

Department of Mechanical Engineering  
Massachusetts Institute of Technology  
**2.010 Modeling, Dynamics, and Control III**  
**Spring 2002**

**SOLUTIONS: Quiz #3**

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**Problem 1**

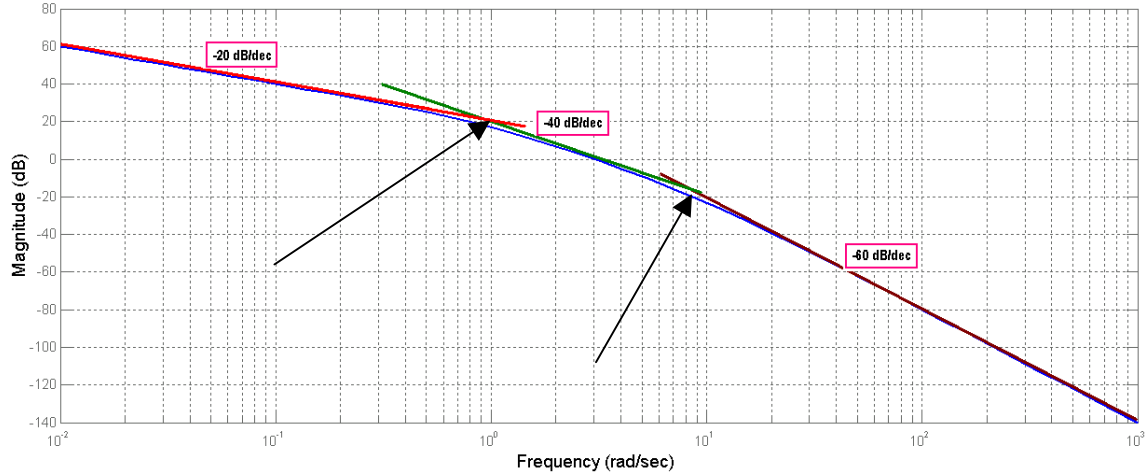
**(1 – a) 15 points**

The slope of the gain curve at low frequencies is  $-20$  dB/dec; therefore there is one pole at the origin and this is a Type 1 system.

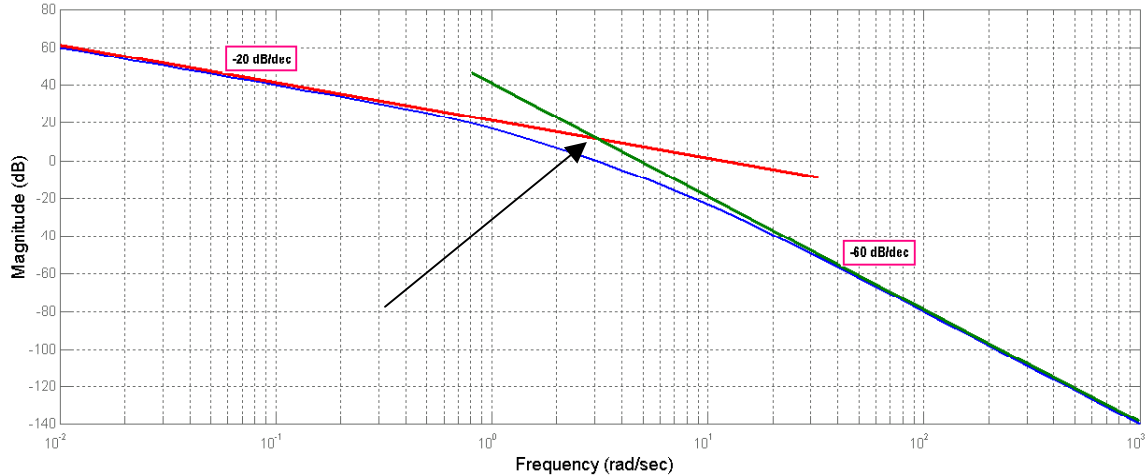
The phase curve asymptotically reaches  $-270^\circ$ , hence the relative order of the system is 3. Since both the gain and the phase curves are monotonically decreasing, there is no zero in this system.

As mentioned, there is one pole at the origin, and there must be two more poles in the system.

