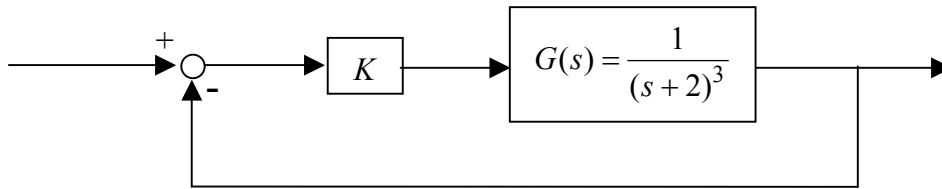


Department of Mechanical Engineering
 Massachusetts Institute of Technology
2.010 Modeling, Dynamics, and Control III
 Spring 2002

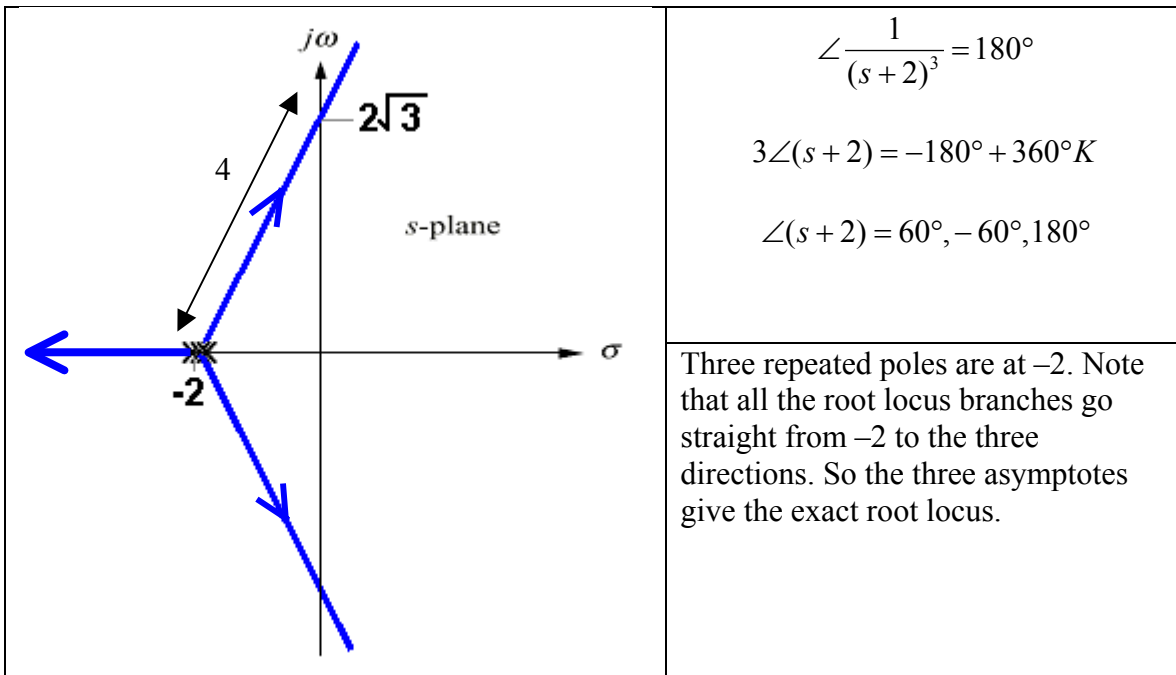
SOLUTIONS: Quiz #2

Problem 1

(1 – a) [10 points] Plotting the Root Locus



Root Locus



(1 – b) [15 points] Feedback Gain

$$K = \frac{1}{|G(s)|} = |s+2|^3$$

From our plot we know that the marginally stable poles lie at: $\pm j2\sqrt{3}$

$$|s + 2| = \sqrt{2^2 + (2\sqrt{3})^2} = 4$$

$$\therefore K = 4^3 = 64$$

This computation is quite simple, if you realize that you can use the characteristics of a 30-60-90 triangle to find each length graphically.

Checking with the Routh Hurwitz Table

First finding the closed-loop characteristic equation:

