

Injection Molding



2.810

T. Gutowski

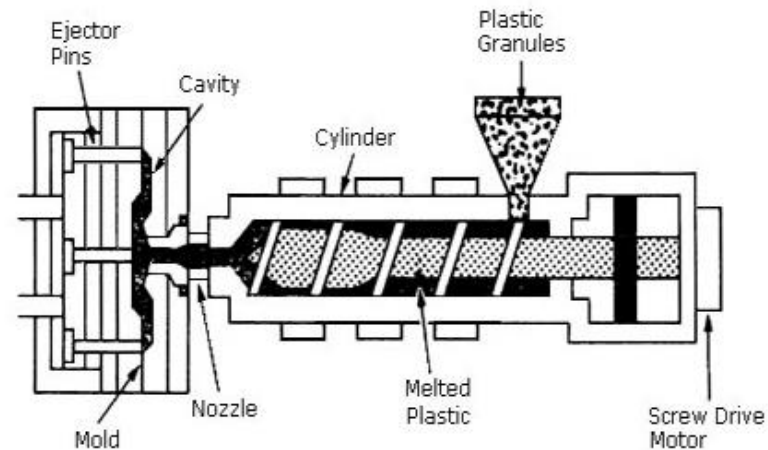
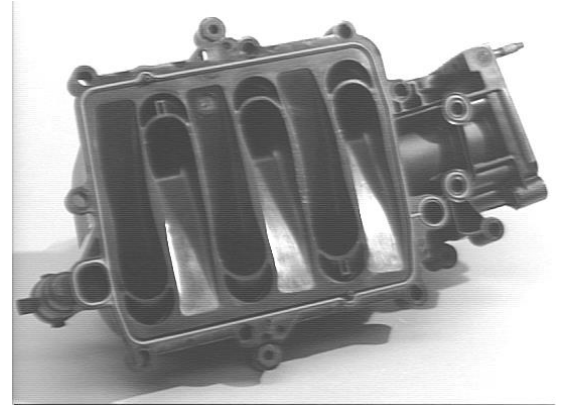
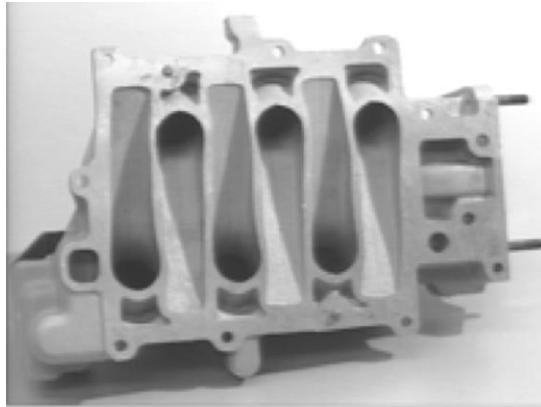
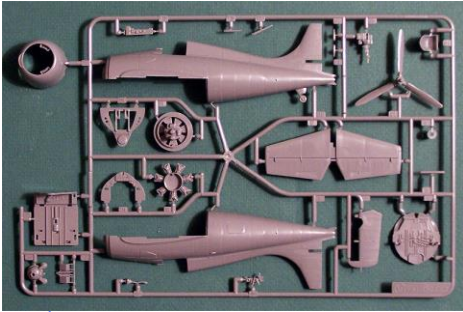


Diagram of a typical injection molding process. (Image taken from the [OSHA Technical Manual](#).)



V-6 air intake manifold



Water control valve
Brass Vs injection mold
www.mnrubber.com

Short history of plastics

- 1866 Celluloid
- 1891 Rayon
- 1907 Bakelite
- 1913 Cellophane
- 1926 PVC
- 1933 Polyethylene
- 1938 Teflon
- 1939 Nylon stockings
- 1957 velcro
- 1967 "The Graduate"
- 1970 Earth Day recycling



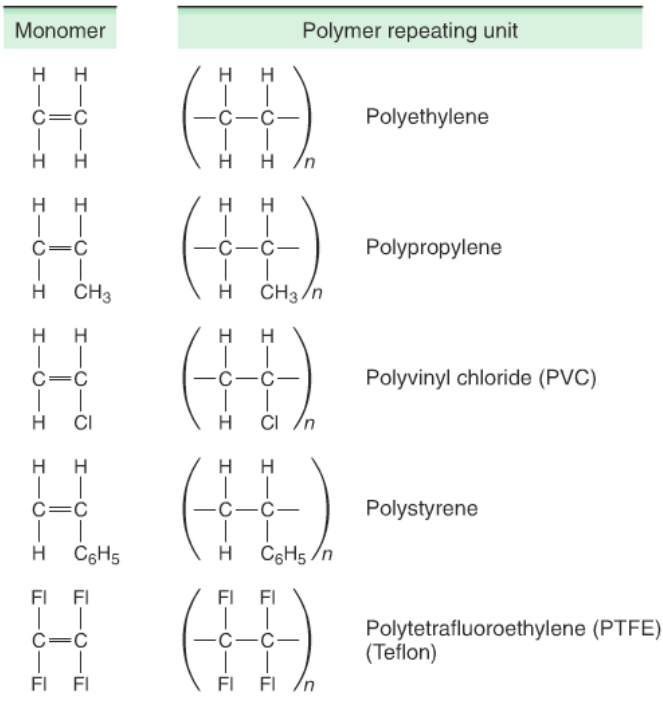


FIGURE 7.2 Molecular structure of various polymers. These are examples of the basic building blocks for plastics.

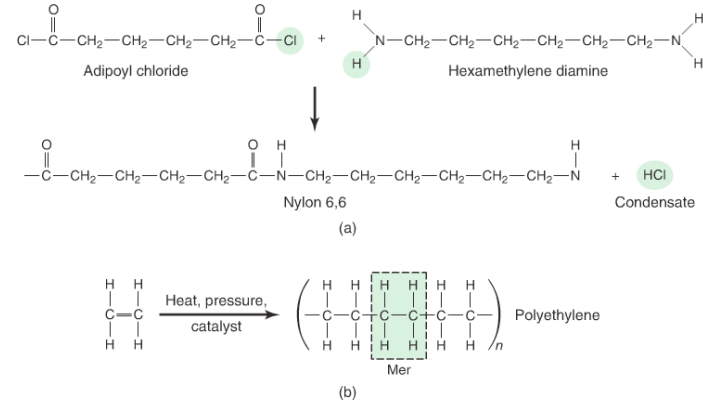
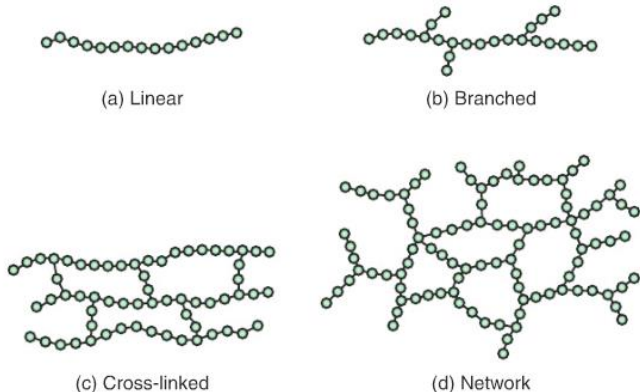
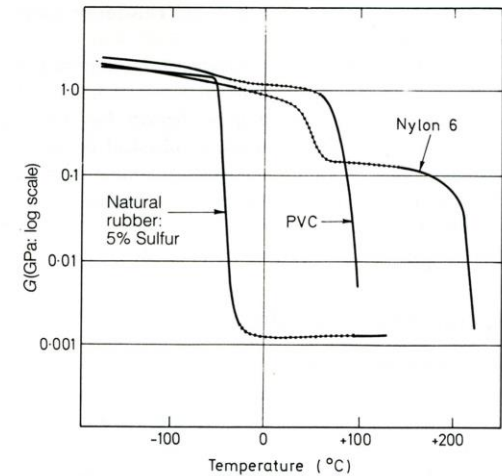


FIGURE 7.3 Examples of polymerization. (a) Condensation polymerization of nylon 6,6 and (b) addition polymerization of polyethylene molecules from ethylene mers.

TABLE 7.2

Glass-transition and Melting Temperatures of Some Polymers

Material	T_g (°C)	T_m (°C)
Nylon 6,6	57	265
Polycarbonate	150	265
Polyester	73	265
Polyethylene		
High density	-90	137
Low density	-110	115
Polymethylmethacrylate	105	—
Polypropylene	-14	176
Polystyrene	100	239
Polytetrafluoroethylene	-90	327
Polyvinyl chloride	87	212
Rubber	-73	—



4.21 Dependence of the shear modulus on temperature for three representative engineering polymers: natural rubber (cross-linked); PVC (essentially amorphous and not cross-linked); and nylon 6 (crystalline). The temperatures at which these polymers are used in technology are indicated (---) (after Wolf).

Outline

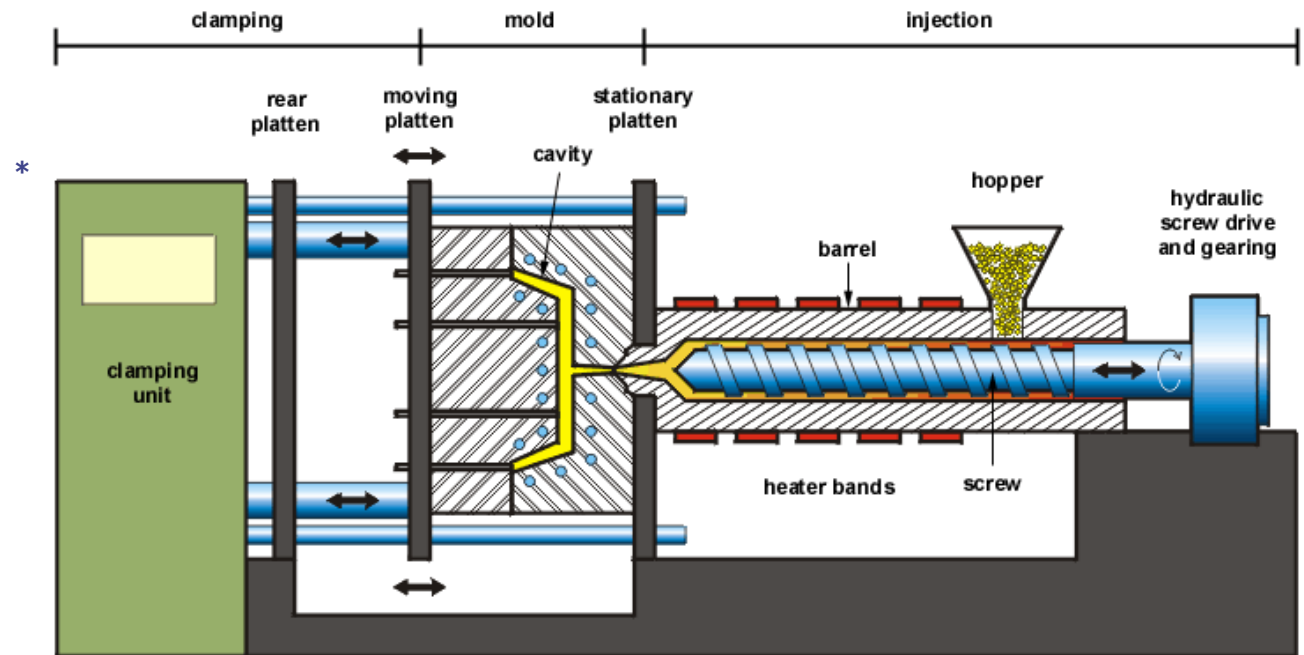
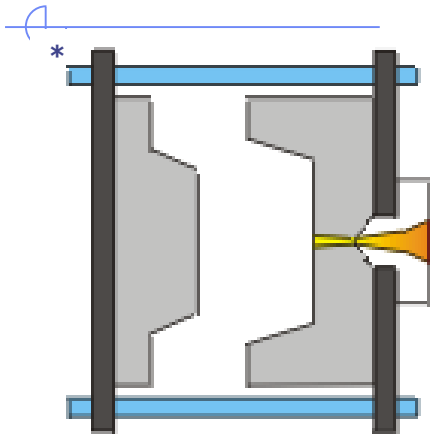
- ◆ Basic operation
- ◆ Cycle time and heat transfer
- ◆ Flow and solidification
- ◆ Part design
- ◆ Tooling
- ◆ New developments
- ◆ Environment