Approximating the gain curve by three asymptotes of slope  $-20$  dB/dec,  $-40$  dB/dec and  $-60$  dB/dec, respectively we obtain the break frequencies at  $1$  rad/sec and  $10$  rad/sec, as shown in the figure.



Another way of approximating the gain curve is to use two asymptotes of slope  $-20$  dB/dec and  $-60$  dB/dec, respectively. That is the case having one integrator and two repeated poles on the real axis. Then the intersection of these two asymptotes is found at  $3$  rad/sec. The break frequency is  $3$  rad/sec.



**(1 – b) 10 points**

At 3 rad/sec, the gain is 0 dB and the phase is  $-180^\circ$ . Therefore the gain margin is 0 dB, and the phase margin is  $0^\circ$ .

$$GM = 0 \text{ dB}, \Phi_M = 0^\circ$$

At this point the system is critically stable, i.e. the closed-loop poles are on the imaginary axis. Therefore, the undamped natural frequency is 3 rad/sec. Also note that  $\Phi_M = \omega_n$ , when  $\zeta = 0$ .

**(1 – c) 10 points**

See the attached Bode plots

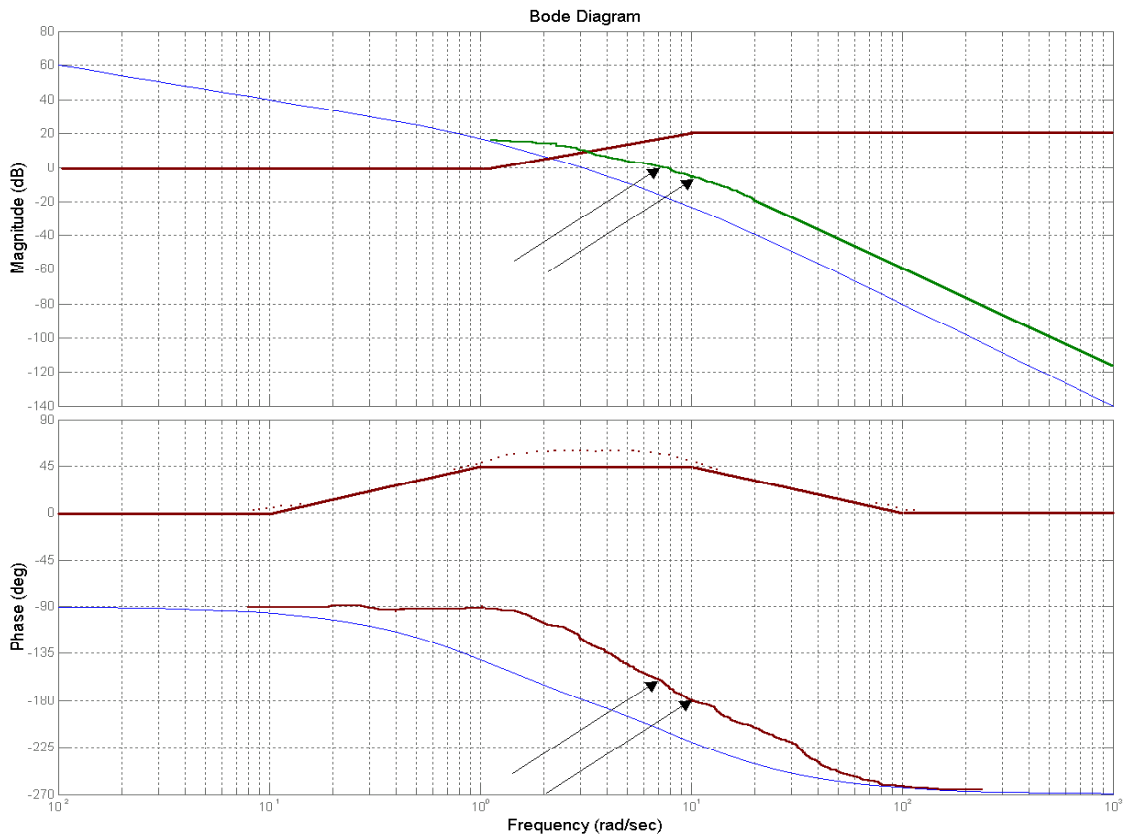
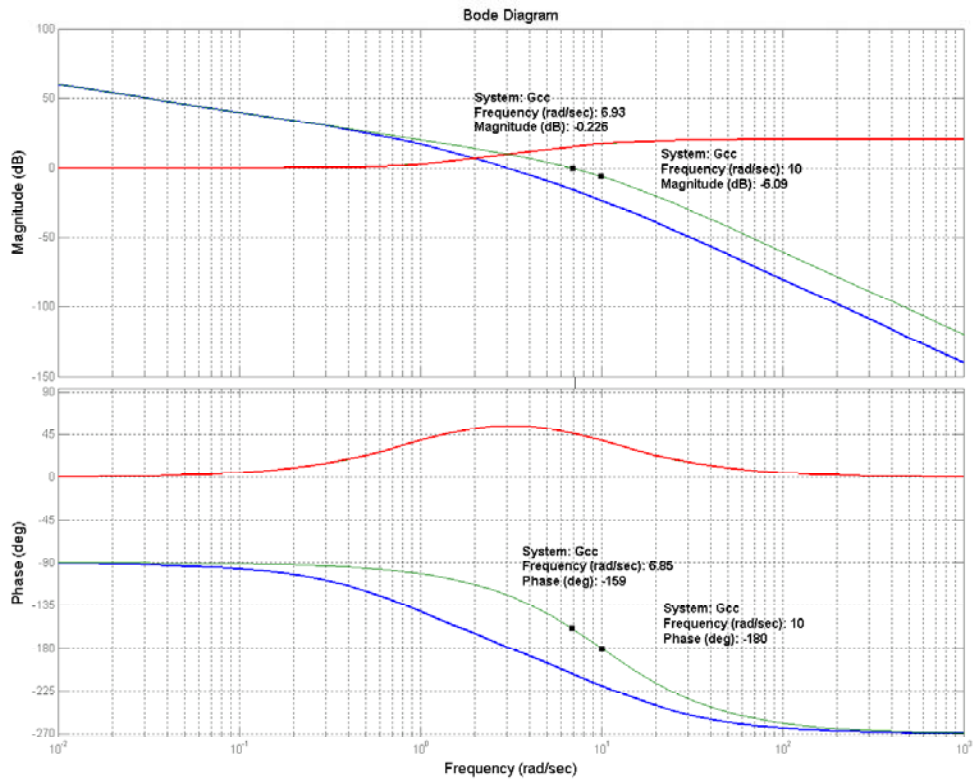
$$G_c = \frac{Ts + 1}{\beta Ts + 1} = \frac{s + 1}{0.1s + 1} \therefore T = 1, \beta = 0.1$$

