# **Precision Machine Design**

# Topic 17

### Flexures

### **Purpose:**

From the flip-top on a shampoo bottle to the piezo-beams on a scanning tunneling microscope, flexural bearings are one of the most widely used types of bearings. However, they are one of the least well-understood bearings by most engineers. This lecture introduces the concept of flexural bearings and their characteristics.

# **Outline:**

- Introduction
- General characteristics
- Types of flexures

"Genius can only breathe in an atmosphere of freedom"

John Stuart Mill

# Introduction

• Monolithic designs:



- Most accurate.
- Sometimes difficult to machine:
  - Abrasive water jet machining is an economical way to cut non-citical areas (links).
  - Wire EDM can be used for precision cuts in critical hinge areas.
- May require localized heat treating of the material in the flexure.
- Applications include flexural couplings, mirror mounts, STM's, and many others.
- Size is about 20 times the range of motion

• Clamped designs:



- Nanometer accuracy and better can be obtained if the bolted joint is properly designed.
  - Rounded edges
  - bolt cones-of-action overlap
- Easy to assemble from annealed parts and hardened spring steel.
  - Careful when tightening bolts, as the torque can twist the flexure!
    - Lubricated thrust washers can help.
- Care is required to make sure residual stresses don't create asymmetries that create parasitic error motions.
  - Cut spring metal with EDM or waterjet.
  - Use dual lubricated washers under bolt heads and guides for clamp plates.
- Applications include wafer steppers, mirror mounts, and many others.
- Size is about 10 times the range of motion

# Speed and acceleration limits

• Limited only by yield strength and design.

# **Range of motion**

- Typically used for motions less than a few millimeters.
- Monolithic designs: flexure length/motion = 20 or more.
- Clamped designs: flexure length/motion = 5-10

# **Applied** loads

• Design goal is to obtain load capacity with minimum spring constant.

# Repeatability

- Axial: limited only by the drive system.
- Lateral: less than nanometers for monolithic designs.

# Resolution

• Axial: limited only by the drive system.

# Preload

• Inherently preloaded.

# Stiffness

- The greater the motion and the lower the spring rate, the less the stiffness.
- Theory of elasticity or finite element analysis yields very accurate predictions of performance.
- Flexures often have low transverse stiffness, so they are more susceptible to parasitic forces!

# Vibration and shock resistance

• Very good.

# **Damping capability**

- Material damping only (2-5%).
- Damping mechanisms (constrained layer dampers) can be used to obtain high damping.

#### Accuracy

- Axial: limited only by the drive system.
- Lateral: can be less than nanometers for monolithic designs.
- Depends on how well the bearing was assembled or machined.
- Even if there is a small off-axis error motion associated with the primary motion:
  - The error motion is usually very predictable and highly repeatable.
- Flexural bearings cannot attain perfect motion because of:
  - Variation in spring strength
    - Elastic modulus varies with rolling direction in steels.
  - Variation in spring geometry.
  - Overall inaccuracies of manufacture.
  - Bending of the bearing in an unintended manner.
  - Bending of structure.
  - External applied loads (e.g., gravity and the manner in which the actuation force is applied)

- The most common errors are the pitch angle and vertical motion.
  - They accompany linear motion in a four bar linkage flexure.
- For small displacements, the errors are a function of:



- The distance moved x.
- The length of the springs  $\ell$ .
- The spring thickness t.
- The platform length b.
- The distance of force application *a* above the fixed end of the springs

$$\theta_{\text{pitch}} = \left(\frac{6(\ell - 2a) t^2}{3b^2 \ell - 2t^2 \ell + 6at^2}\right) \left(\frac{x}{\ell}\right)$$
$$\delta_{\text{vertical}} \approx \frac{x^2}{2\ell}$$

• Note that there is no pitch error when  $a = \ell/2$ 

- If the force is applied at a point other than halfway between the platforms:
  - A bending moment is generated which causes a pitch error to occur.
- The pitch errors caused by the difference in spring length and difference in platform length are respectively:

$$\theta_{\text{spring}} = \frac{\delta_{\text{spring}} x^2}{2\ell^2 b}$$
$$\theta_{\text{platform}} = \frac{\delta_{\text{platform}} x}{\ell b}$$

• Proven by Jones who gives typical tolerances on the spring and platform length to be 25  $\mu$ m and 1-3  $\mu$ m respectively.