30 ton, 1.5 fl oz (45 cm³) Engel



Injection Molding Machine
for wheel fabrication

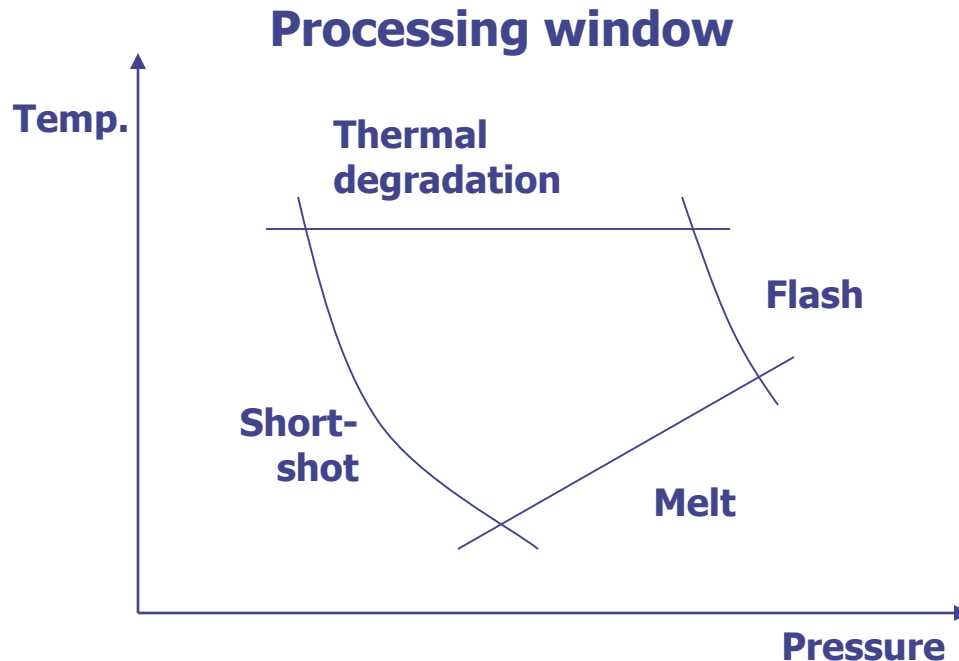
Process & machine schematics



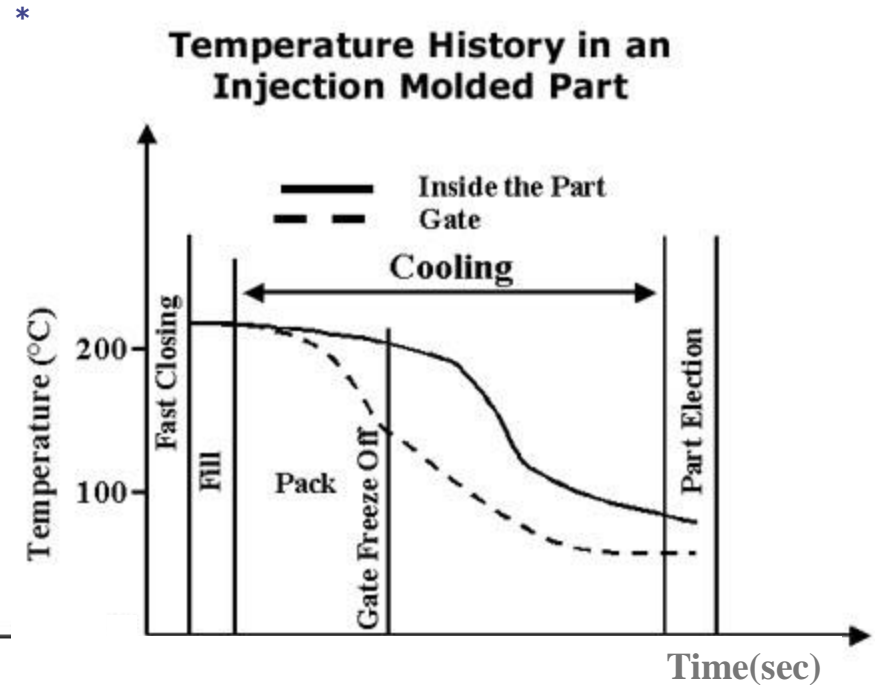
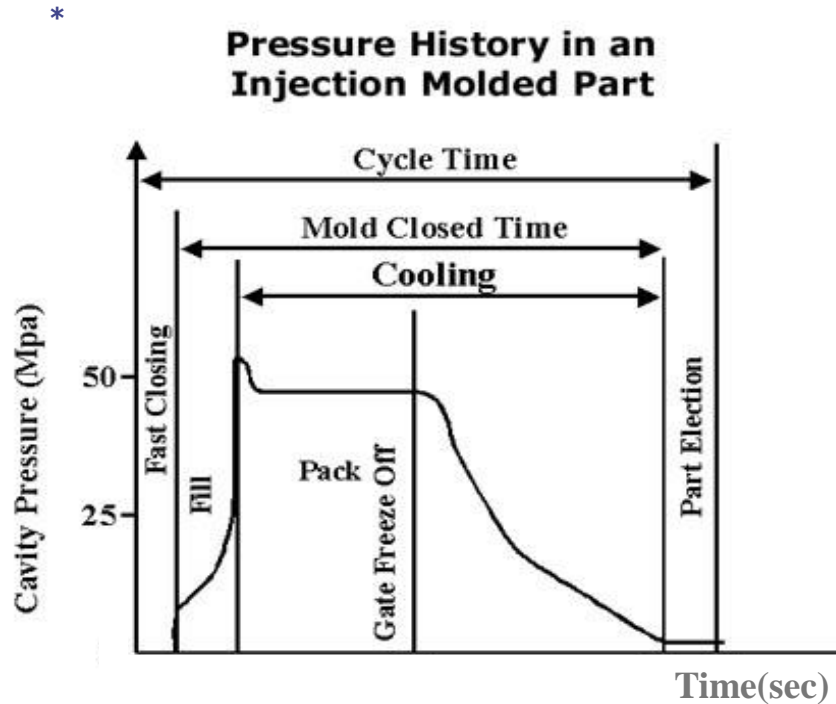
Schematic of thermoplastic Injection molding machine

Process Operation

- ◆ Temperature: barrel zones, tool, die zone
- ◆ Pressures: injection max, hold
- ◆ Times: injection, hold, tool opening
- ◆ Shot size: screw travel



Typical pressure/temperature cycle

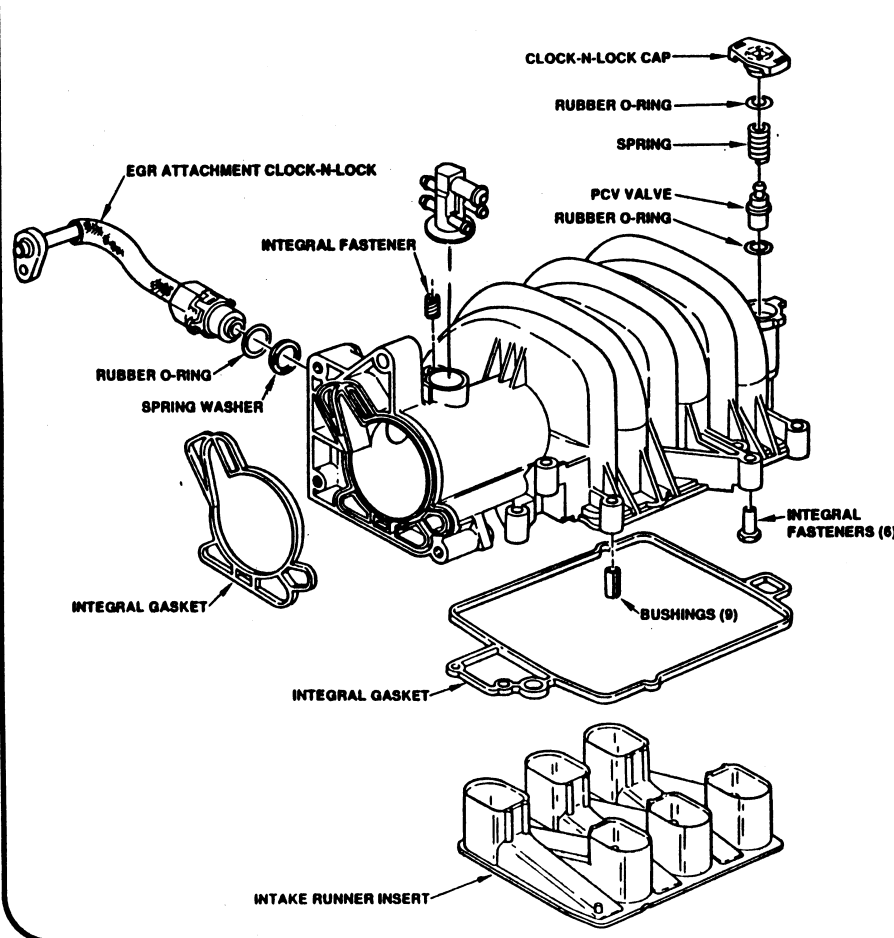


Cooling time generally dominates cycle time

$$t_{cool} = \frac{(half\ thickness)^2}{\alpha}$$

$$\alpha = 10^{-3} \frac{cm^2}{sec} \text{ for polymer}$$

Calculate clamp force, & shot size



$$F = P \times A = 420 \text{ tons}$$

$$3.8 \text{ lbs} = 2245 \text{ cm}^3 \\ = 75 \text{ oz}$$

Actual ; 2 cavity 800 ton

Clamp force and machine cost

Design for Injection Molding

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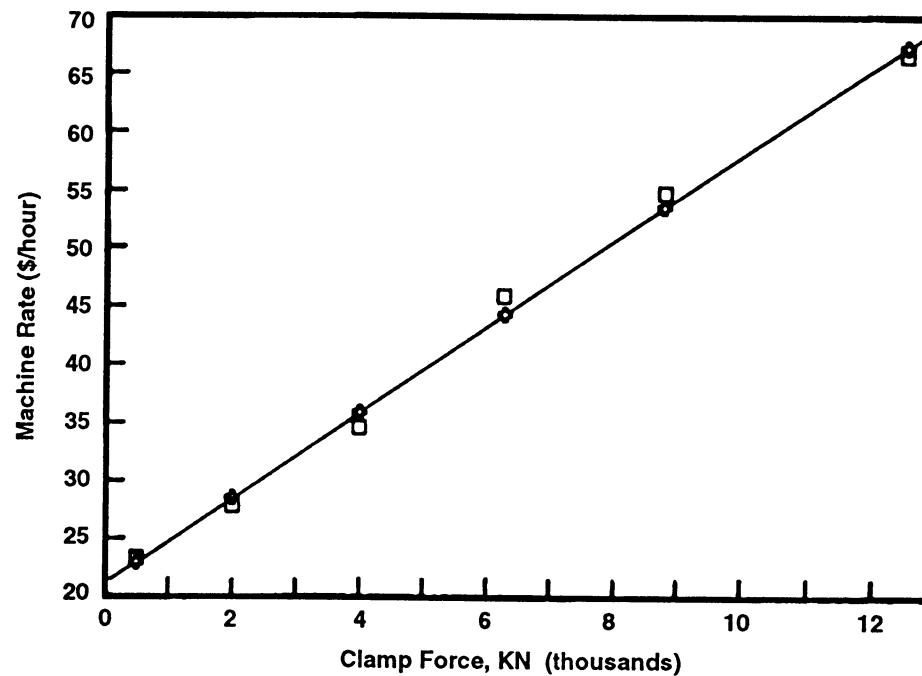
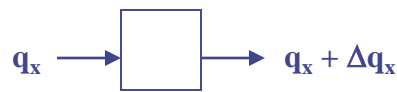


Figure 8.9 National average injection molding machine rates.

Heat transfer

Note; $\alpha_{\text{Tool}} \geq \alpha_{\text{polymer}}$

1-dimensional heat conduction equation :



Fourier's law

$$\frac{\partial}{\partial t} (\rho \cdot c \cdot T) \Delta x \Delta y = - \frac{\partial q_x}{\partial x} \Delta x \Delta y$$

$$q_x = -k \frac{\partial T}{\partial x}$$

$$\rho \cdot c \cdot \frac{\partial T}{\partial t} = k \frac{\partial^2 T}{\partial x^2} \quad \text{or} \quad \frac{\partial T}{\partial t} = \alpha \frac{\partial^2 T}{\partial x^2}$$

Boundary Conditions:

1st kind

$$T(x = x') = \text{constant}$$

2nd kind

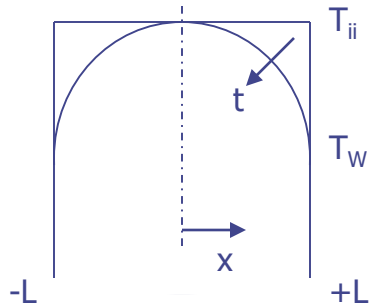
$$-k \frac{\partial T}{\partial x} (x = x') = \text{constant}$$

3rd kind

$$-k \frac{\partial T}{\partial x} (x = x') = \bar{h} (T - T_\infty)$$

The boundary condition of 1st kind applies to injection molding since the tool is often maintained at a constant temperature

Heat transfer



Let $L_{ch} = H/2$ (half thickness) = L ; $t_{ch} = L^2/\alpha$;
 $\Delta T_{ch} = T_i - T_w$ (initial temp. – wall temp.)

Non-dimensionalize: $\theta = \frac{T - T_w}{T_i - T_w}$; $\xi = \frac{x}{L} + 1$; $F_o = \frac{\alpha \cdot t}{L^2}$

Dimensionless equation:

$$\frac{\partial \theta}{\partial F_o} = \frac{\partial^2 \theta}{\partial \xi^2}$$

Initial condition $F_o = 0 \quad \theta = 1$

Boundary condition $\xi = 0 \quad \theta = 0$

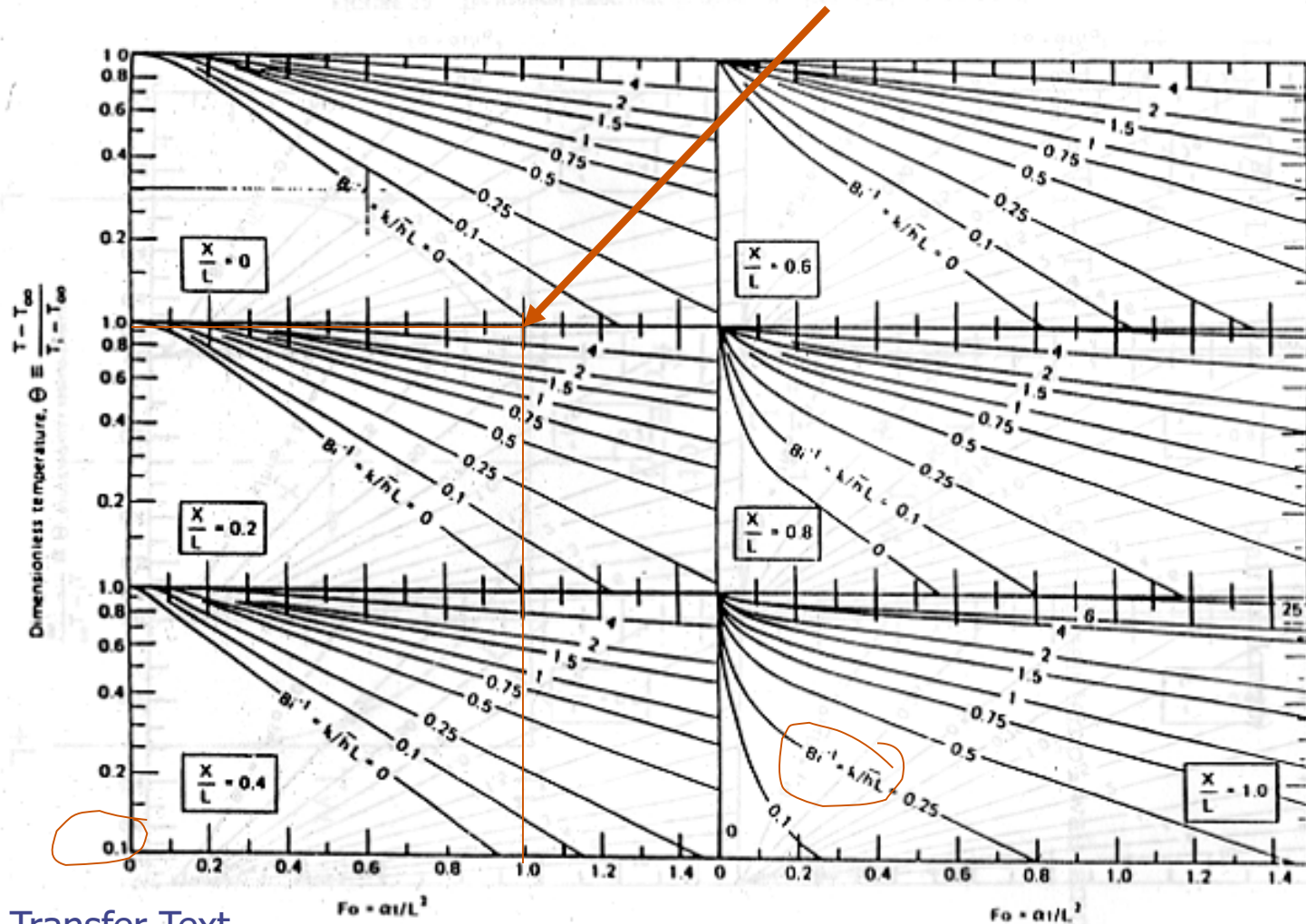
$\xi = 2 \quad \theta = 0$

Separation of variables ;
 matching B.C.; matching I.C.