**(1 – d) 10 points**

From the new compensated gain curve, the gain cross over frequency, i.e. the phase margin frequency, is 7 rad/s. From the phase curve the phase margin is  $21^\circ$ .

The compensated phase curve crosses the minus  $180^\circ$  line at 10 rad/s hence the gain margin is: 6 dB

Here is a plot of the exact solution done in matlab. For this problem, exact values are not needed, but your answer must be consistent with your plots.



Obviously, MATLAB was not available on the test, so here is an approximated solution done by hand. The arrows show the same relevant points marked above.

**(1 – e) 15 points**

The damping ratio  $\zeta$  of the dominant poles is determined directly from the phase margin  $\Phi_M$ . Approximately the relationship between  $\zeta$  and  $\Phi_M$  for  $0 < \zeta \leq 0.6$  is given by

$$\zeta \cong \frac{\Phi_M}{100} = 0.21$$

The percent overshoot is then

$$\%OS = e^{-\frac{\pi\zeta}{\sqrt{1-\zeta^2}}} = 50\%$$

The gain cross over frequency  $\omega_{\Phi_M}$  is related to  $\zeta$ , and  $\omega_n$  such that:

$$\omega_{\Phi_M} = \omega_n \sqrt{-2\zeta^2 + \sqrt{1 + 4\zeta^4}}$$

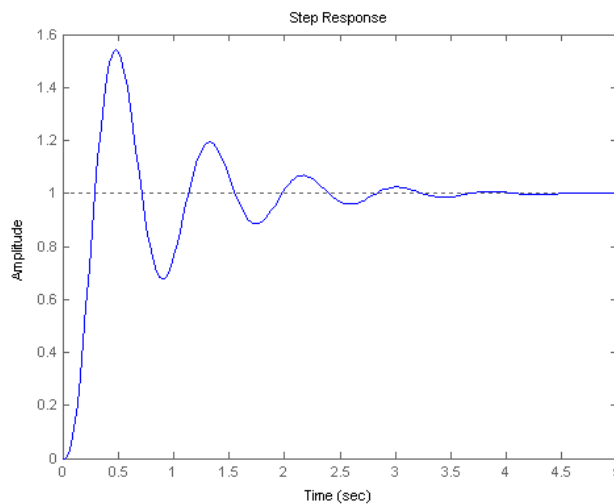
Therefore

$$\omega_n = \frac{\omega_{\Phi_M}}{\sqrt{-2\zeta^2 + \sqrt{1 + 4\zeta^4}}} = 7.1 \text{ rad/s}$$

The peak time is obtained from  $\omega_n$  and  $\zeta$

$$T_p = \frac{\pi}{\omega_n \sqrt{1 - \zeta^2}} = 0.45 \text{ sec}$$

You didn't have to plot the step response, but it's nice to see that it does indeed it displays the characteristics that were calculated.



**(1 – f) 10 points**

The gain curve at low frequencies is approximated to:

$$|G(j\omega)| \cong \left| \frac{k}{s} \right|_{s=j\omega} = \frac{k}{\omega}$$

Velocity constant  $K_v$  is given by the frequency at which the extension of the approximate gain curve intersects the 0 dB line. Lifting the gain curve 10 dB higher, the approximate gain curve intersects the 0 dB line at 30 rad/sec, therefore  $K_v = 30$  rad/sec.

**Problem 2**

**(2 – a) 15 points**

This is a typical second order system, whose transfer function will look like:

$$G(s) = \frac{Y(s)}{F(s)} = \frac{1}{Ms^2 + Bs + K}$$

Given a percent overshoot we can find the value of  $\zeta$  :

$$\zeta = \frac{-\ln(\%OS/100)}{\sqrt{\pi^2 + \ln^2(\%OS/100)}} = 0.46$$

The peak magnitude  $M_p$  is determined by  $\zeta$ ,

$$M_p = \frac{1}{2\zeta\sqrt{1-\zeta^2}} = 1.23$$

To obtain the peak resonant frequency the undamped natural frequency  $\omega_n$  must be determined:

$$\omega_n = \sqrt{\frac{K}{M}} = 10 \text{ rad / sec}$$

Therefore the peak resonant frequency  $\omega_r$  is

$$\omega_r = \omega_n \sqrt{1 - 2\zeta^2} = 7.64 \text{ rad / sec}$$

**(2 – b) 15 points**

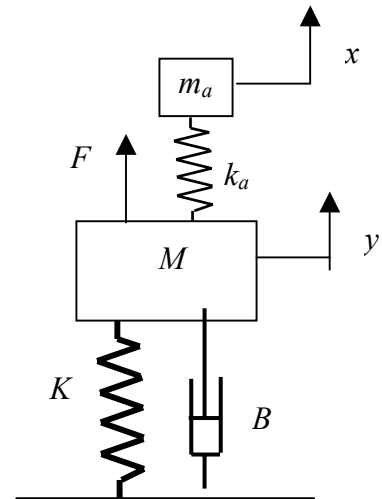
$$M\ddot{y} = -Ky - B\dot{y} + F + k_a(x - y)$$

$$m_a\ddot{x} = -k_a(x - y)$$

$$[Ms^2 + Bs + (K + k_a)]Y(s) = F + k_ax$$

$$[m_as^2 + k_a]X(s) = k_aY(s)$$

$$G(s) = \frac{Y(s)}{F(s)} = \frac{m_as^2 + k_a}{[Ms^2 + Bs + (K + k_a)][m_as^2 + k_a] - k_a^2}$$



The minimum for this transfer function will occur when  $|G(j\omega)|$  becomes zero i.e. when the numerator of the transfer function becomes zero:

$$(m_as^2 + k_a)|_{s=j\omega} = 0$$

$$\omega = \sqrt{\frac{k_a}{m_a}}$$

so,

$$k_a = \omega^2 m_a = 10^2 \cdot 5 = 500 \text{ N/m}$$