delta u = 716.5(690-300) = 280 \text{ kJ/kg} \\ W = -280 \text{ kJ/kg} \\ Q = 0 \\ \Delta h = C_p \Delta T = 391 \text{ kJ/kg} \end{array} \right.$$

LEG ②-③ ISOTHERMAL $\Delta u = q - w$

$$q = w$$

$$w = RT \ln\left(\frac{v_2}{v_1}\right) = 287(690) \ln(8)$$

$$\left[\begin{array}{l} w = 412 \text{ kJ/kg} \\ \Delta u = 0 \\ \Delta h = 0 \\ q = 412 \text{ kJ/kg} \end{array} \right.$$

LEG ③-① CONST. VOLUME

$$\left[\begin{array}{l} w = 0 \quad \Delta u = q \quad C_v \Delta T = q \\ q = 716.5(300 - 690) = - \text{ kJ/kg} \\ \Delta h = C_p \Delta T = 1003.5(300 - 690) = -391 \text{ kJ/kg} \end{array} \right.$$

c) NET WORK

$$W_{\text{cycle}} = W_{1-2} + W_{2-3} + W_{3-1}$$

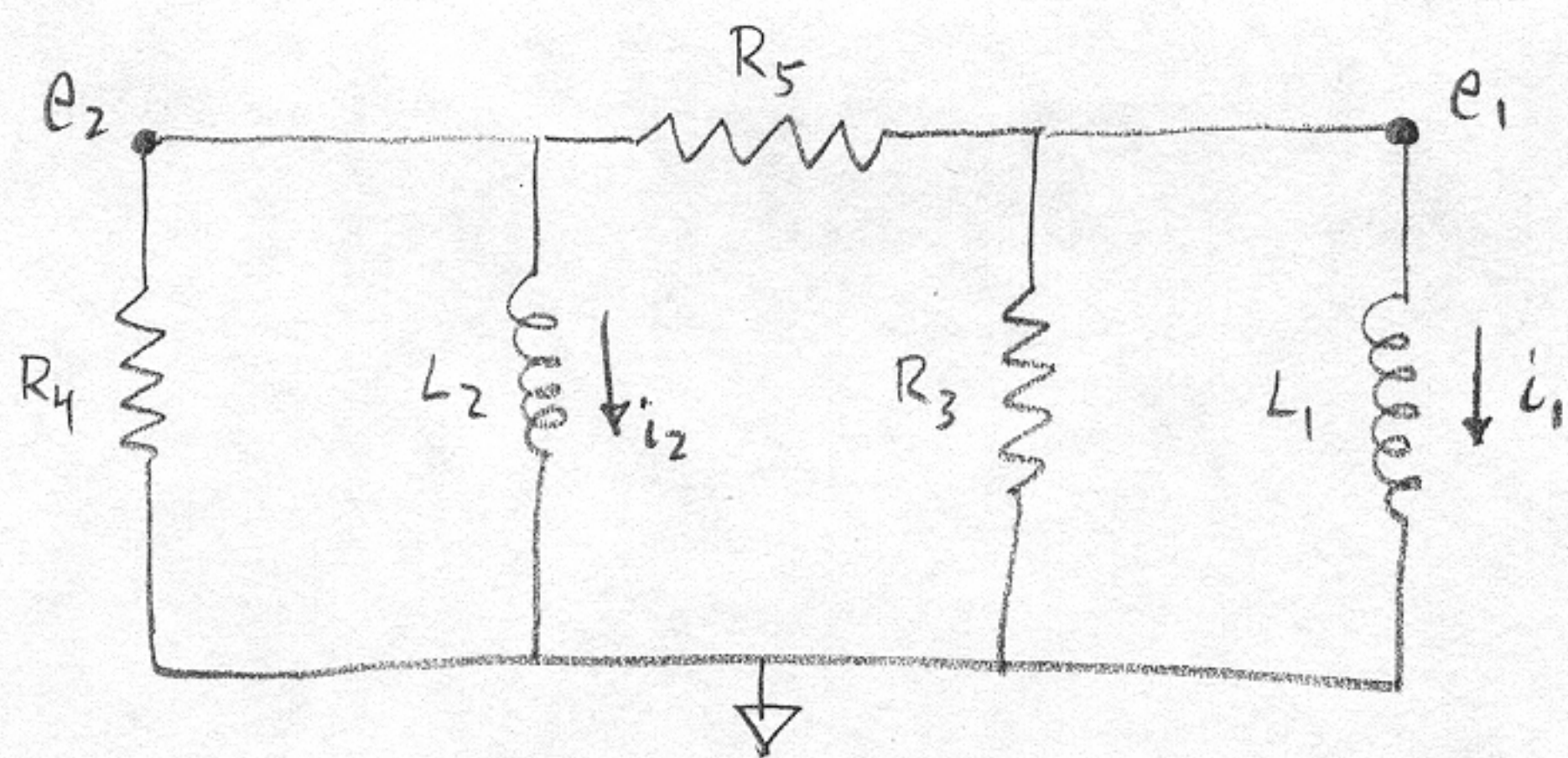
$$= -280 + 412 + 0 = 132 \text{ kJ/kg}$$