### **Types of flexures**<sup>1</sup>

• Four bar linkage flexure:



• In the Y direction there is a small error motion  $\delta y$  that is a function of the X motion  $\delta x$  and flexure length  $\ell$ :

$$\delta_{\rm y} \approx \frac{\delta_{\rm x}^2}{2\ell}$$

- Consider other parasitic motions mentioned earlier.
- X direction stiffness is equal to two fixed-fixed beams acting together in a side by side mode.
- Y direction stiffness is equal to that of two columns.
- Buckling effect is negligible for small motions and should be prevented by the X direction servo.

<sup>&</sup>lt;sup>1</sup> Modular flexural bearing components can be purchased: Alson E. Hatheway Inc., Suite 400, 595 East Colorado Blvd., Pasadena, California 91101.

- To minimize parasitic motions:
  - Symmetrical dual four bar linkage eliminates  $\delta Y$  error.
    - Strains along flexure's length resisted by the frame:
      - Stiffness is increased: range of motion is decreased:



• Use a two stage (stacked) four bar linkage:



- The parasitic motions of one 4-bar cancel the parasitic motions of the second 4-bar.
- Lateral and yaw stiffness will not be high, however, due to buckling effect.
- Overcome by use of monolithic hourglass-type members.

- A differential actuation system can be used to increase resolution.
  - A wobble pin will minimize parasitic force actuation errors:



#### • Alternate differential design:



• Left and right platforms would be connected to a common rigid top-plate.

• When the flexure is built in to "walls", it needs extensional capability: (after F. Zhu at Delft):



• Many thin blades can be used to increase lateral stiffness and load capacity while keeping axial stiffness and stress low:





- Be careful of alignment and slip problems between the blades.
- EDM process can be used to prevent these problems.
- Rubber placed between the blades can increase damping.
- Careful when tightening bolts, as the torque can twist the flexure!

• Lever and fulcrum transmission:



• A bowed flexure used as a high reduction transmission:



• A downward motion  $\delta$  causes a lateral motion  $\Delta$ :

$$\Delta \approx \frac{4\delta\ell_{h}}{\ell_{w}}$$

- It is possible to chain together a series of these bowed flexures at right angles to each other.
  - This can yield a very high transmission ratio.
  - Assume that  $\ell_h = 2 \text{ mm}$  and  $\ell_W = 20 \text{ mm}$ , then the transmission ratio is 5.
  - In series, the ratios become 25, 125, 625... for 2, 3, 4... units respectively.
- A variation to this bowed beam approach is to use two beams laid on top of each other and tied together at one end.
- When the beams bend there will be differential motion along the interface between them.

### Flexures that provide angular motion

• Device for adjusting pitch and yaw (Courtesy of Polaroid Corp.):



- Note the transmission effect, where the screws push up on the upper beam, using the lower beam as a base.
- If the top beam were 1/2" thick, and the bottom beam were 1/8" thick, then the transmission ration would be  $((1/2)/(1/8))^3 = 64!$
- The slope at the end of the beam causes an Abbe error in the beam that holds the optic which cancels the beam deflection  $(\delta = \alpha(2/3L):$



• Cross-strip flexure for angular motion:



• Lucas flexural pivots (Courtesy of Lucas Aerospace Power Transmission Corporation.):



- For limited motion applications use in place of rolling element bearings.
- Flexural pivots are not subject to fretting problems.

### Flexures to guide and lock components into place

• Flexures can be used as one-shot hinges to guide components into alignment and then lock them into place:

![](_page_16_Figure_3.jpeg)

- X direction stiffness of the clamping system is equal to:
  - The sum of the X direction stiffness of the anvil and locking member due to the preload effect.
- Small taper keeps component preloaded in both the X and Y directions.
- To minimize distortion caused by bending, line of force must pass through the support ledge.
- A lens could be kinematically held by two anvils and a single locking member.
- The geometry is tolerant of manufacturing errors.

• For precise X position location, utilize a grooved structure:

![](_page_17_Figure_2.jpeg)

- Numerous permutations are possible.
- The moral of the story is don't do this:

![](_page_17_Figure_5.jpeg)

• Flexures allow for snap assembly of components which make the design of systems more efficient:

![](_page_18_Figure_2.jpeg)

(From US Patent 5,102,235 by Peter Mugglestone of Thomson Industries Inc.)

- End caps click together.
- Seal is a single molded piece.
- No screws required.

• Flexures for fixturing: Opposed L's support a platform so it can move in six degrees of freedom<sup>2</sup>.

![](_page_19_Figure_2.jpeg)

• This allows chips held in the platform to be operated on (tested in this case).

<sup>&</sup>lt;sup>2</sup> Patent Pending, Kinetrix, Inc. 33 Constituition Drive, Bedford, MH 03110-6000. Contact Dr. Alexander Slocum.