

1)

a) $V_\theta = \frac{C}{r}$, $V_r = 0$ is an irrotational, incompressible flow. From table: $V_\theta = -\frac{\Gamma}{2\pi r}$
 so for this case, $C = -\frac{\Gamma}{2\pi}$. Also from table for this flow: $\psi = \frac{\Gamma}{2\pi} \ln r = -C \ln r$

Alternatively, can obtain $\psi(r, \theta)$ from $\frac{\partial \psi}{\partial r} = -V_\theta = -\frac{C}{r} \Rightarrow \psi = -C \ln r + f(\theta)$ (10)
 $\frac{1}{r} \frac{\partial \psi}{\partial \theta} = V_r = 0 \Rightarrow \psi = \text{const}$ equal, set to 0 arbitrarily

b) $\dot{V}' = \int \vec{V} \cdot \hat{n} dA = \int_{R_1}^{R_2} V_\theta dr = \int_{R_1}^{R_2} \frac{C}{r} dr = C (\ln R_2 - \ln R_1) = C \ln \left(\frac{R_2}{R_1} \right)$ (10)

Alternatively; use streamfunction: $\dot{V}' = \psi_1 - \psi_2 = C (\ln R_2 - \ln R_1)$ same result

c) This is an irrotational flow (it's on the table), so $\xi = 0$ (10) constant

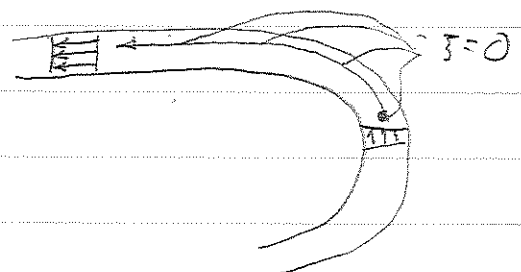
Alternatively, can compute directly: $\xi = \nabla \times \vec{V} = \frac{1}{r} \frac{\partial}{\partial r} (r V_\theta) - \frac{1}{r} \frac{\partial V_r}{\partial \theta} = \frac{1}{r} \frac{\partial}{\partial r} \left(r \cdot \frac{C}{r} \right) = 0$

d) Helmholtz Equation: $\frac{D\xi}{Dt} = 0$, or $\xi = \text{constant}$ along streamlines.

So... Since $\xi = 0$ in bend, it will stay at $\xi = 0$ in straight section.

We have parallel flow in straight section, so $v = 0$, and $\xi = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} = 0$

So $\frac{\partial u}{\partial y} = 0$, or $u(y) = \text{const.}$ Correct answer is (iii) (10)

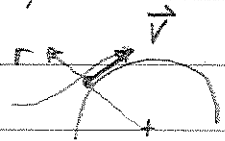


2).

$$a) V_r = \frac{\partial \phi}{\partial r} = V_\infty \cos \theta - \frac{K}{2\pi} \frac{\cos \theta}{r^2} = \left(V_\infty - \frac{K}{2\pi} \frac{1}{r^2} \right) \cos \theta$$

On cylinder surface: $V_r = 0$

$$\text{at } r=R: V_\infty - \frac{K}{2\pi R^2} = 0 \Rightarrow \boxed{K = 2\pi R^2 V_\infty} \quad (10)$$



$$b) V_\theta = \frac{1}{r} \frac{\partial \phi}{\partial \theta} = -V_\infty \sin \theta - \frac{K}{2\pi} \frac{\sin \theta}{r^2} - \frac{\Gamma}{2\pi r} = -V_\infty \left[1 + \frac{R^2}{r^2} \right] \sin \theta - \frac{\Gamma}{2\pi r}$$

$$\text{On cylinder, } r=R, V_r=0, \text{ so } V = \sqrt{V_r^2 + V_\theta^2} = |V_\theta| = \left| -2V_\infty \sin \theta - \frac{\Gamma}{2\pi R} \right|$$

$$A: \sin \theta = 1, \quad V = \left| 2V_\infty + \frac{\Gamma}{2\pi R} \right| \quad (5)$$

$$B: \sin \theta = -1, \quad V = \left| 2V_\infty - \frac{\Gamma}{2\pi R} \right| \quad (5)$$

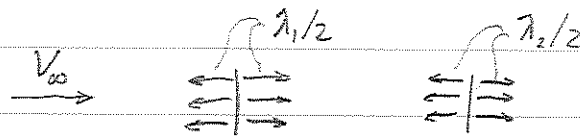
$$C: \sin \theta = 0, \quad V = \left| \frac{\Gamma}{2\pi R} \right| \quad (5)$$

$$c) i) \text{ From a) } R^2 = \frac{K}{2\pi V_\infty}, \text{ so to hold } R \text{ constant if } V_2 = 2V, \quad \boxed{K_2 = 2K} \quad (5)$$

$$ii) L' = \rho V_\infty \Gamma, \text{ so to hold } L' \text{ constant if } V_2 = 2V, \quad \boxed{\Gamma_2 = \frac{1}{2} \Gamma} \quad (5)$$

3)

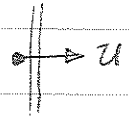
a) Velocity components:



At point A: $u = V_\infty - \frac{\lambda_1}{2} - \frac{\lambda_2}{2} = 0$ (required)

$1 - \frac{\lambda_1}{2} - (-\frac{1}{2}) = 0$

$\lambda_1 = 3$ (10)



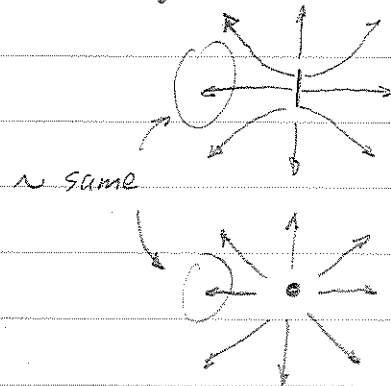
b) At point B: $u = V_\infty + \frac{\lambda_1}{2} + \frac{\lambda_2}{2}$

$u = 1 + \frac{3}{2} - \frac{1}{2} = 2$ (5)



c) At large distances ($d \gg l$), the velocity field of a source panel becomes the same as that of a point source with the same total strength $\Lambda = \lambda l$

So far away, velocity of source panel is $V_r = \frac{\lambda l}{2\pi r}$



For this case, at point A,

$u = V_\infty - \frac{\lambda_1}{2} - \frac{\lambda_2 l}{2\pi d} = 0$ (required)

$1 - \frac{\lambda_1}{2} + \frac{1}{20\pi} = 0$

$\lambda_1 = 2 + \frac{1}{10\pi}$ (10)