$$\theta(\xi, F_o) = \sum f(F_o)g(\xi)$$

Temperature in a slab

Centerline, $\theta = 0.1$, $F_o = \alpha t/L^2 = 1$



See Heat Transfer Text
By Lienhard on line

FIGURE 5.7 The transient temperature distribution in a slab at six positions. $x/L = 0$ is the center; $x/L = 1$ is one outside boundary.

$$Bi^{-1} = k/hL$$

Reynolds Number

Reynolds Number:

$$Re = \frac{\frac{\rho V^2}{L} \text{ inertial}}{\mu \frac{V}{L^2} \text{ viscous}} = \frac{\rho V L}{\mu}$$

For typical injection molding

$$\rho = 1 \text{ g/cm}^3 = 10^3 \text{ N/m}^4 / \text{s}^2; \quad L_z = 10^{-3} \text{ m} \quad \text{thickness}$$

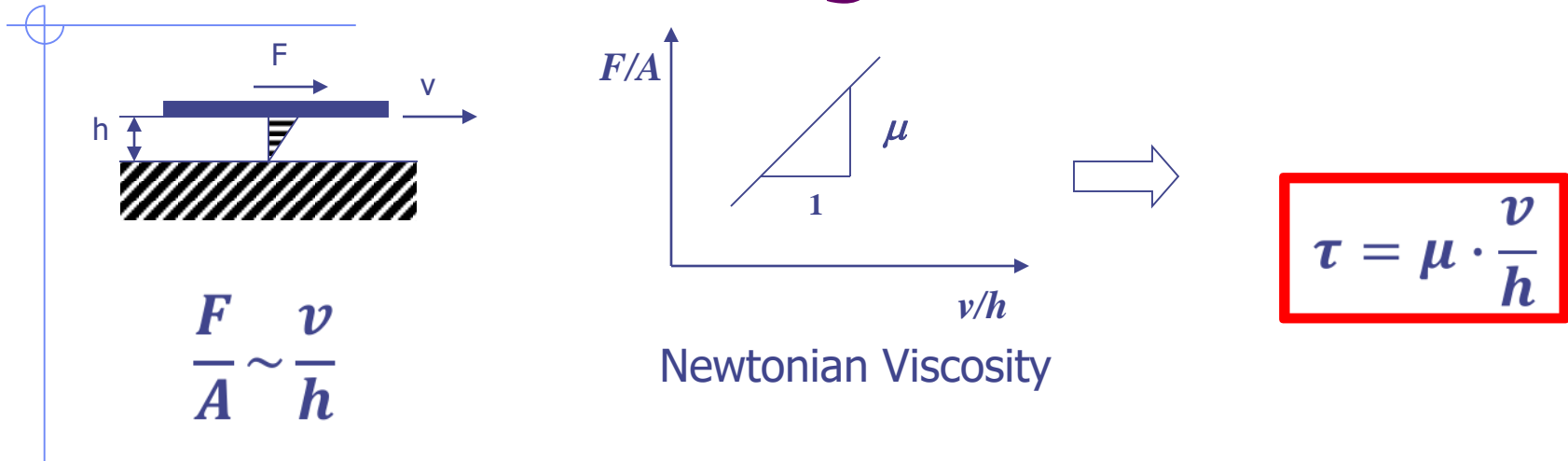
$$V \approx \frac{\text{Part length}}{\text{Fill time}} = \frac{10^{-1}}{1 \text{ s}}; \quad \mu = 10^3 \text{ N} \cdot \text{s/m}^2$$

$$Re \cong 10^{-4}$$

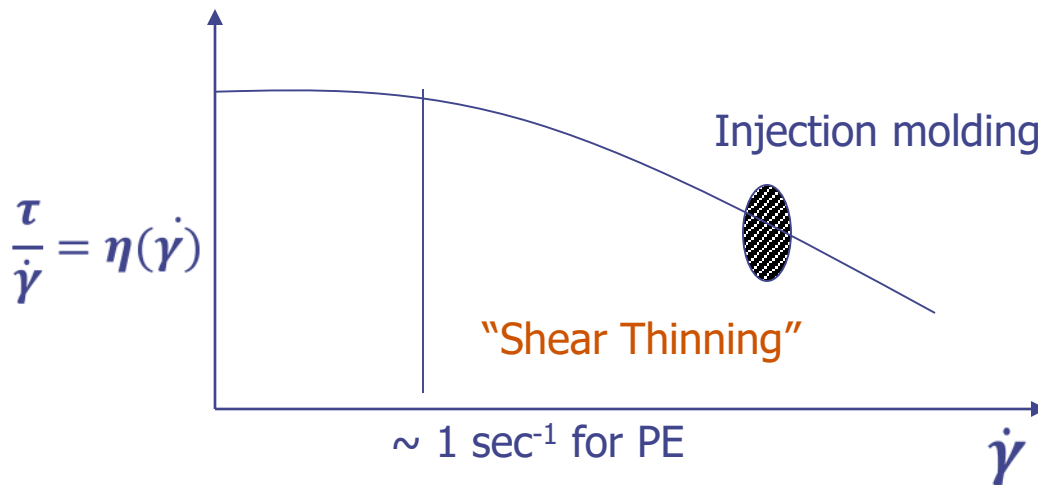
For Die casting

$$Re \approx \frac{3 \cdot 10^3 \times 10^{-1} \times 10^{-3}}{10^{-3}} = 300$$

Viscous Shearing of Fluids



Generalization: $\tau = \mu \cdot \dot{\gamma}$; $\dot{\gamma} = \text{shear rate}$



Typical shear rate for
Polymer processes (sec)⁻¹

Extrusion	$10^2 \sim 10^3$
Calendering	$10 \sim 10^2$
Injection molding	$10^3 \sim 10^4$
Comp. Molding	$1 \sim 10$

Viscous Heating

Rate of Heating
= Rate of Viscous Work

$$\frac{P}{Vol} = \frac{F \cdot v}{Vol} = \frac{F}{A} \cdot \frac{v}{h} = \mu \left(\frac{v}{h} \right)^2$$

Rate of Temperature rise

$$\rho \cdot c \cdot \frac{dT}{dt} = \mu \left(\frac{v}{h} \right)^2 \quad \text{or} \quad \frac{dT}{dt} = \frac{\mu}{\rho \cdot c} \left(\frac{v}{h} \right)^2$$

Rate of Conduction out

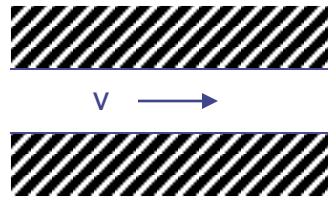
$$\frac{dT}{dt} = \frac{k}{\rho \cdot c} \frac{d^2T}{dx^2} \sim \frac{k}{\rho \cdot c} \frac{\Delta T}{h^2}$$

$$\frac{\text{Viscous heating}}{\text{Conduction}} = \frac{\mu v^2}{k \Delta T}$$

Brinkman number

For injection molding, order of magnitude ~ 0.1 to 10

Non-Isothermal Flow



Flow rate: $1/t \sim V/L_x$

Heat transfer rate: $1/t \sim a/(L_z/2)^2$

Péclet No.

$$\frac{\text{Flow rate}}{\text{Heat xfer rate}} = \frac{V \cdot L_z^2}{4\alpha \cdot L_x} = \frac{1}{4} \frac{VL_z}{\alpha} \cdot \frac{L_z}{L_x}$$

Small value
=> Short shot

For injection molding

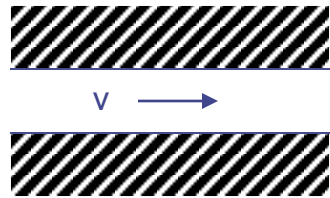
$$\frac{\text{Flow rate}}{\text{Heat xfer rate}} \sim \frac{1}{4} \frac{10 \frac{\text{cm}}{\text{s}} \cdot 0.1 \text{cm}}{10^{-3} \frac{\text{cm}^2}{\text{s}}} \cdot \frac{0.1 \text{cm}}{10 \text{cm}} = 2.5$$

For Die casting of aluminum

$$\frac{\text{Flow rate}}{\text{Heat xfer rate}} \sim \frac{1}{4} \frac{10 \frac{\text{cm}}{\text{s}} \cdot 0.1 \text{cm}}{0.3 \frac{\text{cm}^2}{\text{s}}} \cdot \frac{0.1 \text{cm}}{10 \text{cm}} = 10^{-2}$$

* Very small, therefore it requires thick runners

Non-Isothermal Flow



Flow rate: $1/t \sim V/L_x$

Heat transfer rate: $1/t \sim a/(L_z/2)^2$

Péclet No.

$$\frac{\text{Flow rate}}{\text{Heat xfer rate}} = \frac{V \cdot L_z^2}{4\alpha \cdot L_x} = \frac{1}{4} \frac{VL_z}{\alpha} \cdot \frac{L_z}{L_x}$$

Small value
=> Short shot

For injection molding

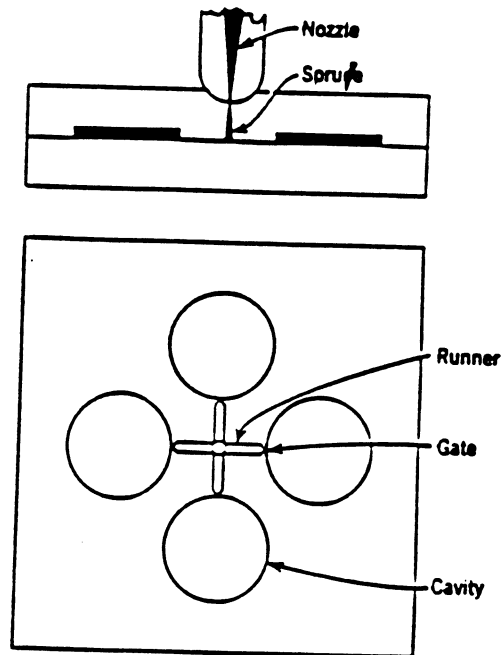
$$\frac{\text{Flow rate}}{\text{Heat xfer rate}} \sim \frac{1}{4} \frac{10 \frac{\text{cm}}{\text{s}} \cdot 0.1 \text{cm}}{10^{-3} \frac{\text{cm}^2}{\text{s}}} \cdot \frac{0.1 \text{cm}}{10 \text{cm}} = 2.5$$

For Die casting of aluminum

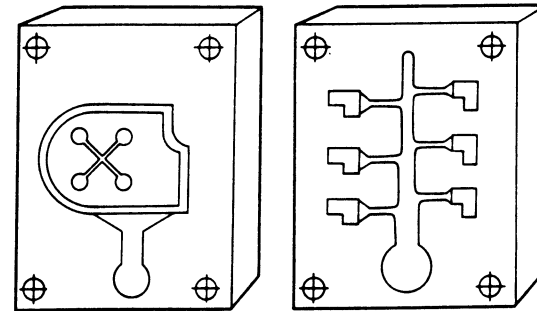
$$\frac{\text{Flow rate}}{\text{Heat xfer rate}} \sim \frac{1}{4} \frac{10 \frac{\text{cm}}{\text{s}} \cdot 0.1 \text{cm}}{0.3 \frac{\text{cm}^2}{\text{s}}} \cdot \frac{0.1 \text{cm}}{10 \text{cm}} = 10^{-2}$$

Very small value for aluminum requires thicker runners

Injection mold

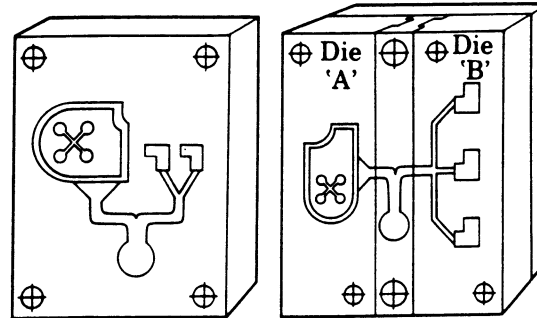


die cast mold



Single-cavity die

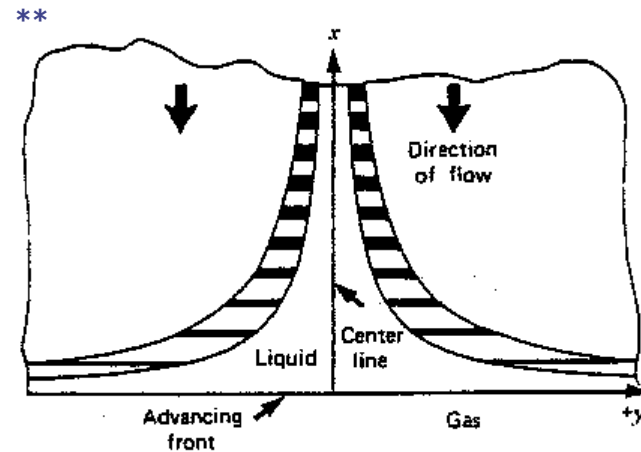
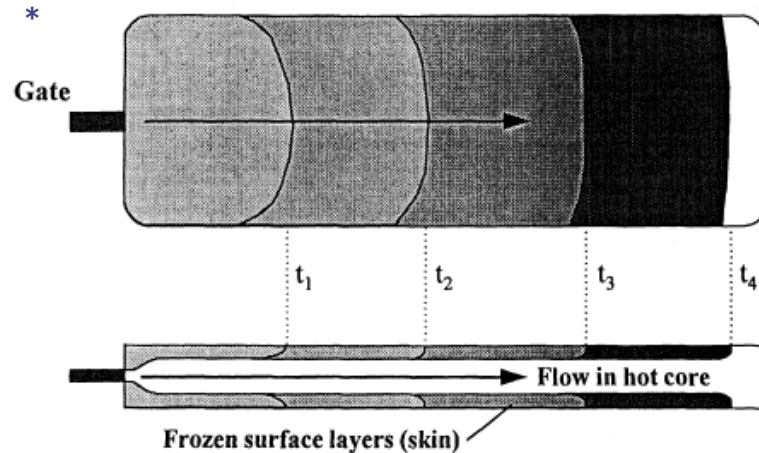
Multiple-cavity die