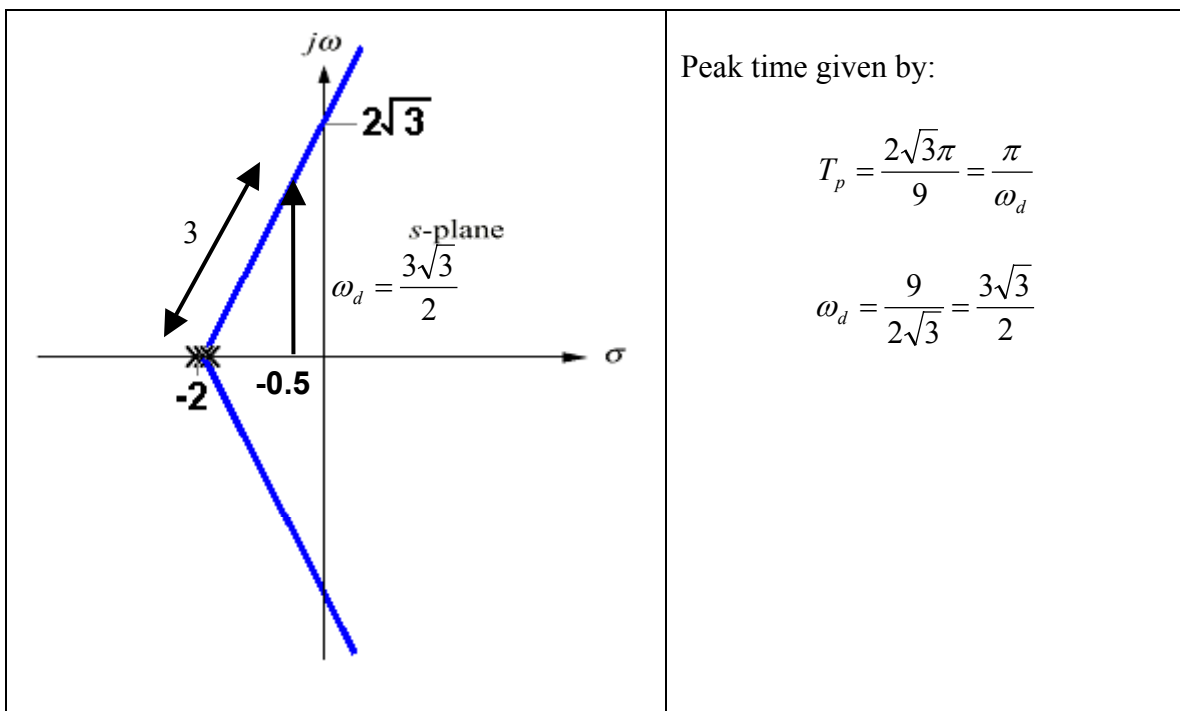
$$T(s) = \frac{KG}{1 + KG} = \frac{K}{(s + 2)^3 + K} = \frac{K}{s^3 + 6s^2 + 12s + (8 + K)}$$

s^3	1	12
s^2	6	$8 + K$
s^1	$12 - \frac{8 + K}{6}$	0
s^0	$8 + K$	0

So, $8 + K < 72 \therefore K < 64$

Marginally stable when $K = 64$, just as we found graphically.

(1 – c) [15 points] Poles for peak time



The position of this pole can be found graphically, using the characteristics of a 30-60-90 triangle as shown above. Or, you can also think of the root locus is given by the line with slope = $\sqrt{3}$, and y-intercept $2\sqrt{3}$. Then, the equation for this line would be:

$$y = \sqrt{3}x + 2\sqrt{3}$$

We already know the y-coordinate so all we need to find is the x-coordinate.

$$y = \frac{3\sqrt{3}}{2}, \text{ so:}$$

$$\frac{3\sqrt{3}}{2} = \sqrt{3}x + 2\sqrt{3}$$

$$\therefore x = -\frac{1}{2}$$

So, the dominant closed loop poles are

$$p_{1,2} = -\frac{1}{2} \pm j\frac{3\sqrt{3}}{2}$$

$$K = |s + 2|^3 = \left(\sqrt{\left(\frac{3}{2}\right)^2 + \left(\frac{3\sqrt{3}}{2}\right)^2} \right)^3 = 3^3 = 27$$

The third pole for this given gain is found by working backwards from the equation above. Replacing s by a real number σ in the above equation,

$$K = |\sigma - (-2)|^3 = |\sigma + 2|^3 = 27$$

$$|\sigma + 2| = 3$$

$$\therefore \sigma = -5$$

The third pole is at -5 ; 10 times farther from the imaginary axis than the dominant poles. Therefore the second-order approximation is valid.

Problem 2

(2 – a) [10points] Modeling

The equation of motion:

$$J\ddot{\theta} = \tau - b\dot{\theta} + F_d \times L$$

The nozzle reaction force creates this moment about the joint axis.

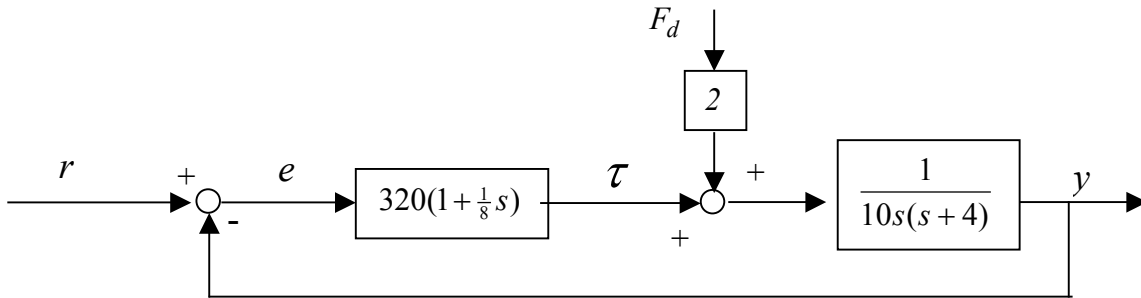
$$(Js^2 + bs)\theta(s) = \tau(s) + LF_d(s)$$