✓ [NOTE FOR CYCLE, $W_{\text{cycle}} = q_{\text{cycle}} = q_{1-2} + q_{2-3} + q_{3-1}$]

$$\begin{aligned} &= 0 + 412 - 280 \\ &= 132 \text{ kJ/kg} \end{aligned}$$

d) THERMAL EFFICIENCY = $\frac{\text{WHAT YOU GET}}{\text{WHAT YOU PAY FOR}} = \frac{\text{NET WORK}}{\text{HEAT IN}}$

$$\eta_{\text{TH}} = \frac{132 \text{ kJ/kg}}{412 \text{ kJ/kg}} = 32\%$$



$$\begin{aligned} L_1 &= 1 \text{ H} \\ L_2 &= 1 \text{ H} \\ R_3 &= 1 \Omega \\ R_4 &= 1 \Omega \\ R_5 &= \frac{1}{2} \Omega \end{aligned}$$

APPLY NODE METHOD AT e_1 & e_2 :

$$e_1: i_1 + (G_3 + G_5)e_1 - G_5e_2 = 0$$

$$e_2: i_2 - G_5e_1 + (G_4 + G_5)e_2 = 0$$

ASSUME EXPONENTIAL SOLUTIONS & WRITE i_1 & i_2 IN TERMS OF IMPEDANCES:

$$\frac{1}{L_1 s} E_1 + (G_3 + G_5)E_1 - G_5E_2 = 0$$

$$\frac{1}{L_2 s} E_2 - G_5E_1 + (G_4 + G_5)E_2 = 0$$

PLUG IN VALUES AND WRITE IN FORM $M(s)\underline{E} = \underline{0}$

$$\begin{bmatrix} 3 + \frac{1}{s} & -2 \\ -2 & 3 + \frac{1}{s} \end{bmatrix} \begin{bmatrix} E_1 \\ E_2 \end{bmatrix} = \underline{0}$$

SOLVE FOR CHARACTERISTIC VALUES USING $\det(M(s))$

$$\left(3 + \frac{1}{s}\right)\left(3 + \frac{1}{s}\right) - 4 = 0$$

$$9 + \frac{6}{s} + \frac{1}{s^2} - 4 = 0$$

$$5s^2 + 6s + 1 = 0$$

$$\therefore s = -1 \text{ and } -\frac{1}{5}$$

FIND CHARACTERISTIC VECTOR \underline{E} FOR EACH CHARACTERISTIC VALUE

$$s_1 = -1 \quad M(-1) = \begin{bmatrix} 2 & -2 \\ -2 & 2 \end{bmatrix}$$

$$M(s)\underline{E} = \underline{0} \Rightarrow \underline{E} = \begin{bmatrix} 1 \\ 1 \end{bmatrix}$$

$$s_2 = -\frac{1}{5} \quad M\left(-\frac{1}{5}\right) = \begin{bmatrix} -2 & -2 \\ -2 & -2 \end{bmatrix}$$

$$M(s)\underline{E} = \underline{0} \Rightarrow \underline{E} = \begin{bmatrix} 1 \\ -1 \end{bmatrix}$$

$$\text{so } e(t) = a \begin{bmatrix} 1 \\ 1 \end{bmatrix} e^{-t} + b \begin{bmatrix} 1 \\ -1 \end{bmatrix} e^{-\frac{1}{5}t}$$