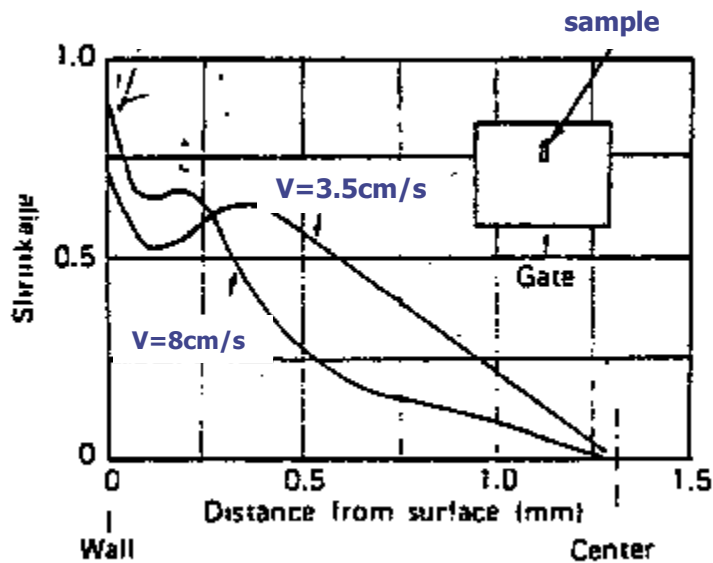
Combination die

Unit die

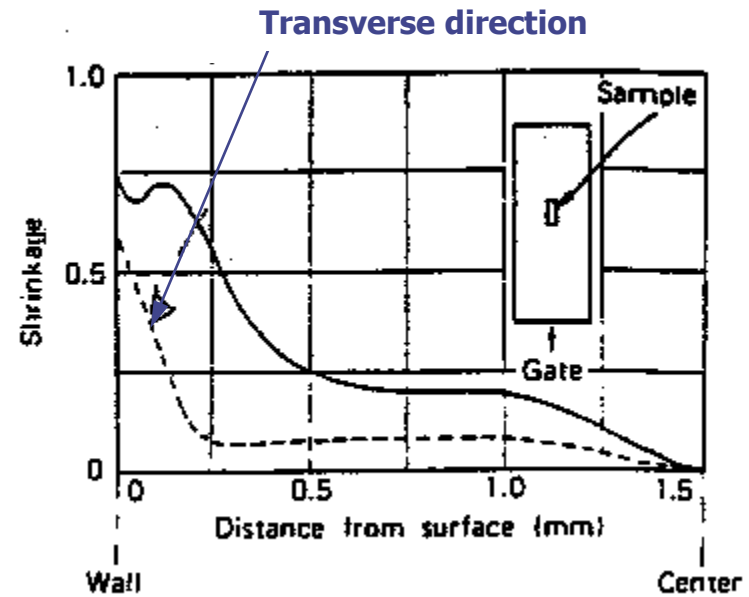
Fountain Flow



Shrinkage distributions

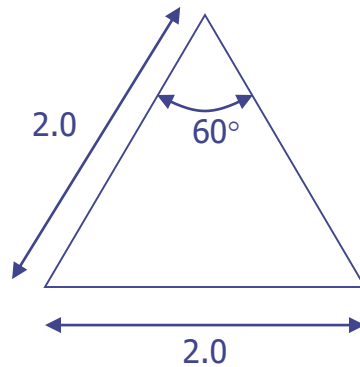
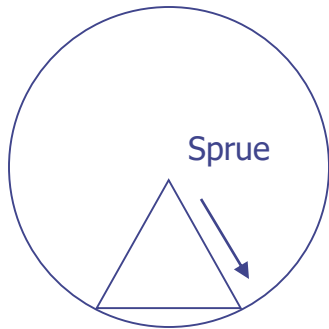


(a)

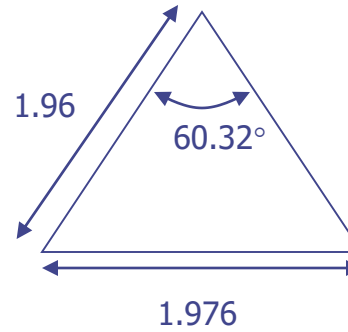


(b)

Gate Location and Warping

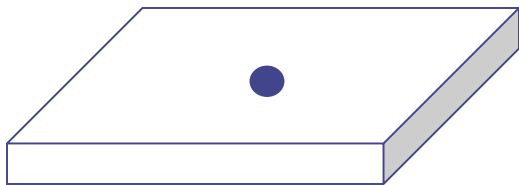


Before shrinkage



After shrinkage

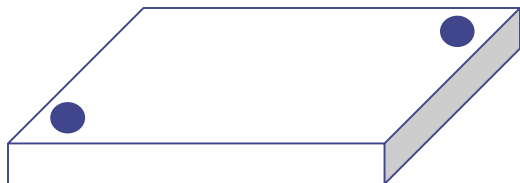
Shrinkage
Direction of flow – 0.020 in/in
Perpendicular to flow – 0.012



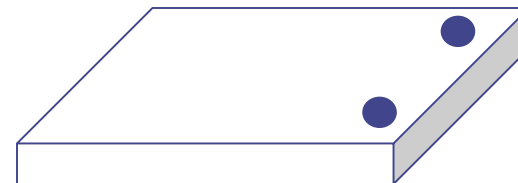
Center gate: radial flow – severe distortion



Edge gate: warp free, air entrapment

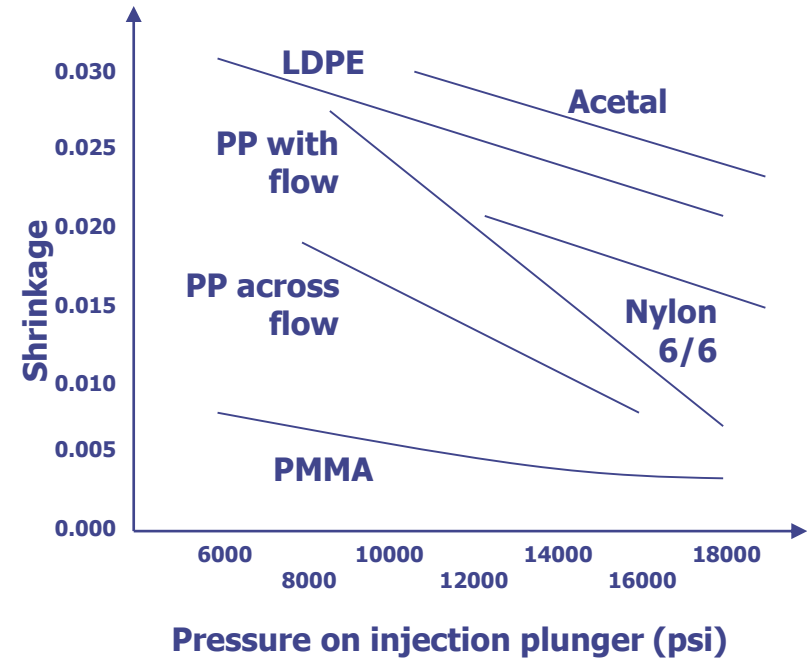
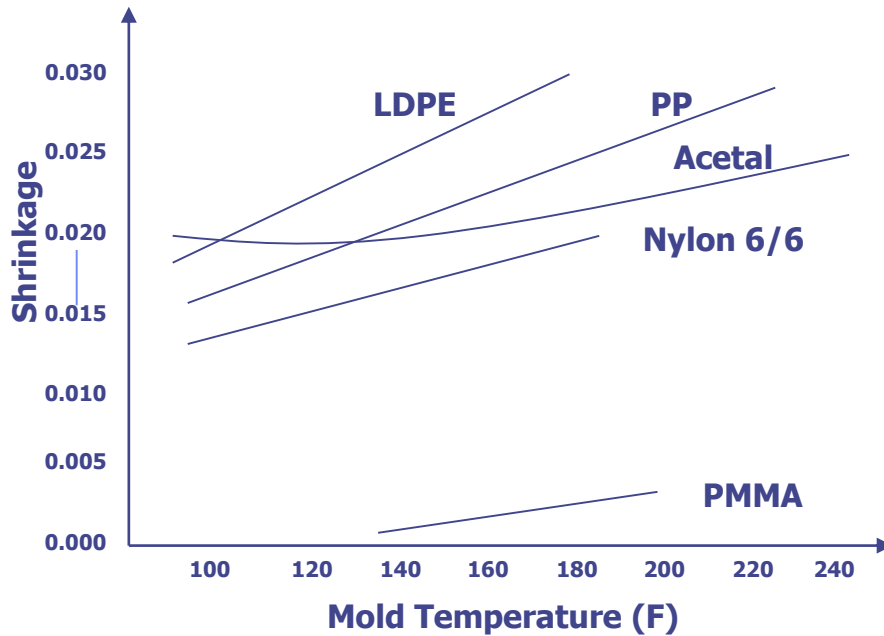


Diagonal gate: radial flow – twisting

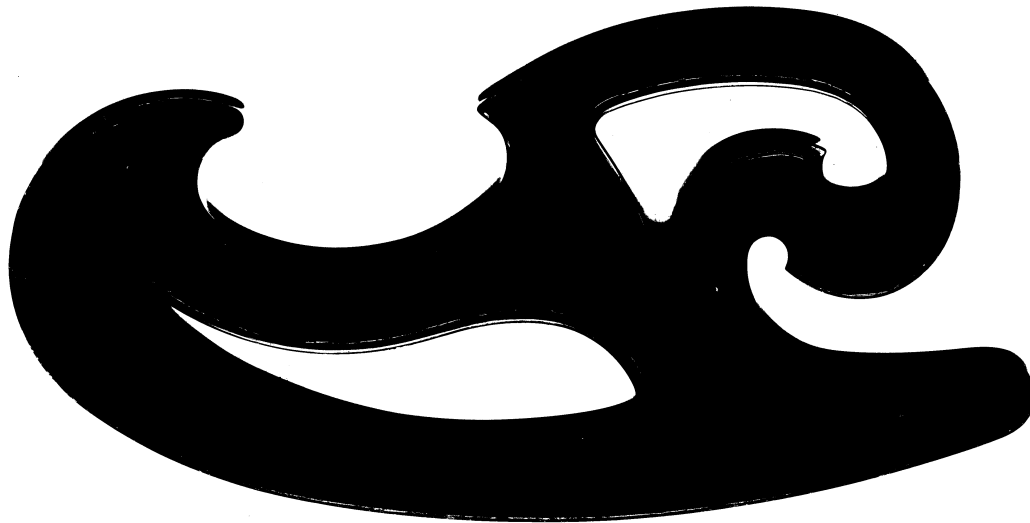


End gates: linear flow – minimum warping

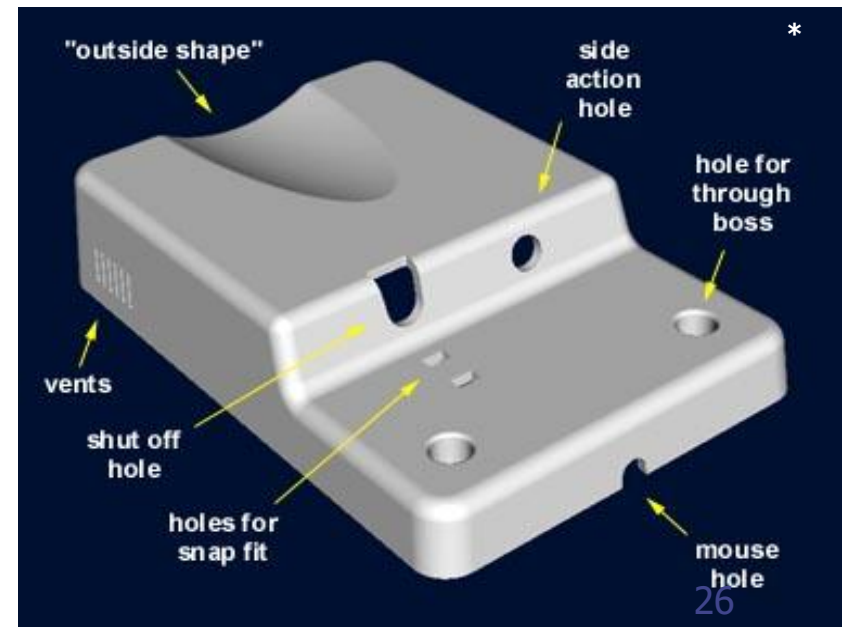
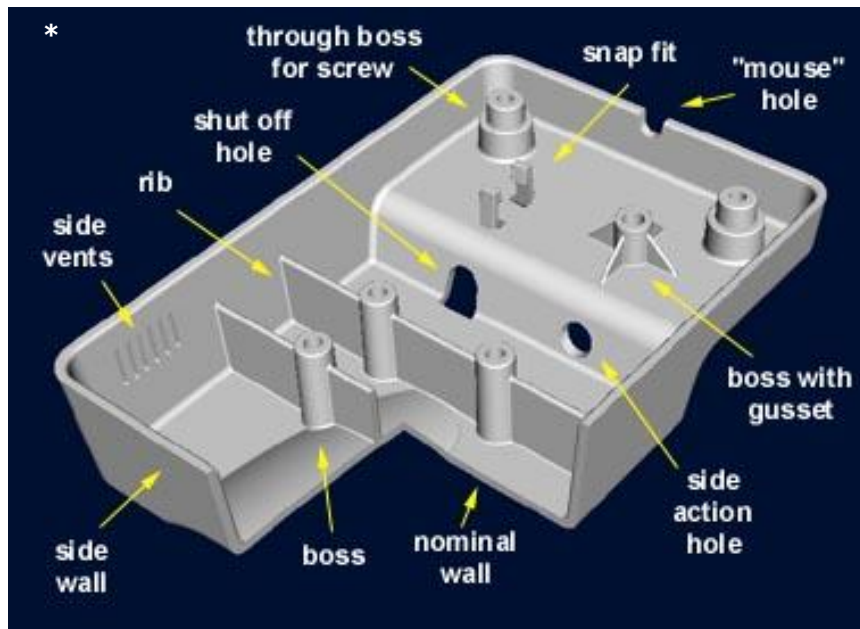
Effects of mold temperature and pressure on shrinkage



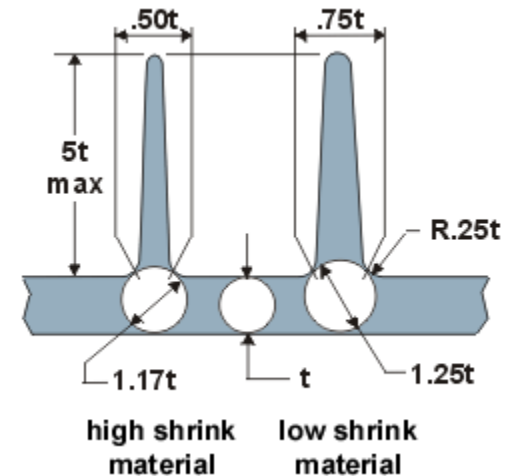
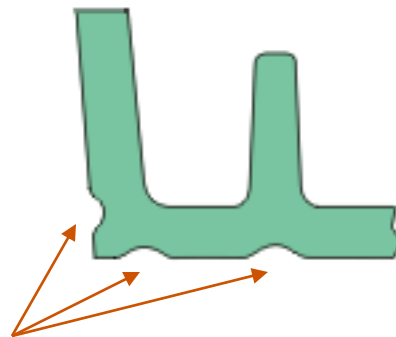
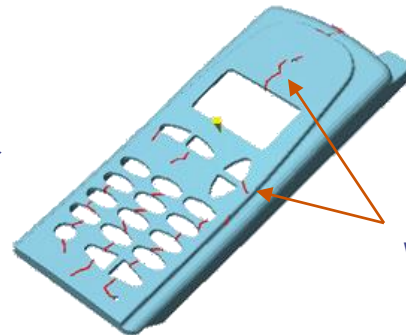
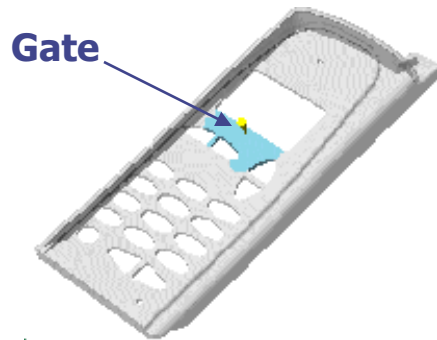
Where would you gate this part?