$$y(s) = \theta(s) \cdot L = \frac{L\tau(s) + L^2F_d(s)}{s(Js + b)}$$

(2 – b) [20 points] PD Control

<p>A root locus plot in the s-plane. The horizontal axis is the real axis and the vertical axis is the imaginary axis. There is a zero at Z_c on the negative real axis and two poles at $s = -4$ and $s = 0$. A desired closed-loop pole is marked with a blue 'x' at $\sigma = 4$ on the real axis. A line from the origin to this pole makes a 45° angle with the real axis. Another 45° angle is shown between the real axis and the line connecting the origin to the pole at $s = -4$.</p>	$T_s = 1 \text{ sec} = \frac{4}{\zeta \omega_n} = \frac{4}{\sigma}$ $\sigma = 4$ $\zeta = \frac{1}{\sqrt{2}}, \sin \theta = \frac{1}{\sqrt{2}}$ $\theta = 45^\circ$ <p>Now we know exactly what our desired Closed Loop Poles are:</p> $p_{1,2} = -4 \pm j4$ $\angle \frac{s + Z_c}{s(s + 4)} = 180^\circ$ $\angle(s + Z_c) = 180^\circ + \angle s + \angle(s + 4)$ $= 180^\circ + 135^\circ + 90^\circ = 405^\circ$ $= 45^\circ$
<p>A root locus plot in the s-plane. The horizontal axis is the real axis and the vertical axis is the imaginary axis. There is a zero at $s = -8$ and two poles at $s = -4$ and $s = 0$. A blue circle highlights the region around the zero at $s = -8$ and the pole at $s = -4$. The distance from the origin to the zero is $4\sqrt{2}$, and the distance from the origin to the pole at $s = -4$ is also $4\sqrt{2}$. Blue arrows on the real axis indicate the direction of the root locus branches.</p>	<p>Now we need to find the location of the zero along the real axis</p> $\frac{4}{Z_c - 4} = \tan 45^\circ = 1$ $\therefore Z_c = 8$ $K'G_c G(s) = \frac{K'(s + 8)}{10s(s + 4)} = -1$ $K' = \frac{10 s \cdot s + 4 }{ s + 8 } = \frac{10 \cdot 4\sqrt{2} \cdot 4}{4\sqrt{2}} = 40$ $K'G_c = 40(s + 8) = 320(1 + \frac{1}{8}s)$ $\therefore K = 320, k_D = \frac{1}{8} = 0.125$

(2 – c) [15 points] Steady State error



Deriving the equation for error again:

$$\begin{aligned}
 y &= G(2F_d + G_c e) \\
 e &= r - y = r - 2GF_d - GG_c e \\
 (1 + GG_c)e &= r - 2GF_d \\
 e &= \frac{r - 2GF_d}{1 + GG_c}
 \end{aligned}$$

$$\text{For } r = \frac{1}{s}, \quad e_{ss,r} = \lim_{s \rightarrow 0} s \frac{1}{s} \frac{10s(s+4)}{10s(s+4) + 320(1 + \frac{1}{8}s)} = 0$$

$$\text{For } F_d = \frac{1}{s}, \quad -e_{ss,F_d} = \lim_{s \rightarrow 0} s \frac{1}{s} \frac{2}{10s(s+4) + 320(1 + \frac{1}{8}s)} = \frac{1}{160} = 0.00625$$

(2 – d) [15 points] Compensator: PI

In order to reduce the steady state error contribution of the disturbance to zero consider a PI controller with a pole at the origin and a zero at $s = -\sigma$

$$G_c = K \left(1 + \frac{1}{8}s \right) \left(1 + \frac{\sigma}{s} \right)$$

$$\text{For } F_d = \frac{1}{s^2}$$

$$-e_{ss,F_d} = \lim_{s \rightarrow 0} s \frac{1}{s^2} \frac{2}{10s(s+4) + 320(1 + \frac{1}{8}s)(1 + \frac{\sigma}{s})}$$

$$-e_{ss} = \lim_{s \rightarrow 0} \frac{2}{10s^2(s+4) + 320\left(1 + \frac{1}{8}s\right)(s+\sigma)} = \frac{1}{160\sigma} = 0.0625 = 6.25\%$$

$$\sigma = \frac{1}{160 \times 0.0625} = 0.1$$

The transfer function for the combined controller is now given by:

$$G_c = 320 \left(1 + \frac{1}{8}s\right) \left(1 + \frac{0.1}{s}\right) = \frac{(320 + 40s)(s + 0.1)}{s}$$

$$G_c = \frac{10s^2 + 324s + 32}{s} = 32 \frac{1.25s^2 + 10.125s + 1}{s}$$

