

1. (35 %) If we ignore the variation of wind speed with altitude, wind distribution in a hurricane is in effect a 2D velocity field. The wind speeds of a hurricane vary with radius  $r$  from the center roughly as sketched. In the “eye” of the hurricane, the velocity very nearly has the simple form

$$V_\theta = C_0 r \quad V_r = 0$$

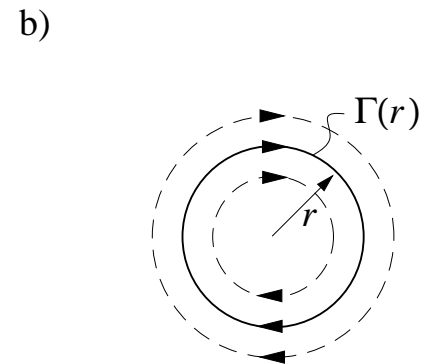
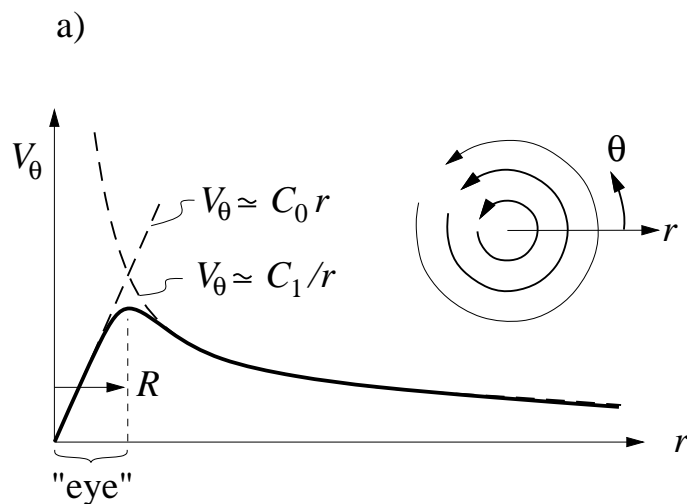
while outside the eye, the velocity nearly has the form

$$V_\theta = C_1/r \quad V_r = 0.$$

Typical constants for a medium-size hurricane are

$$C_0 = 1 \text{ (m/s)/km} \quad C_1 = 2500 \text{ (m/s)km}$$

- Estimate the radius  $R$  of the eye.
- Consider a circular circuit of radius  $r$  around the center of hurricane. Determine and sketch the circulation  $\Gamma(r)$  versus the circuit radius over the entire hurricane. Be sure to specify the units.
- Determine and sketch the vorticity versus radius  $\xi(r)$  over the entire hurricane (i.e. inside and outside the eye). Be sure to specify the units.



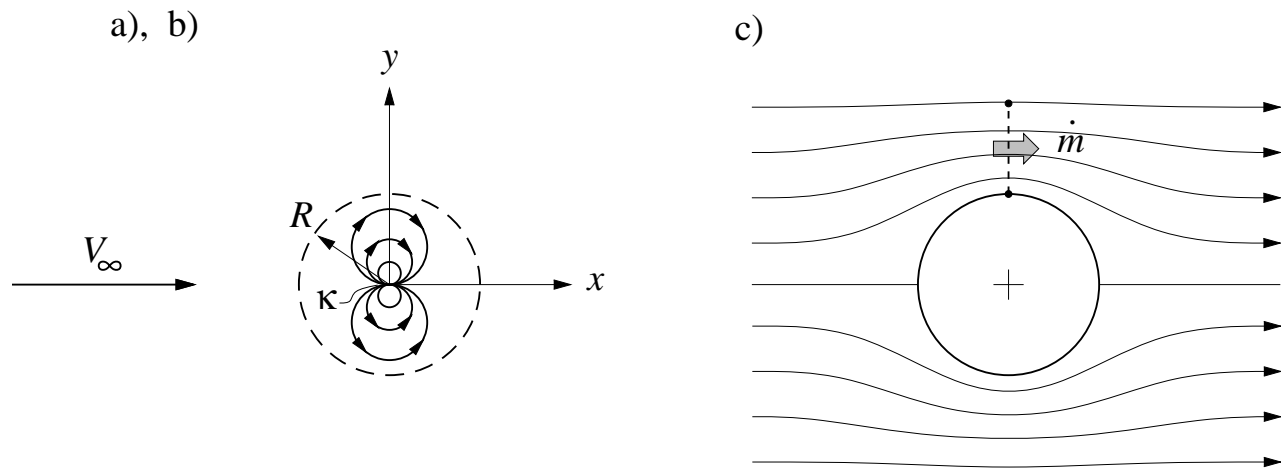
2. (40 %) A potential flow consists of a superposition of a uniform flow and doublet.

$$\phi = V_{\infty} r \cos \theta + \frac{\kappa \cos \theta}{2\pi r}$$

a) Determine the doublet strength  $\kappa$  required to make this be the potential flow about a circular cylinder of radius  $R$ .

b) Show that with the  $\kappa$  value from a), the surface of the cylinder is a streamline.

c) Determine the mass flow rate  $\dot{m}$  through the vertical line connecting the points  $(x, y) = (0, R)$  and  $(0, 2R)$ . Your result will be in terms of  $V_{\infty}$ ,  $R$ , and some constant density  $\rho$ .