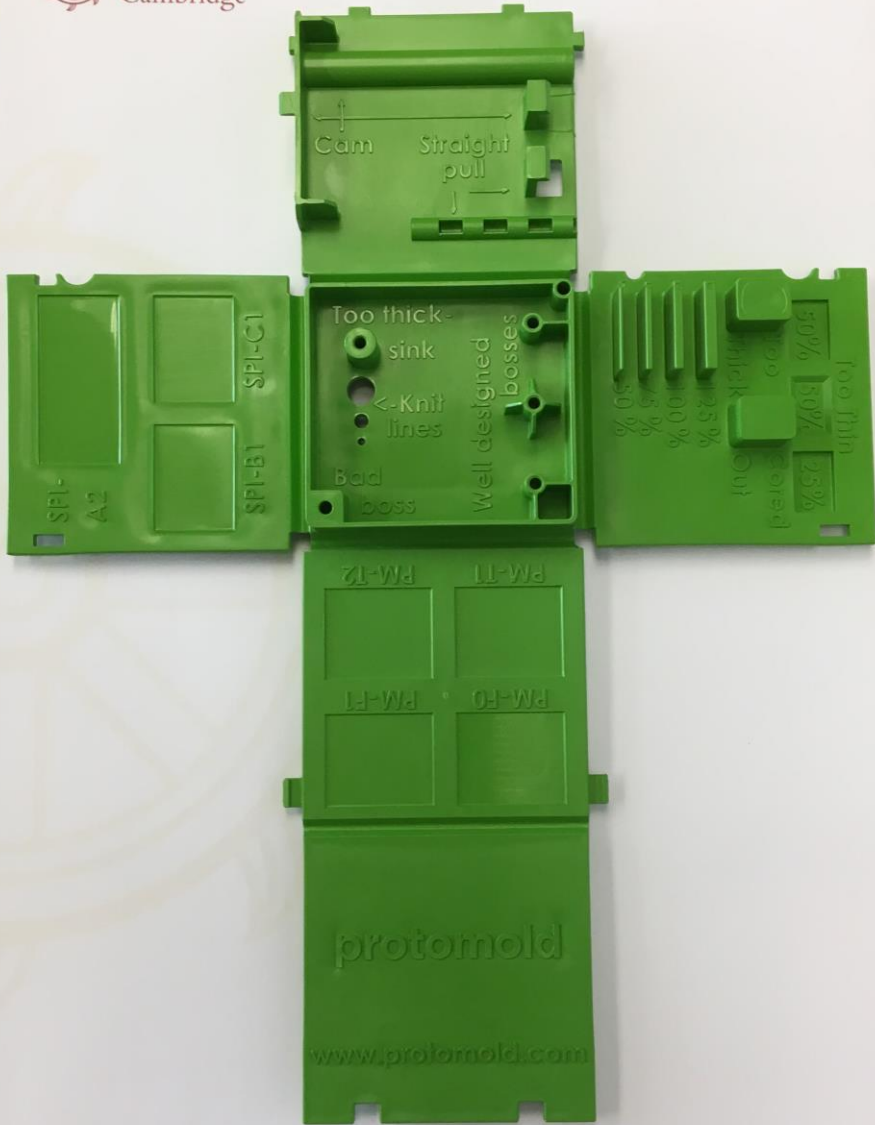
Design Features



Weld line, Sink mark



Basic rules in designing ribs to minimize sink marks 27



DESIGN SUGGESTIONS

- 1 Thick bosses can cause sink on the other side of part.
- 2 Knit lines may form downstream of through-holes.
- 3 Thinner sections may not fill and can cause surface flaws.



- 4 Thicker features can sink, have voids or cause warp.
- 5 Thick ribs can cause sink on the other side of the part.
- 6 Surface finishes:

SPI-A2 High polish, no tool marks (suitable for many applications but not for precision imaging).

SPI-B1 Finished with 600 grit paper; no tool marks.

SPI-C1 Finished with a 600 grit stone; no tool marks.

PM-F0 As-machined or to Protomold discretion (default B-side finish).

PM-F1 Mostly SPI-C1, but evidence of underlying tool marks may still be noticeable in some areas (default A-side finish).

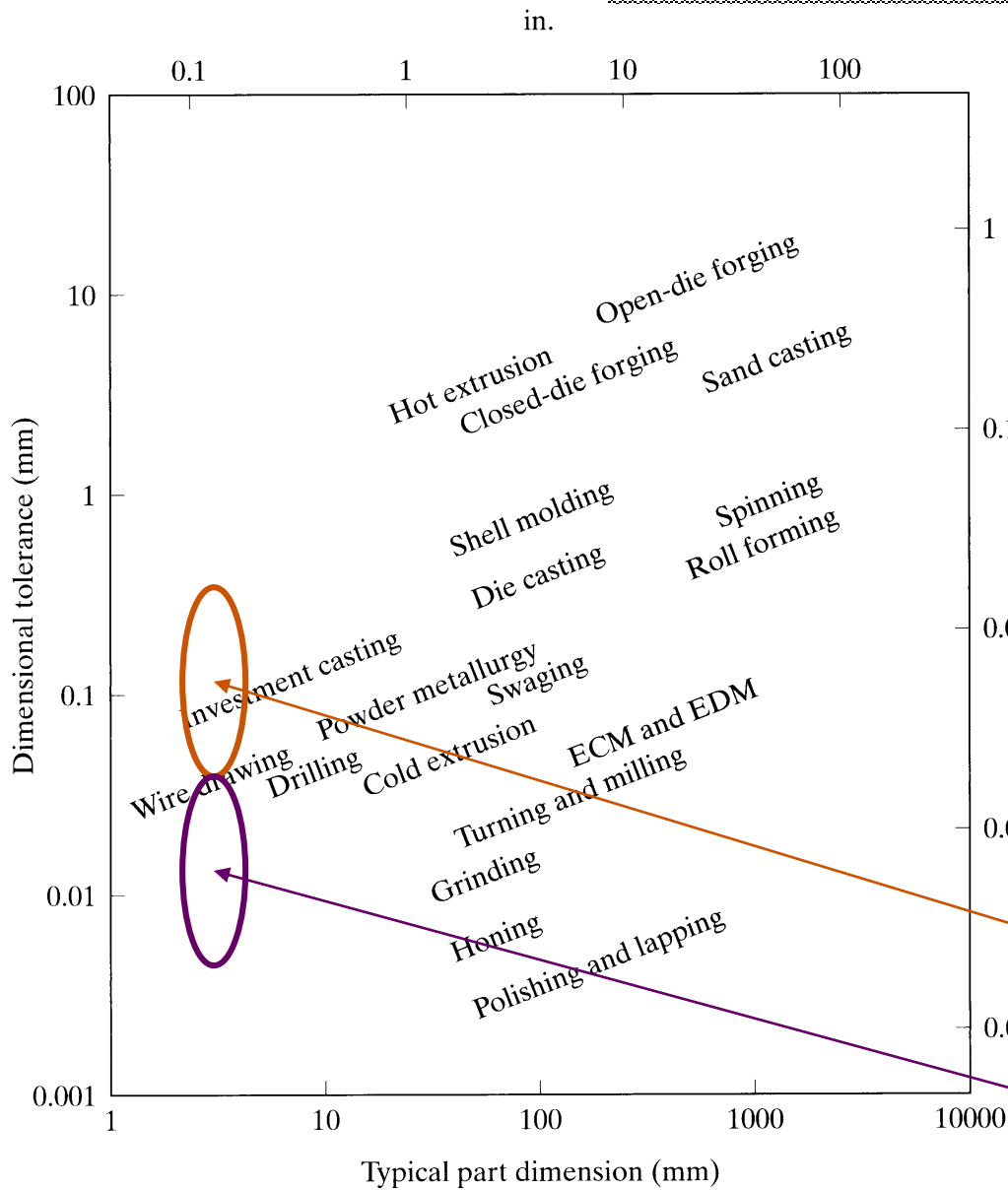
PM-T1 SPI-C1 followed by light bead blast.

PM-T2 SPI-C1 followed by medium bead blast.

- 7 If you incorporate the boss into the wall, do so without undesirable thicker sections.
- 8 Design bosses and ribs to be 40-60% of the wall thickness. Bosses can be strengthened with gussets rather than using thicker walls.
- 9 Tie bosses to walls with short ribs.

- 10 Create undercut features that can be molded using sliding shutoffs in straight-pull molds. Maintain 3 degree minimum draft on shutoffs.
- 11 Core out thick sections.
- 12 Living hinges add functionality but parts can be difficult to fill. They work best in polypropylene or polyethylene.
- 13 Side action cams can create features perpendicular to the main direction of pull. These include holes, hooks, text, texture on side walls, and much more.

Visit www.protomold.com/designguidelines for more tips on design.

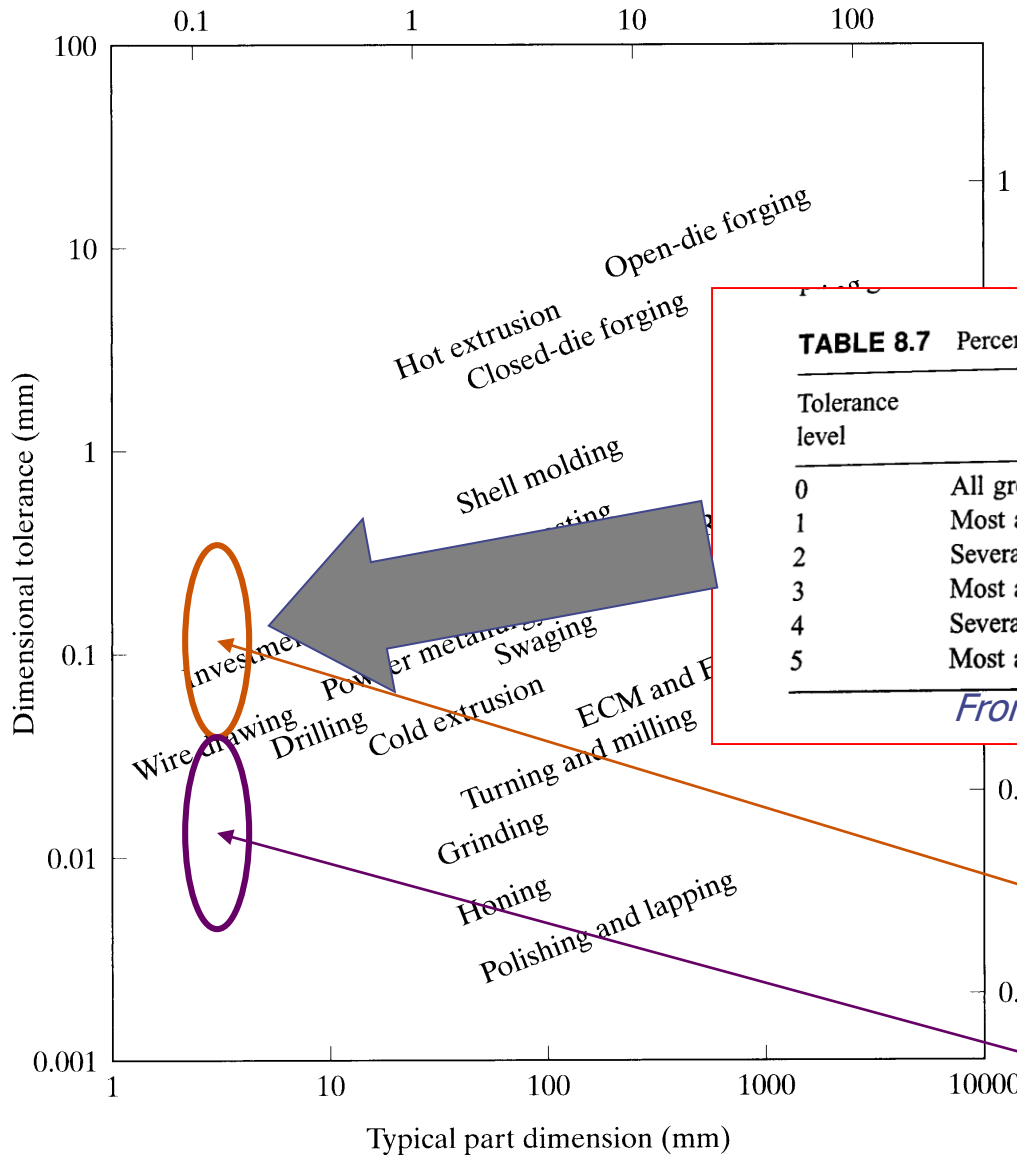


Where is injection molding?

Controlled by shrinkage and warping. Hence, polymer, fillers, mold geometry and processing conditions can all influence the final tolerance.

Shrinkage is of order 10-100/1000 for unfilled and 1-10/1000 for filled across the thickness

in.



Where is injection molding?

TABLE 8.7 Percentage Increases for Tolerance

Tolerance level	Description of tolerances	Percentage increase
0	All greater than ± 0.5 mm	0
1	Most approx. ± 0.35 mm	2
2	Several approx. ± 0.25 mm	5
3	Most approx. ± 0.25 mm	10
4	Several approx. ± 0.05 mm	20
5	Most approx. ± 0.05 mm	30

From Boothroyd et al

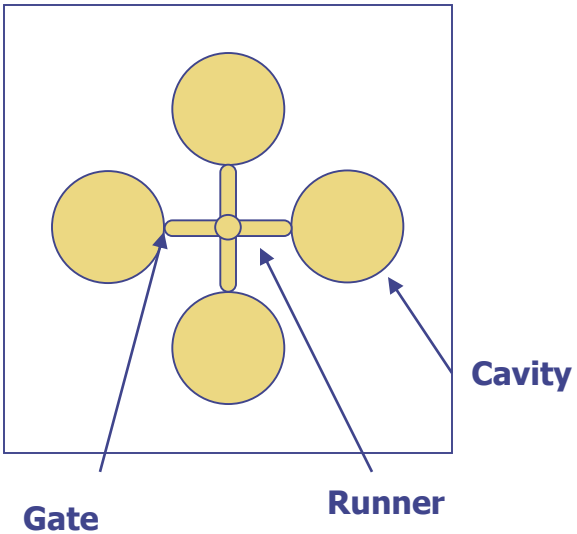
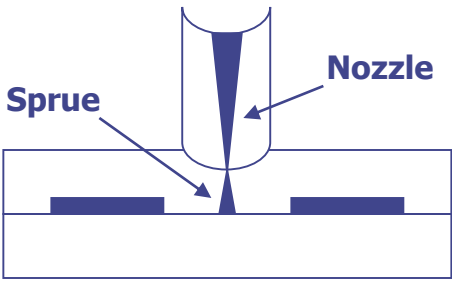
shrinkage
tolerance,
mold
processing
all

influence the final tolerance.