NOW USE CONSTITUTIVE LAW FOR INDUCTOR TO FIND $i_1(t)$ & $i_2(t)$

$$v(t) = L \frac{di(t)}{dt}$$

$$i(t) = \frac{1}{L} \int v(t) dt$$

SINCE L_1 & $L_2 = 1 \text{ H}$,

$$i_1(t) = -ae^{-t} - 5be^{-\frac{1}{5}t}$$

$$i_2(t) = -ae^{-t} + 5be^{-\frac{1}{5}t}$$

USE INITIAL CONDITIONS TO SOLVE FOR a & b

$$i_1(0) = 10 \text{ A} \quad i_2(0) = 0 \text{ A}$$

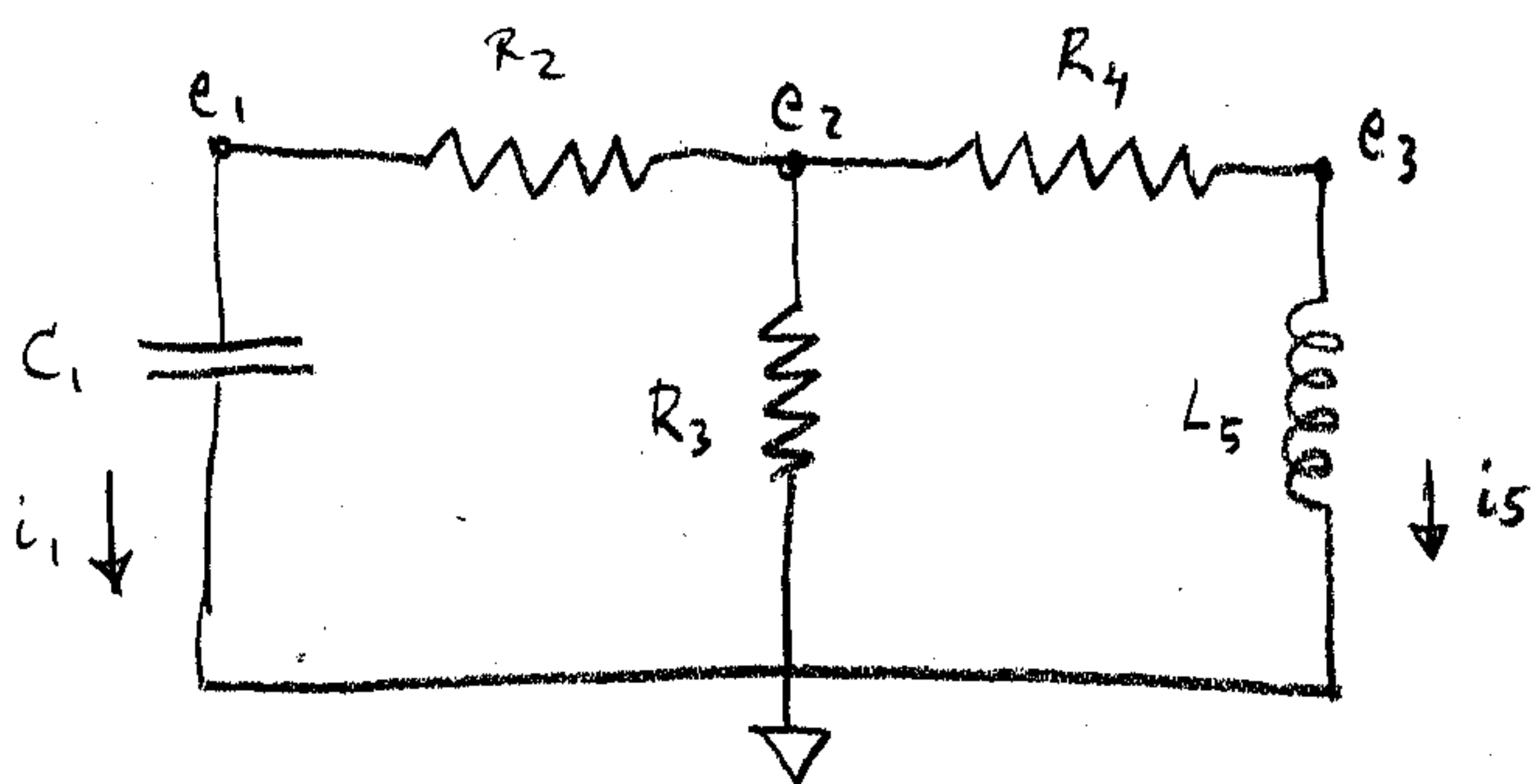
$$10 = -a - 5b \quad 0 = -a + 5b$$

$$10 = -5b - 5b \quad a = 5b$$

$$10 = -10b$$

$$\boxed{b = -1} \quad \longrightarrow \quad \boxed{a = -5}$$

$$\therefore \boxed{\begin{aligned} i_1(t) &= 5e^{-t} + 5e^{-\frac{1}{5}t} \\ i_2(t) &= 5e^{-t} - 5e^{-\frac{1}{5}t} \end{aligned}}$$