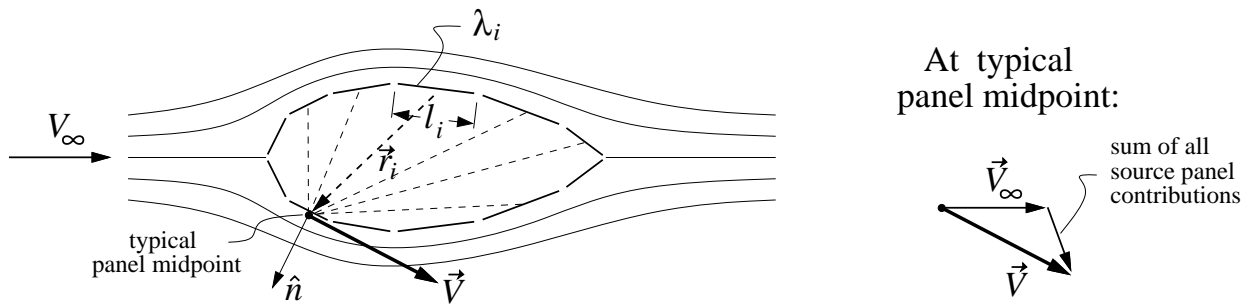


3. (25 %) The flow around a nonlifting body is represented in a panel method by a superposition of  $N$  source panels and a uniform freestream.

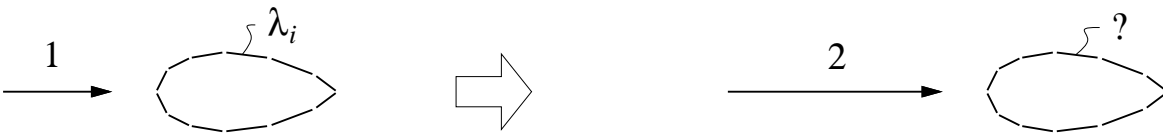
$$\vec{V}(x, y) = \vec{V}_\infty + \sum_{i=1}^N \lambda_i \int_0^{\ell_i} \frac{\vec{r}_i}{2\pi r_i^2} ds$$

The  $i$ 'th panel has a length  $\ell_i$ , and a constant strength  $\lambda_i$ . All the  $\lambda_i$  are determined by the panel method program so as to obtain flow tangency on each panel midpoint, as shown in the Figure below.

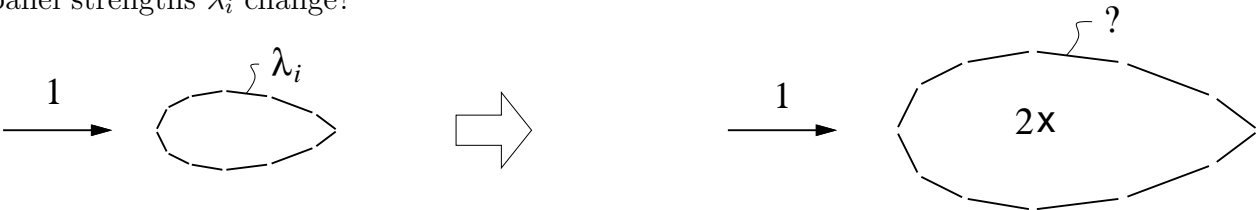
$$\vec{V} \cdot \hat{n} = 0 \quad \text{on all panel midpoints}$$



a) The freestream speed is now doubled, from  $V_\infty = 1$  to  $V_\infty = 2$ , and the panel method is run again. By how much will all the panel strengths  $\lambda_i$  change?



b) The freestream speed is set back to  $V_\infty = 1$ , but the body and all the panels are doubled in size, keeping the shape the same. The panel method is then run again. How will all the panel strengths  $\lambda_i$  change?



Hint: For each case, consider what must or must not happen to the direction of each  $\vec{V}(x, y)$  vector at the panel midpoints when  $V_\infty$  or the geometry size is changed.