# **Precision Machine Design**

# **Topic 17**

#### **Flexures**

#### **Purpose:**

**From the flip-top on a shampoo bottle to the piezo-beams on a scanning tunneling microscope, flexural bearings are one of the most widely used types of bearings. However, they are one of the least well-understood bearings by most engineers. This lecture introduces the concept of flexural bearings and their characteristics.**

# **Outline:**

- **Introduction**
- **• General characteristics**
- **• Types of flexures**

**"Genius can only breathe in an atmosphere of freedom"**

**John Stuart Mill**

### **Introduction**

**• Monolithic designs:**



- **• Most accurate.**
- **Sometimes difficult to machine:**
	- **• Abrasive water jet machining is an economical way to cut non-citical areas (links).**
	- **• Wire EDM can be used for precision cuts in critical hinge areas.**
- **May require localized heat treating of the material in the flexure.**
- **• Applications include flexural couplings, mirror mounts, STM's, and many others.**
- **• Size is about 20 times the range of motion**

**• Clamped designs:**



- **• Nanometer accuracy and better can be obtained if the bolted joint is properly designed.**
	- **• Rounded edges**
	- **• bolt cones-of-action overlap**
- **• Easy to assemble from annealed parts and hardened spring steel.**
	- **• Careful when tightening bolts, as the torque can twist the flexure!**
		- **Lubricated thrust washers can help.**
- **• Care is required to make sure residual stresses don't create asymmetries that create parasitic error motions.**
	- **• Cut spring metal with EDM or waterjet.**
	- **• Use dual lubricated washers under bolt heads and guides for clamp plates.**
- **• Applications include wafer steppers, mirror mounts, and many others.**
- **• Size is about 10 times the range of motion**

### **Speed and acceleration limits**

**• Limited only by yield strength and design.**

#### **Range of motion**

- **• Typically used for motions less than a few millimeters.**
- **• Monolithic designs: flexure length/motion = 20 or more.**
- **• Clamped designs: flexure length/motion = 5-10**

## **Applied loads**

**• Design goal is to obtain load capacity with minimum spring constant.**

## **Repeatability**

- **• Axial: limited only by the drive system.**
- **• Lateral: less than nanometers for monolithic designs.**

## **Resolution**

**• Axial: limited only by the drive system.**

### **Preload**

**• Inherently preloaded.**

#### **Stiffness**

- **• The greater the motion and the lower the spring rate, the less the stiffness.**
- **• Theory of elasticity or finite element analysis yields very accurate predictions of performance.**
- **Flexures often have low transverse stiffness, so they are more susceptible to parasitic forces!**

### **Vibration and shock resistance**

**• Very good.**

## **Damping capability**

- **• Material damping only (2-5%).**
- **• Damping mechanisms (constrained layer dampers) can be used to obtain high damping.**

#### **Accuracy**

- **• Axial: limited only by the drive system.**
- **• Lateral: can be less than nanometers for monolithic designs.**
- **• Depends on how well the bearing was assembled or machined.**
- **• Even if there is a small off-axis error motion associated with the primary motion:**
	- **• The error motion is usually very predictable and highly repeatable.**
- **• Flexural bearings cannot attain perfect motion because of:**
	- **• Variation in spring strength**
		- **• Elastic modulus varies with rolling direction in steels.**
	- **Variation in spring geometry.**
	- **• Overall inaccuracies of manufacture.**
	- **• Bending of the bearing in an unintended manner.**
	- **• Bending of structure.**
	- **• External applied loads (e.g., gravity and the manner in which the actuation force is applied)**
- **• The most common errors are the pitch angle and vertical motion.**
	- **• They accompany linear motion in a four bar linkage flexure.**
- **• For small displacements, the errors are a function of:**



- **• The distance moved x.**
- The length of the springs  $\ell$ .
- **• The spring thickness t.**
- **• The platform length b.**
- **• The distance of force application** *a* **above the fixed end of the springs**

$$
\theta_{\text{pitch}} = \left(\frac{6(\ell - 2a) t^2}{3b^2 \ell - 2t^2 \ell + 6at^2}\right) \left(\frac{x}{\ell}\right)
$$

$$
\delta_{\text{vertical}} \approx \frac{x^2}{2\ell}
$$

• Note that there is no pitch error when  $a = l/2$ 

- **• If the force is applied at a point other than halfway between the platforms:**
	- **A bending moment is generated which causes a pitch error to occur.**
- **• The pitch errors caused by the difference in spring length and difference in platform length are respectively:**

$$
\theta_{spring} = \frac{\delta_{spring} x^2}{2\ell^2 b}
$$

$$
\theta_{platform} = \frac{\delta_{platform} x}{\ell b}
$$

**• Proven by Jones who gives typical tolerances on the spring and platform length to be 25** µ**m and 1-3** µ**m respectively.**

#### **Types of flexures**<sup>1</sup>

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**• Four bar linkage flexure:**