$$C_1 = \frac{1}{4} \text{ F}$$

$$R_2 = 4 \Omega$$

$$R_3 = 4 \Omega$$

$$R_4 = 1 \Omega$$

$$L_5 = 1 \text{ H}$$

APPLY NODE METHOD AT $e_1, e_2, \& e_3$. ASSUME EXPONENTIAL SOLUTIONS AND WRITE i_1 & i_5 IN TERMS OF IMPEDANCES TO OBTAIN THE FOLLOWING:

$$\begin{bmatrix} C_1 s + G_2 & -G_2 & 0 \\ -G_2 & G_2 + G_3 + G_4 & -G_4 \\ 0 & -G_4 & G_4 + \frac{1}{L_5 s} \end{bmatrix} \begin{bmatrix} E_1 \\ E_2 \\ E_3 \end{bmatrix} = \underline{0}$$

PLUG IN COMPONENT VALUES.

$$\begin{bmatrix} \frac{1}{4}s + \frac{1}{4} & -\frac{1}{4} & 0 \\ -\frac{1}{4} & \frac{3}{2} & -1 \\ 0 & -1 & \frac{1}{s} + 1 \end{bmatrix} \underline{E} = \underline{0}$$

SOLVE FOR CHARACTERISTIC VALUES USING $\det(M(s)) = 0$

$$\left(\frac{1}{4}s + \frac{1}{4}\right) \left[\frac{3}{2} \left(\frac{1}{s} + 1\right) - 1\right] + \frac{1}{4} \left[-\frac{1}{4} \left(\frac{1}{s} + 1\right)\right] = 0$$

$$2s^2 + 7s + 5 = 0$$

$$\therefore s = -1 \text{ AND } -2.5$$

FIND CHARACTERISTIC VECTOR \underline{E} FOR EACH CHARACTERISTIC VALUE THAT SATISFIES $M(s)\underline{E} = \underline{0}$

$$\underline{s_1} = -1 \quad M(-1) = \begin{bmatrix} 0 & \frac{1}{4} & 0 \\ \frac{1}{4} & \frac{3}{2} & -1 \\ 0 & -1 & 0 \end{bmatrix} \quad \therefore \underline{E}_1 = \begin{bmatrix} 1 \\ \frac{1}{4} \\ 0 \end{bmatrix}$$

$$\underline{s_2} = -2.5 \quad M(-2.5) = \begin{bmatrix} -\frac{3}{8} & \frac{1}{4} & 0 \\ \frac{1}{4} & \frac{3}{2} & -1 \\ 0 & -1 & \frac{3}{4} \end{bmatrix} \quad \therefore \underline{E}_2 = \begin{bmatrix} 1 \\ \frac{3}{2} \\ \frac{3}{4} \end{bmatrix}$$

$$\text{So } \underline{e}(t) = a \begin{bmatrix} 1 \\ 0 \\ \frac{1}{4} \end{bmatrix} e^{-t} + b \begin{bmatrix} 1 \\ \frac{3}{2} \\ \frac{3}{4} \end{bmatrix} e^{-2.5t}$$

LOOKING AT CIRCUIT, $v_1(t) = e_1(t) - 0 = e_1(t)$

$$\text{AND } v_5(t) = L_5 \frac{di_5(t)}{dt} \Rightarrow i_5(t) = \frac{1}{L_5} \int v_5(t) dt = \frac{1}{L_5} \int e_3(t) dt$$

$$\therefore v_1(t) = a e^{-t} + b e^{-2.5t}$$

$$i_5(t) = \frac{a}{4} e^{-t} + b e^{-2.5t}$$

USE INITIAL CONDITIONS TO SOLVE FOR a & b :