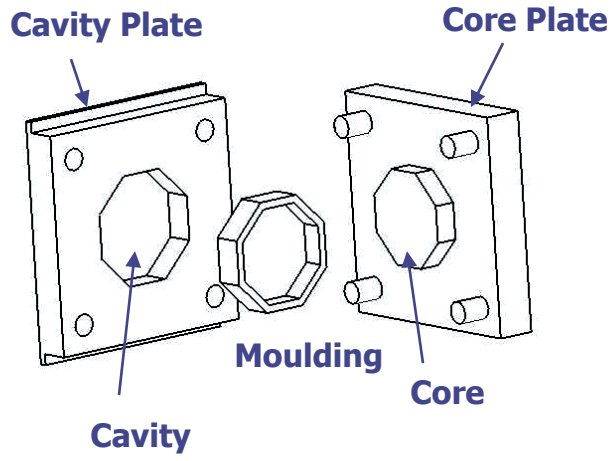
Shrinkage is of order 10-100/1000 for unfilled and

1-10/1000 for filled across the thickness

Tooling Basics

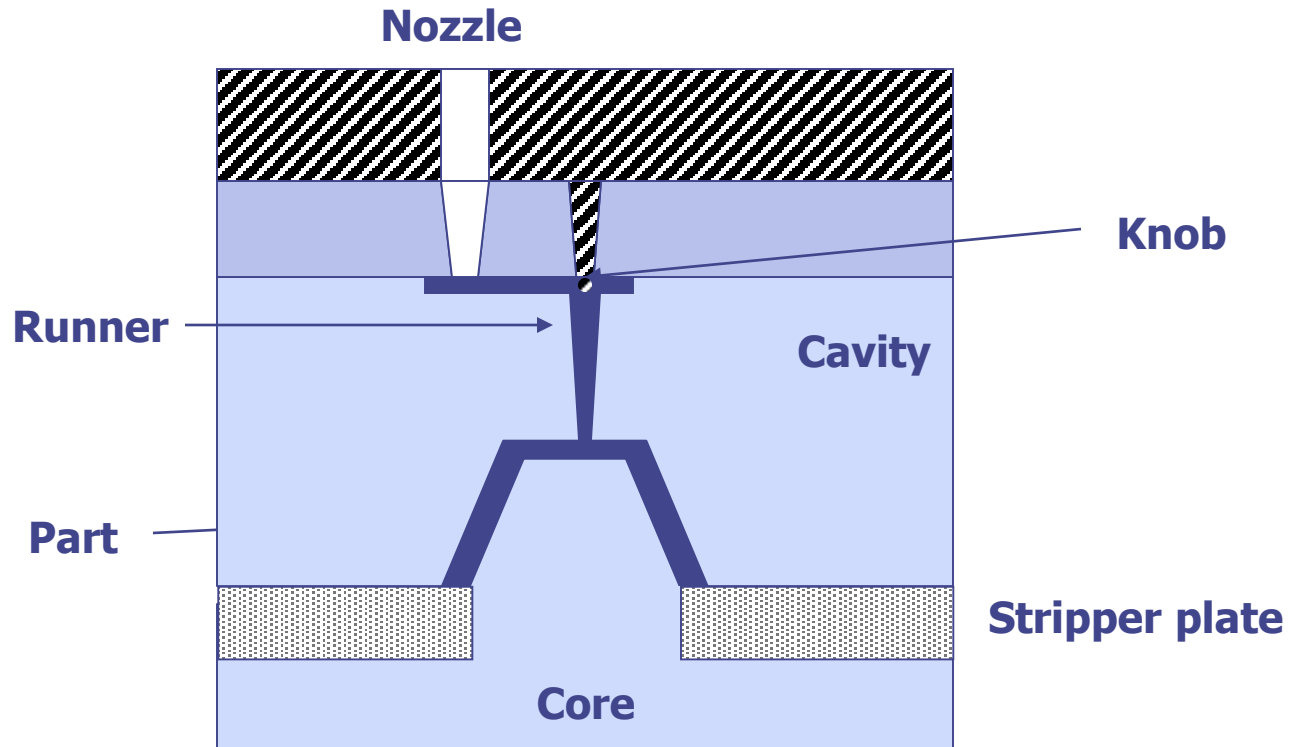


Melt Delivery

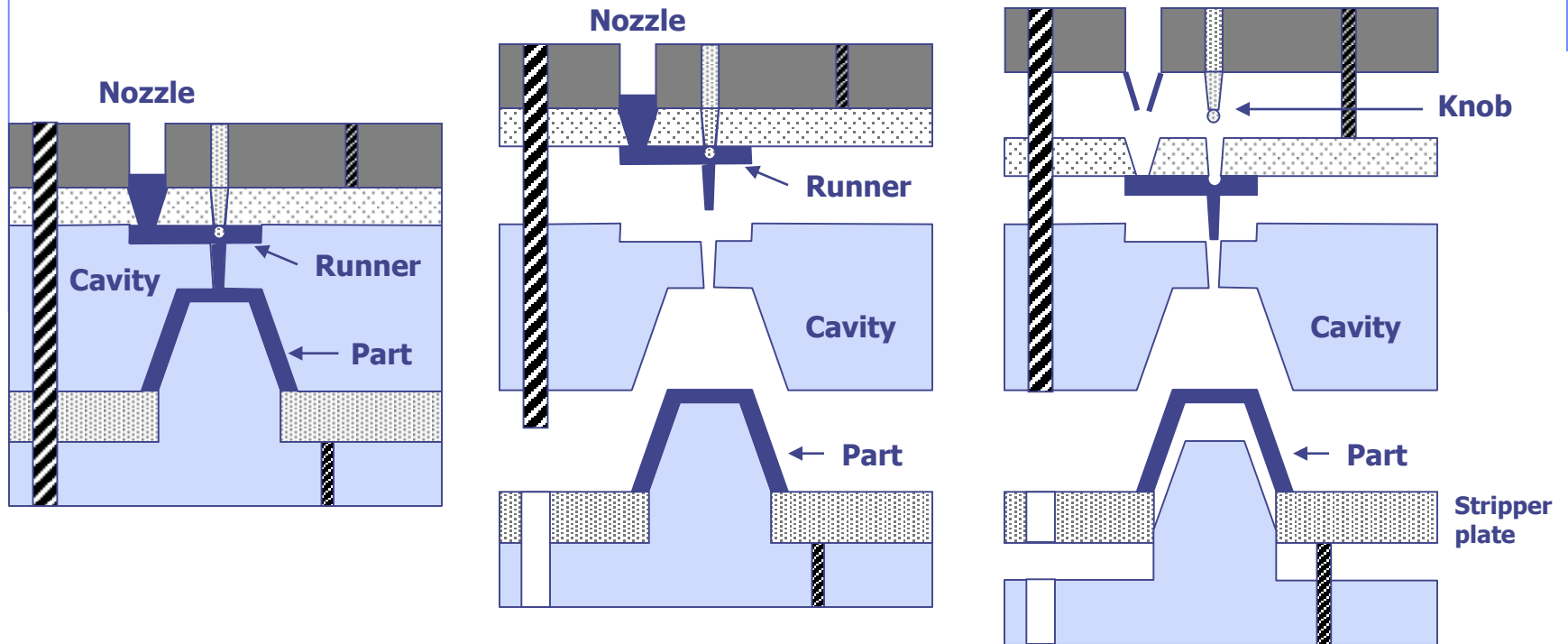
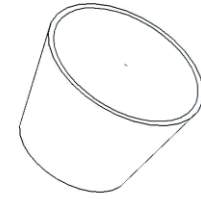


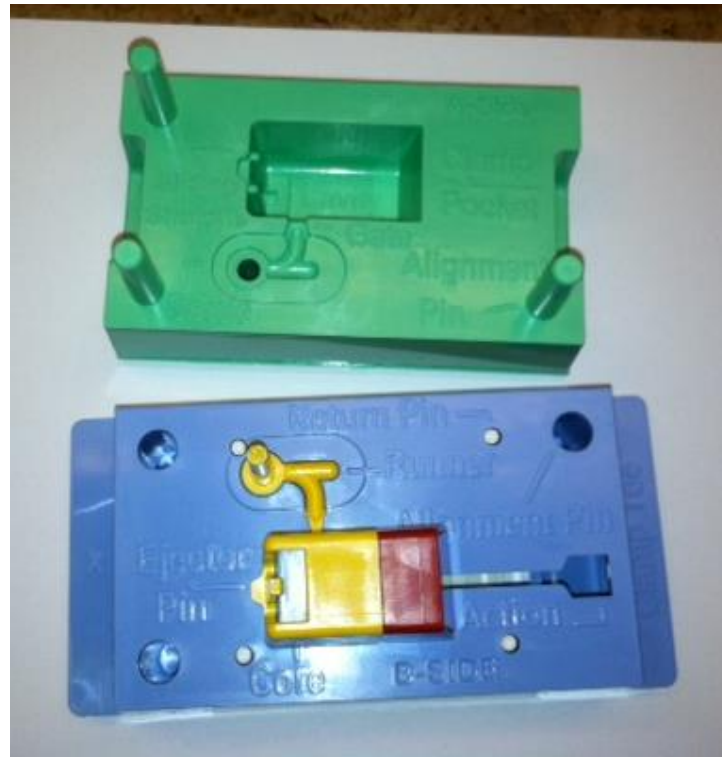
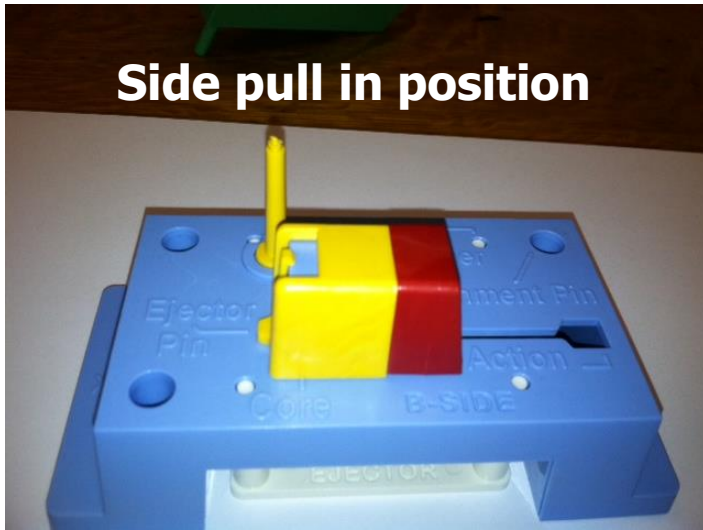
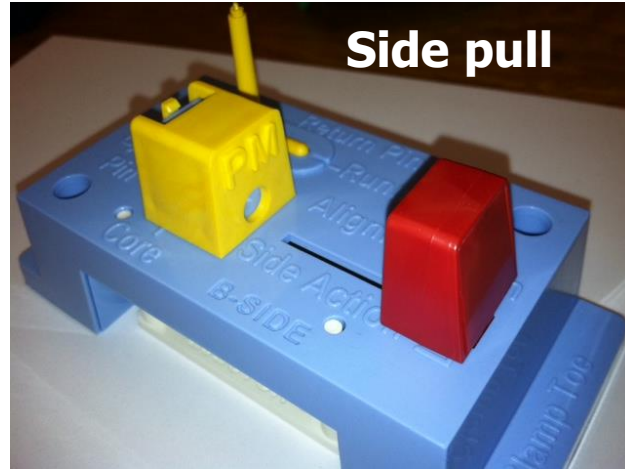
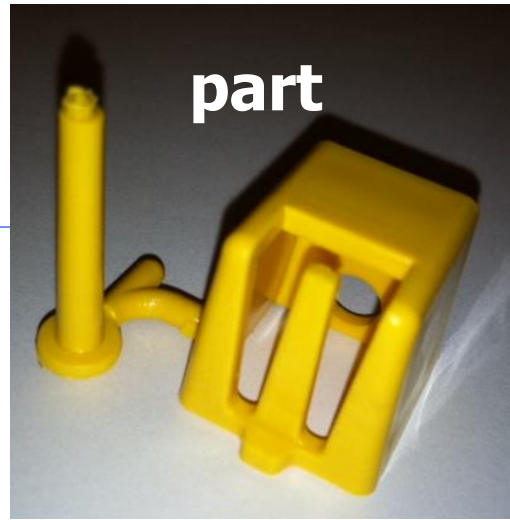
Basic mould consisting of cavity and core plate

Tooling for a plastic cup



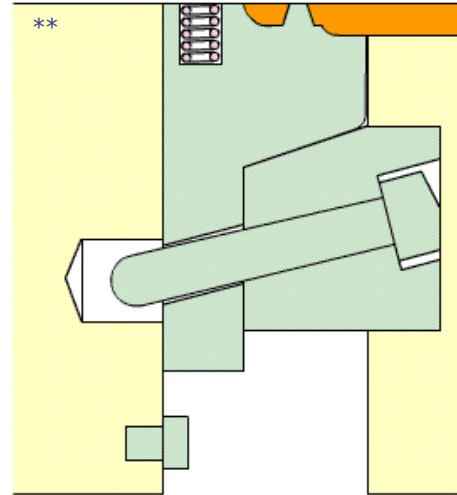
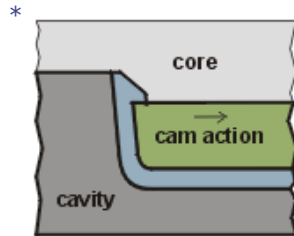
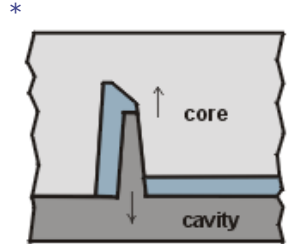
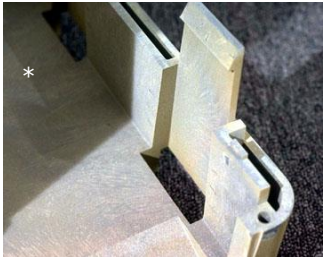
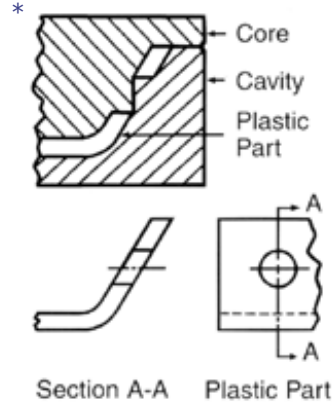
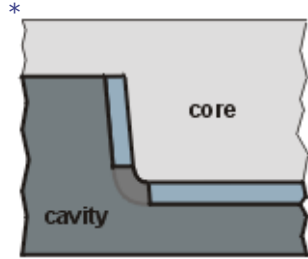
Tooling for a plastic cup