**• In the Y direction there is a small error motion** δ**Y that is a function of the X motion**  $\delta$ **<b>X** and flexure length  $\ell$ :

$$
\delta_y \approx \frac{\delta_x^2}{2\ell}
$$

- **• Consider other parasitic motions mentioned earlier.**
- **X direction stiffness is equal to two fixed-fixed beams acting together in a side by side mode.**
- **Y direction stiffness is equal to that of two columns.**
- **• Buckling effect is negligible for small motions and should be prevented by the X direction servo.**

<sup>&</sup>lt;sup>1</sup> Modular flexural bearing components can be purchased: Alson E. Hatheway Inc., Suite 400, 595 East Colorado Blvd., Pasadena, California 91101.

- **• To minimize parasitic motions:**
	- **• Symmetrical dual four bar linkage eliminates** δ**Y error.**
		- **• Strains along flexure's length resisted by the frame:**
			- **• Stiffness is increased: range of motion is decreased:**



**• Use a two stage (stacked) four bar linkage:**



- **• The parasitic motions of one 4-bar cancel the parasitic motions of the second 4-bar.**
- **• Lateral and yaw stiffness will not be high, however, due to buckling effect.**
- **• Overcome by use of monolithic hourglass-type members.**
- **A differential actuation system can be used to increase resolution.**
	- **A wobble pin will minimize parasitic force actuation errors:**



#### **• Alternate differential design:**



**• Left and right platforms would be connected to a common rigid top-plate.**

**• When the flexure is built in to "walls", it needs extensional capability: (after F. Zhu at Delft):**



**• Many thin blades can be used to increase lateral stiffness and load capacity while keeping axial stiffness and stress low:**





- **• Be careful of alignment and slip problems between the blades.**
- **• EDM process can be used to prevent these problems.**
- **• Rubber placed between the blades can increase damping.**
- **• Careful when tightening bolts, as the torque can twist the flexure!**

**• Lever and fulcrum transmission:**



**• A bowed flexure used as a high reduction transmission:**



**• A downward motion** δ **causes a lateral motion** ∆**:**

$$
\Delta \approx \frac{4\delta\ell_{h}}{\ell_{w}}
$$

- **• It is possible to chain together a series of these bowed flexures at right angles to each other.**
	- **• This can yield a very high transmission ratio.**
	- **• Assume that**  $\ell_{\mathbf{h}} = 2$  **mm and**  $\ell_{\mathbf{w}} = 20$  **mm, then the transmission ratio is 5.**
	- **• In series, the ratios become 25, 125, 625... for 2, 3, 4... units respectively.**
- **A variation to this bowed beam approach is to use two beams laid on top of each other and tied together at one end.**
- **When the beams bend there will be differential motion along the interface between them.**

### **Flexures that provide angular motion**

**• Device for adjusting pitch and yaw** (Courtesy of Polaroid Corp.)**:**



- **Note the transmission effect, where the screws push up on the upper beam, using the lower beam as a base.**
- **If the top beam were 1/2" thick, and the bottom beam were 1/8" thick, then the transmission ration would be**  $((1/2)/(1/8))^3 = 64!$
- **• The slope at the end of the beam causes an Abbe error in the beam that holds the optic which cancels the beam deflection**  $(\delta = \alpha(2/3L))$ :



**• Cross-strip flexure for angular motion:**



**• Lucas flexural pivots** (Courtesy of Lucas Aerospace Power Transmission Corporation.)**:**



- **• For limited motion applications use in place of rolling element bearings.**
- **• Flexural pivots are not subject to fretting problems.**

#### **Flexures to guide and lock components into place**

**• Flexures can be used as one-shot hinges to guide components into alignment and then lock them into place:**



- **X direction stiffness of the clamping system is equal to:**
	- **• The sum of the X direction stiffness of the anvil and locking member due to the preload effect.**
- **• Small taper keeps component preloaded in both the X and Y directions.**
- **• To minimize distortion caused by bending, line of force must pass through the support ledge.**
- **A lens could be kinematically held by two anvils and a single locking member.**
- **• The geometry is tolerant of manufacturing errors.**

**• For precise X position location, utilize a grooved structure:**



- **• Numerous permutations are possible.**
- **• The moral of the story is don't do this:**



**• Flexures allow for snap assembly of components which make the design of systems more efficient:**



(From US Patent 5,102,235 by Peter Mugglestone of Thomson Industries Inc.)

- **• End caps click together.**
- **• Seal is a single molded piece.**
- **No screws required.**

• **Flexures for fixturing: Opposed L's support a platform so it can move in six degrees of freedom2.**



• **This allows chips held in the platform to be operated on (tested in this case).**

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<sup>2</sup> Patent Pending, Kinetrix, Inc. 33 Constituition Drive, Bedford, MH 03110-6000. Contact Dr. Alexander Slocum.