$$v_1(0) = 2V = a + b \quad i_5(0) = 1A = \frac{a}{4} + b$$

$$2 = a + (1 - \frac{a}{4}) \quad \leftarrow b = 1 - \frac{a}{4}$$

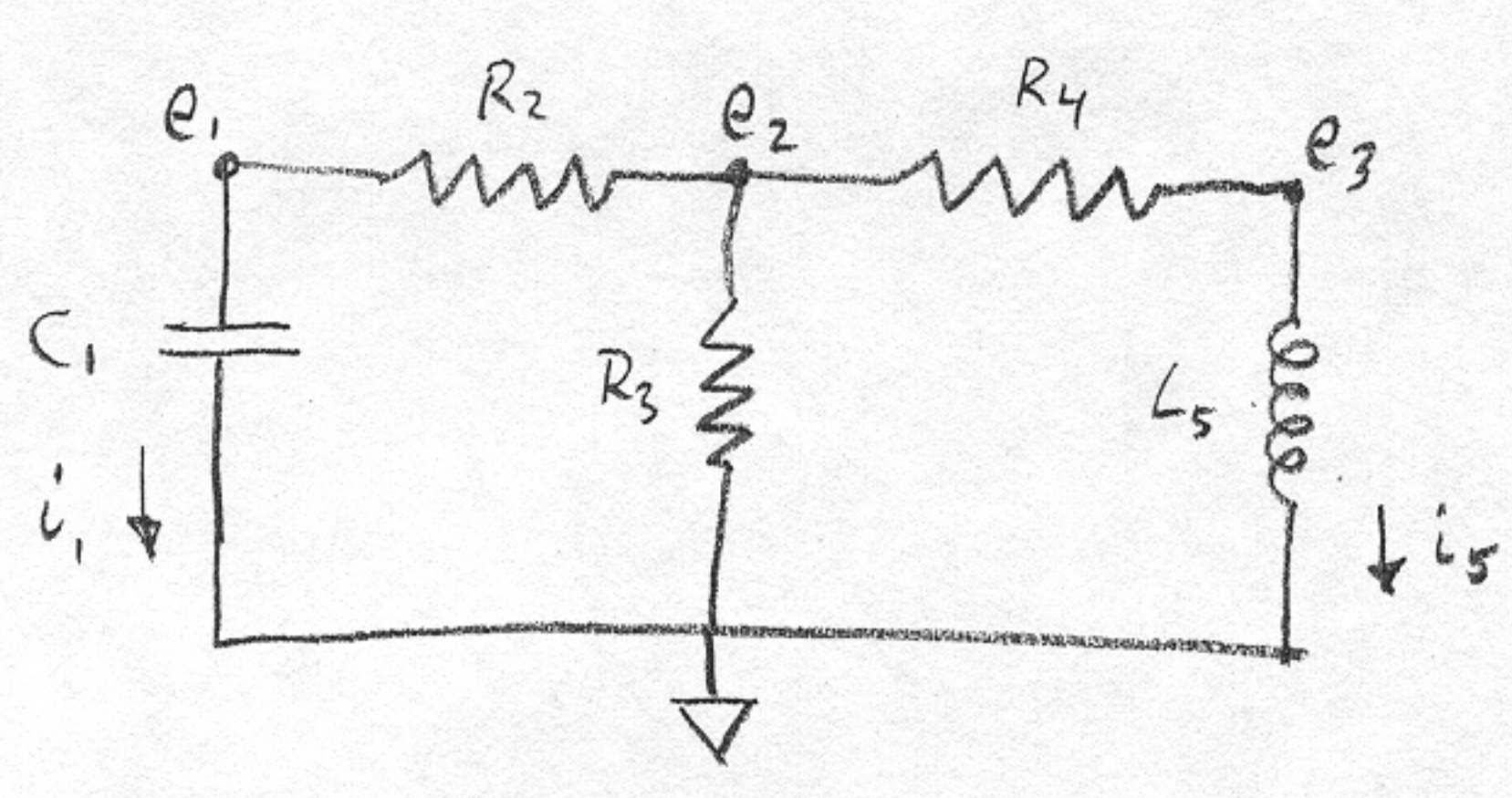
$$1 = \frac{3}{4}a$$

$$a = \frac{4}{3} \quad \rightarrow \quad b = 1 - \frac{4}{3 \cdot 4} = \frac{2}{3}$$

$$\therefore v_1(t) = \frac{4}{3} e^{-t} + \frac{2}{3} e^{-2.5t}$$

$$i_5(t) = \frac{1}{3} e^{-t} + \frac{2}{3} e^{-2.5t}$$

UNIFIED ENGINEERING PROBLEM S12 SOLUTIONS FALL 2004



- $C_1 = \frac{1}{4} F$
- $R_2 = 4 \Omega$
- $R_3 = 4 \Omega$
- $R_4 = 1 \Omega$
- $R_5 = 1 H$