Toy tooling example from Protomold

Tooling



Tooling Alternatives

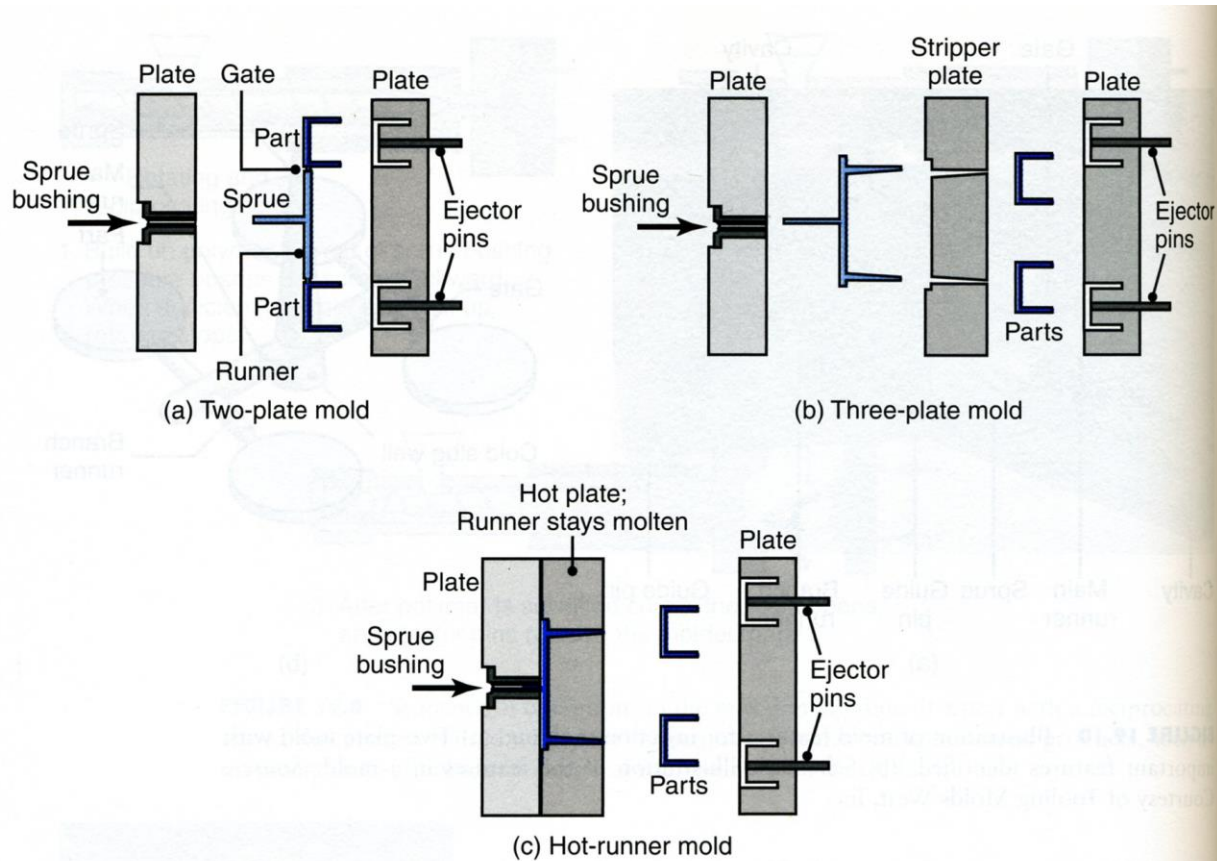


FIGURE 19.11 Types of molds used in injection molding.

Injection Molding Homework

Undercut features to hold tape on

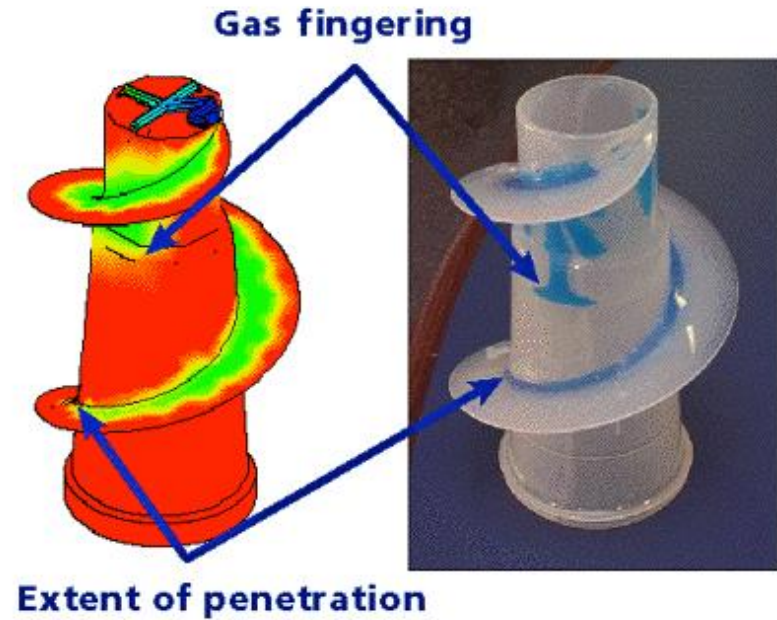
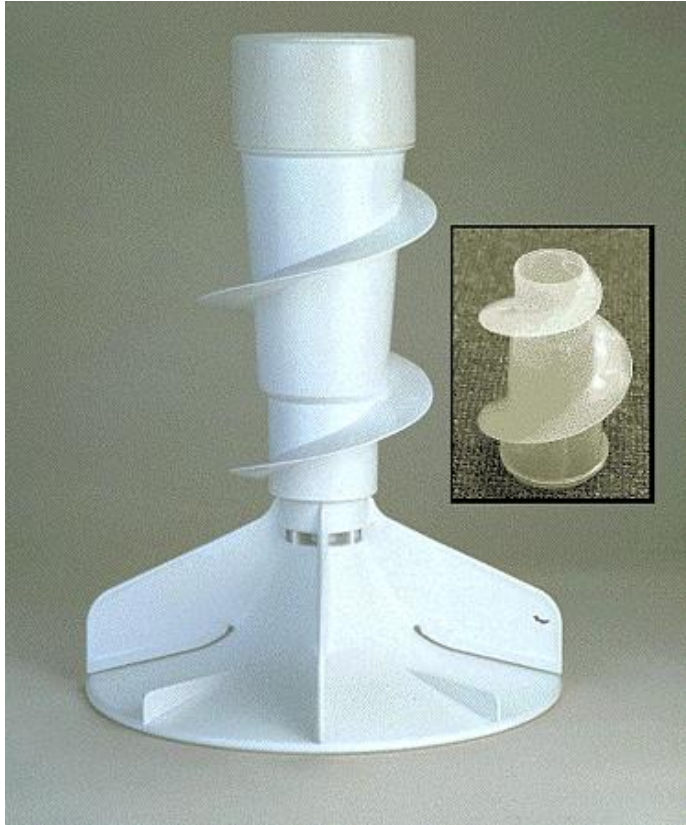


Evidence of tooling feature

Part design rules

- ◆ Simple shapes to reduce tooling cost
 - No undercuts, etc.
- ◆ Draft angle to remove part
 - In some cases, small angles ($1/4^\circ$) will do
 - Problem for gears
- ◆ Even wall thickness
- ◆ Minimum wall thickness ~ 0.025 in
- ◆ Avoid sharp corners
- ◆ Hide weld lines
 - Holes may be molded $2/3$ of the way through the wall only, with final drilling to eliminate weld lines

Novel development- Gas assisted injection molding



Novel development ; injection molding with cores



Injection Molded Housing



Cores used in Injection Molding

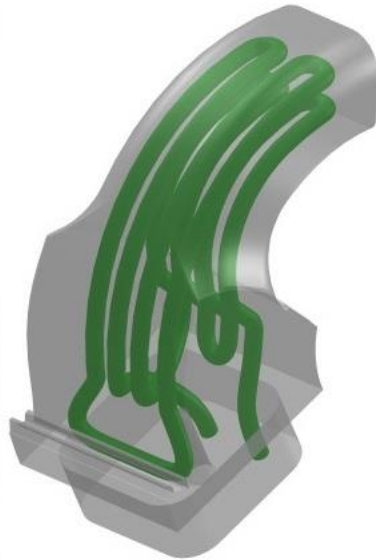


Cores and
Part Molded in Clear Plastic

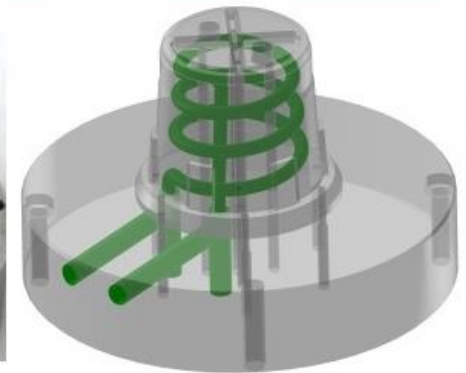
Micro injection molding



Conformal Cooling Channels



Tooling built using
Additive Manufacturing



Innomis.cz

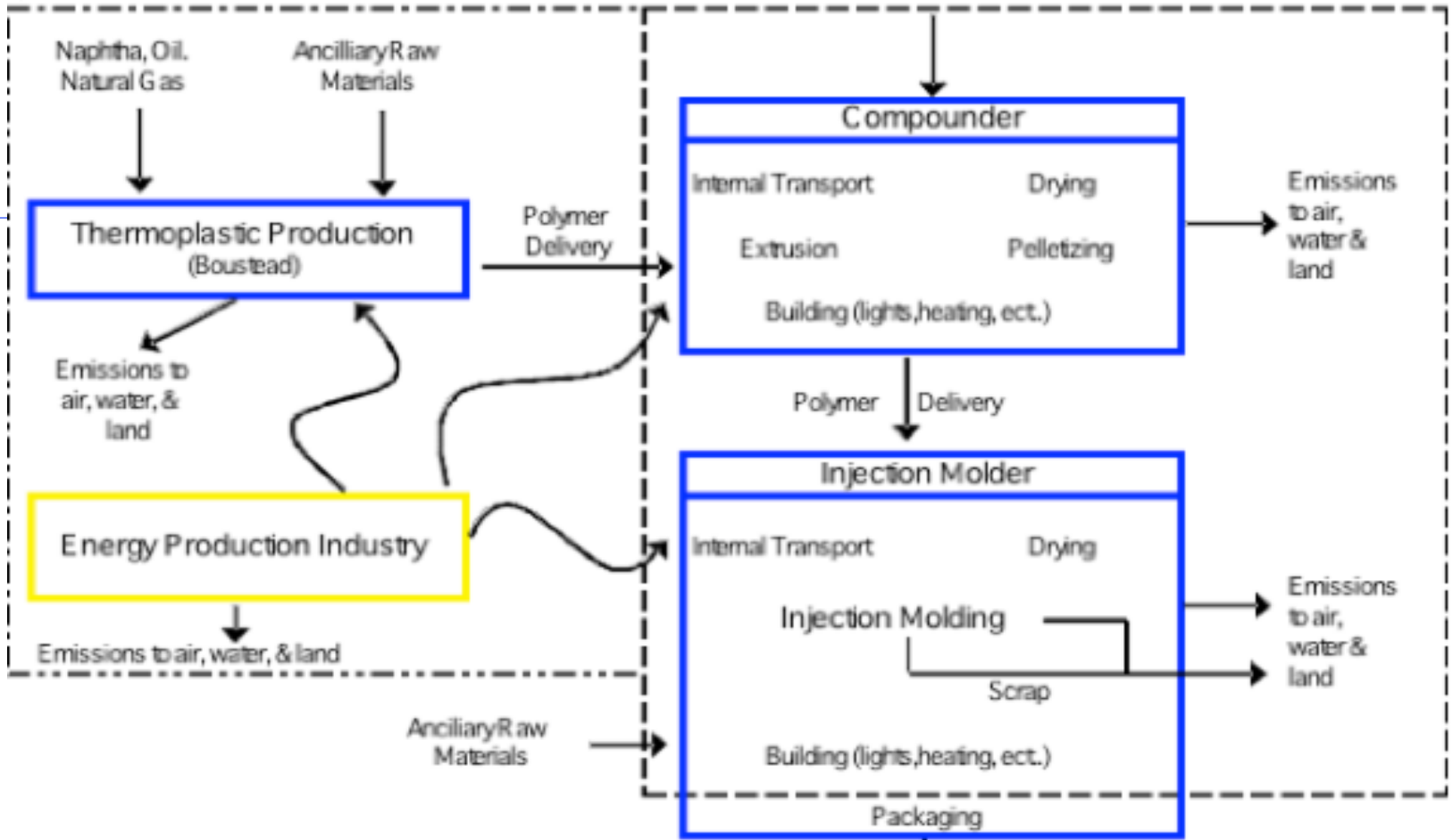
Environmental issues

◆ Energy

- Polymer production
- Compounding
- Machine types

◆ Recycling

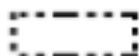
CRADLE



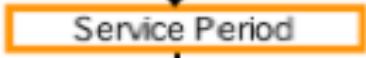
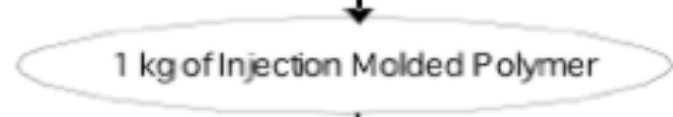
Note to Reader:



= Focus of this Analysis



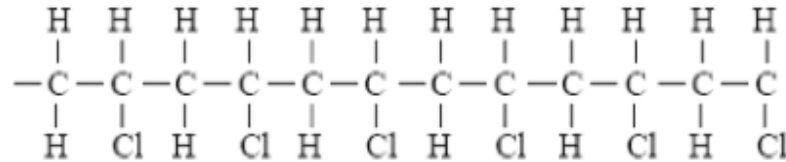
= Also included in the Paper



Polymer Production

Largest Player in the Injection Molding LCI

What is a polymer:



How much energy does it take to make 1 kg of polymer = a lot !!!