STATES CORRESPOND TO ENERGY STORAGE UNITS IN CIRCUIT

SO STATES ARE $x_1 = v_1$
 $x_2 = i_5$

USING CONSTITUTIVE RELATIONS FOR INDUCTOR & CAPACITOR,

$$\dot{x}_1 = \frac{dv_1}{dt} = \frac{i_1}{C_1} \Rightarrow f(v_1, i_5)$$

$$\dot{x}_2 = \frac{di_5}{dt} = \frac{v_5}{L_5} \Rightarrow f(v_1, i_5)$$

WANT STATE DERIVATIVES IN TERMS OF STATE VARIABLES

APPLY NODE METHOD AT $e_1, e_2,$ & e_3 :

$$e_1: i_1 + G_2 e_1 - G_2 e_2 = 0$$

$$e_2: -G_2 e_1 + (G_2 + G_3 + G_4) e_2 - G_4 e_3 = 0$$

$$e_3: i_5 - G_4 e_2 + G_4 e_3 = 0$$

PLUG IN VALUES AND LET $e_1 = v_1$ & $e_3 = v_5$

$$\left. \begin{aligned} i_1 + \frac{1}{4} v_1 - \frac{1}{4} e_2 &= 0 \\ -\frac{1}{4} v_1 + \frac{3}{2} e_2 - v_5 &= 0 \\ i_5 - e_2 + v_5 &= 0 \end{aligned} \right\} \begin{aligned} &\text{TREAT STATES } v_1 \text{ \& } i_5 \text{ AS CONSTANT} \\ &3 \text{ EQUATIONS, } 3 \text{ UNKNOWNNS } (e_2, i_1, v_5) \end{aligned}$$

SOLVING FOR i_1 & v_5 IN ORDER TO FIND \dot{x} FROM ABOVE:

$$i_1 = -\frac{1}{8} v_1 - \frac{1}{2} i_5$$

$$v_5 = \frac{1}{2} v_1 - 3 i_5$$

SINCE $\dot{x}_1 = \frac{i_1}{C_1}$ & $\dot{x}_2 = \frac{v_5}{L_5}$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -\frac{1}{2} & -2 \\ \frac{1}{2} & -3 \end{bmatrix} \begin{bmatrix} v_1 \\ i_5 \end{bmatrix}$$

$\dot{x} \quad A \quad x$

FIND $\det(sI-A)$ TO SOLVE FOR EIGENVALUES OF MATRIX A

$$[sI-A] = \begin{bmatrix} s+\frac{1}{2} & 2 \\ -\frac{1}{2} & s+3 \end{bmatrix}$$

$$\det [sI-A] = (s+\frac{1}{2})(s+3)+1 = 0$$

$$s^2 + \frac{7}{2}s + \frac{5}{2} = 0 \quad \therefore \boxed{s = -1 \text{ AND } -2.5} \rightarrow \text{EIGENVALUES}$$

SO NON-TRIVIAL SOLUTION \underline{v} TO THE EQUATION

$$[sI-A] \underline{v} = 0$$

IS THE EIGENVECTOR

$$s_1 = -1 \quad [sI-A] \underline{v} = 0$$

$$\begin{bmatrix} -\frac{1}{2} & 2 \\ -\frac{1}{2} & 2 \end{bmatrix} \underline{v} = 0 \Rightarrow \underline{v}_1 = \begin{bmatrix} 4 \\ 1 \end{bmatrix}$$

$$s_2 = -2.5 \quad \begin{bmatrix} -2 & 2 \\ -\frac{1}{2} & -\frac{1}{2} \end{bmatrix} \underline{v} = 0 \Rightarrow \underline{v}_2 = \begin{bmatrix} 1 \\ 1 \end{bmatrix}$$

$$\therefore \underline{x} = a \begin{bmatrix} 4 \\ 1 \end{bmatrix} e^{-t} + b \begin{bmatrix} 1 \\ 1 \end{bmatrix} e^{-2.5t}$$

USE INITIAL CONDITIONS TO SOLVE FOR a & b

$$v_1(0) = x_1(0) = 2v = 4a + b \quad i_s(0) = x_2(0) = 1A = a + b$$

$$2 = 4a + (1-a) \quad \leftarrow \quad b = 1-a$$

$$1 = 3a$$

$$a = \frac{1}{3}$$

$$b = 1 - \frac{1}{3}$$

$$b = \frac{2}{3}$$

$$\therefore \boxed{\begin{bmatrix} v_1(t) \\ i_s(t) \end{bmatrix} = \underline{x} = \frac{1}{3} \begin{bmatrix} 4 \\ 1 \end{bmatrix} e^{-t} + \frac{2}{3} \begin{bmatrix} 1 \\ 1 \end{bmatrix} e^{-2.5t}}$$