Sources	HDPE	LLDPE	LDPE	PP	PVC	PS	PC	PET
Boustead	76.56	77.79	73.55	72.49	58.41	86.46	115.45	77.14
Ashby	111.50	—	92.00	111.50	79.50	118.00	—	—
Patel	—	—	64.60	—	53.20	70.80	80.30	59.40
Kindler/Nickles [Patel 1999]	—	—	71.00	—	53.00	81.00	107.00	96.00
Worrell et al. [Patel 1999]	—	—	67.80	—	52.40	82.70	78.20	—
E ³ Handbook [OIT 1997]	131.65	121.18	136.07	126.07	33.24	—	—	—
Energjeweb	80.00	—	68.00	64.00	57.00	84.00	—	81.00

Values are in MJ per kg of polymer produced. Thiriez '06

↑
 Gold ~ 250 GJ/kg

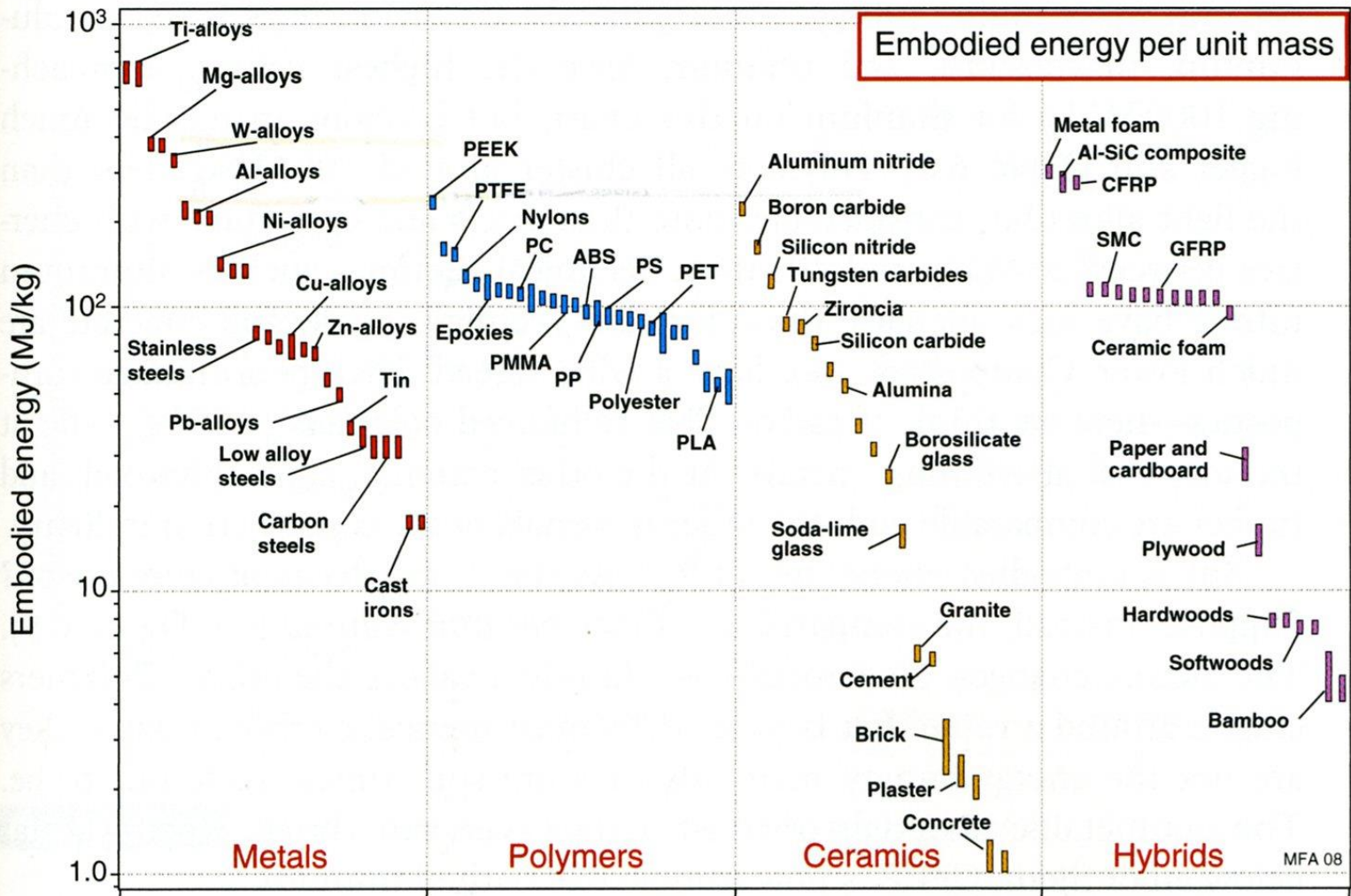


FIGURE 6.8 A bar chart of the embodied energies of materials per unit mass.

Compounding - extrusion

- ◆ An extruder is used to mix additives with a polymer base, to bestow the polymer with the required characteristics.
- ◆ Similar to an injection molding machine, but without a mold and continuous production.
- ◆ Thus it has a similar energy consumption profile.

Environmentally Unfriendly Additives:

- Fluorinated blowing agents (GHG's)
- Phalates (some toxic to human liver, kidney and testicles)
- Organotin stabilizers (toxic and damage marine wildlife)



Injection Molding Process

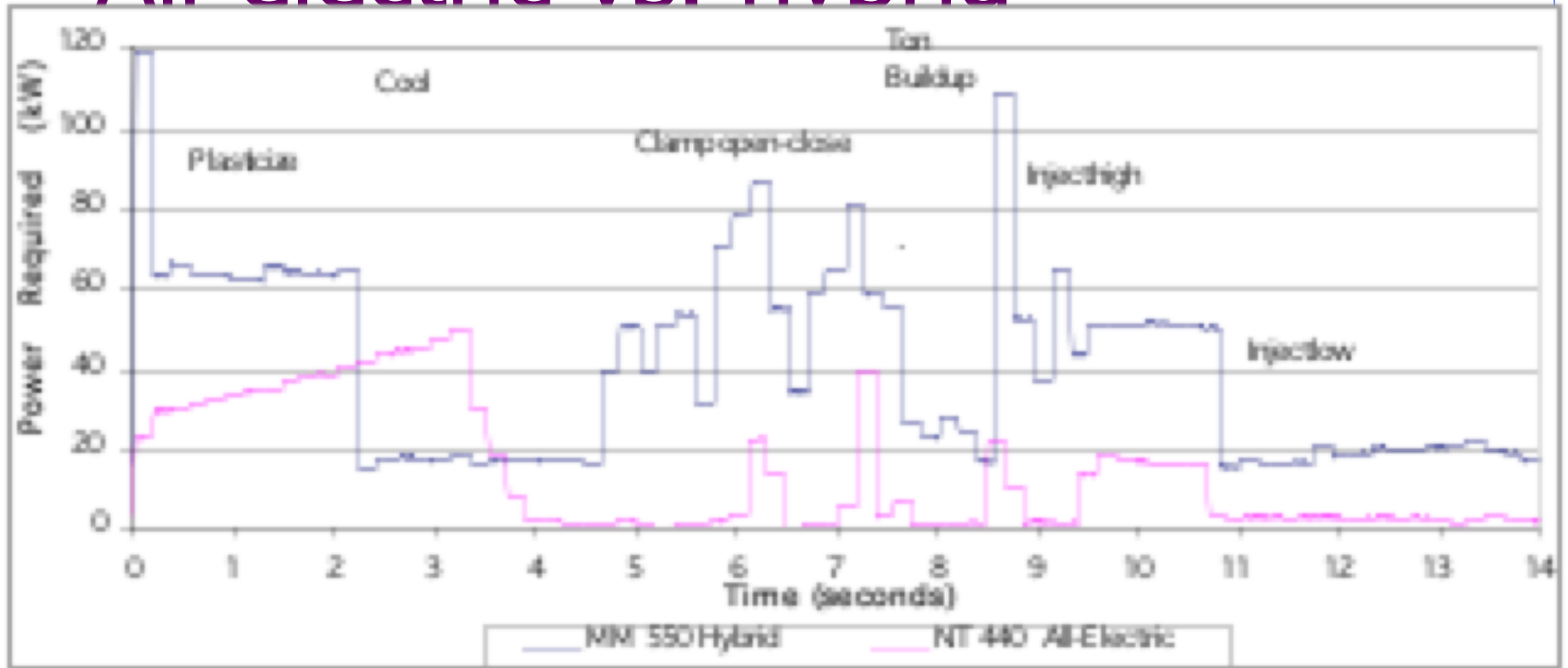


Source:

<http://cache.husky.ca/pdf/ brochures/br-hylectric03a.pdf>

Machine types: Hydraulic, electric, hydro-electric

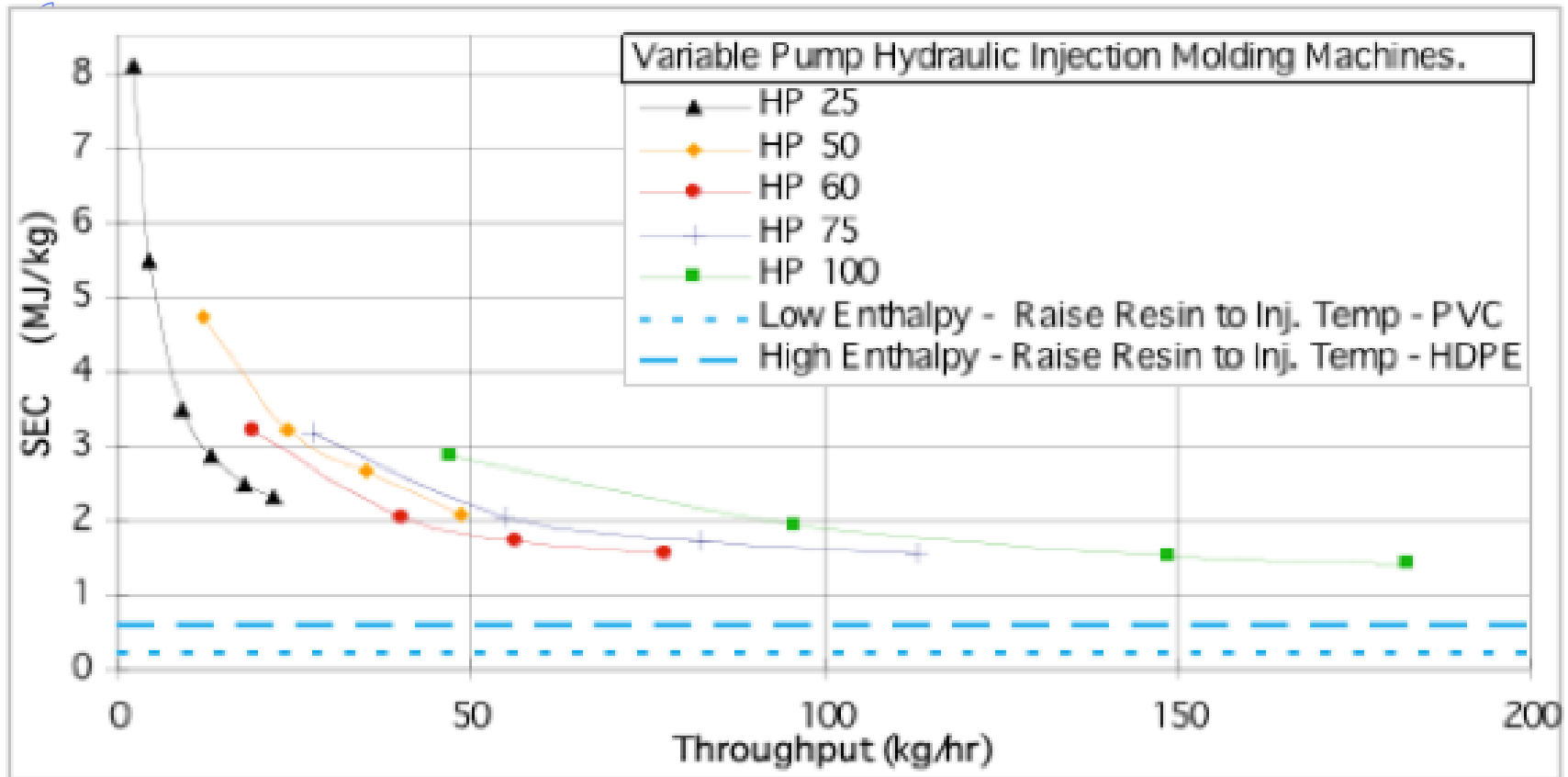
All-electric vs. hybrid



Source: [Thiriez]

The hydraulic plot would be even higher than the hybrid curve

For Hydraulics and Hybrids as throughput increases, SEC \rightarrow k.



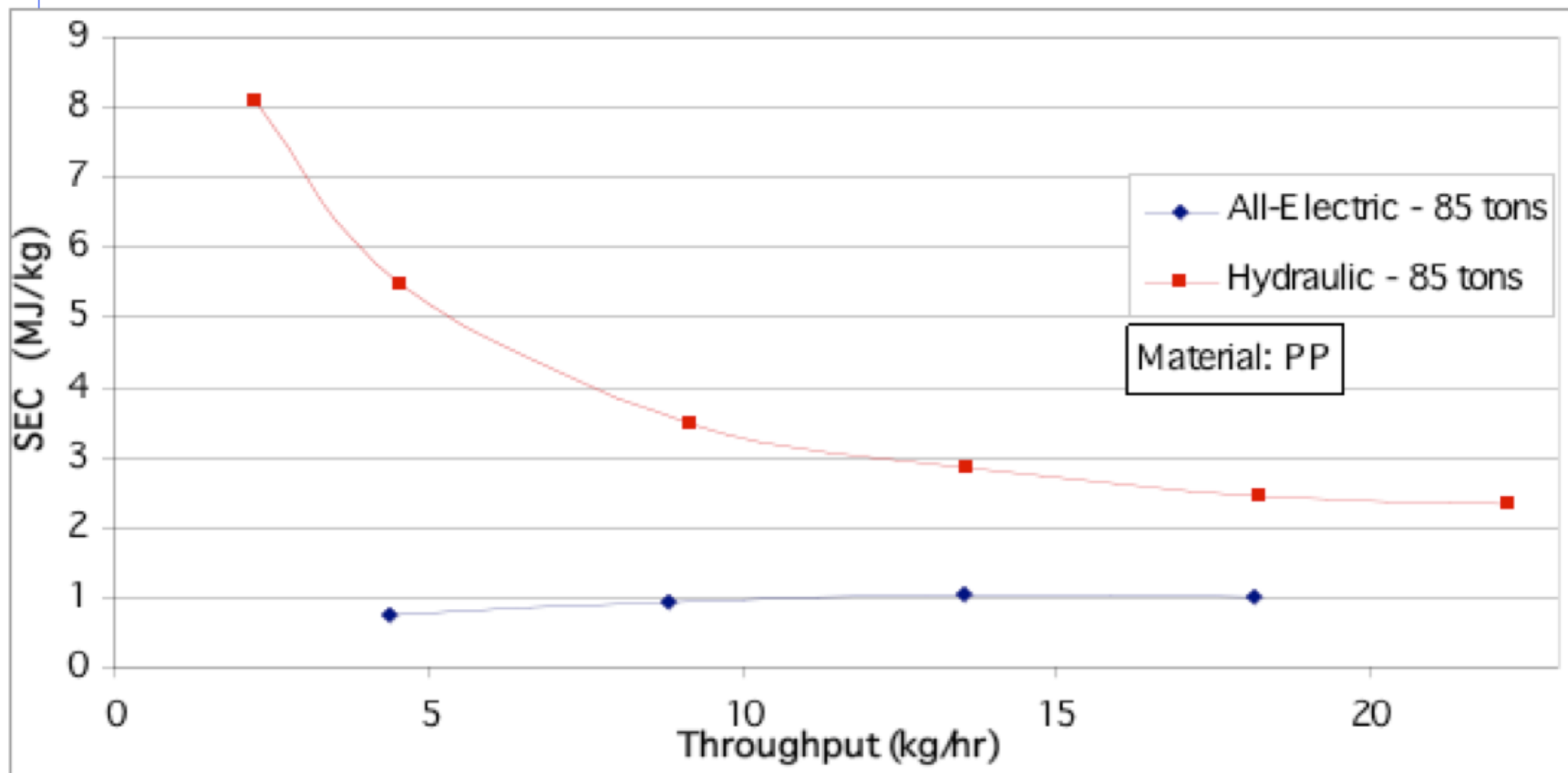
Does not account for the electric grid.

Source: [Thiriez]

Enthalpy value to melt plastics is just 0.1 to 0.7 MJ/kg !!!

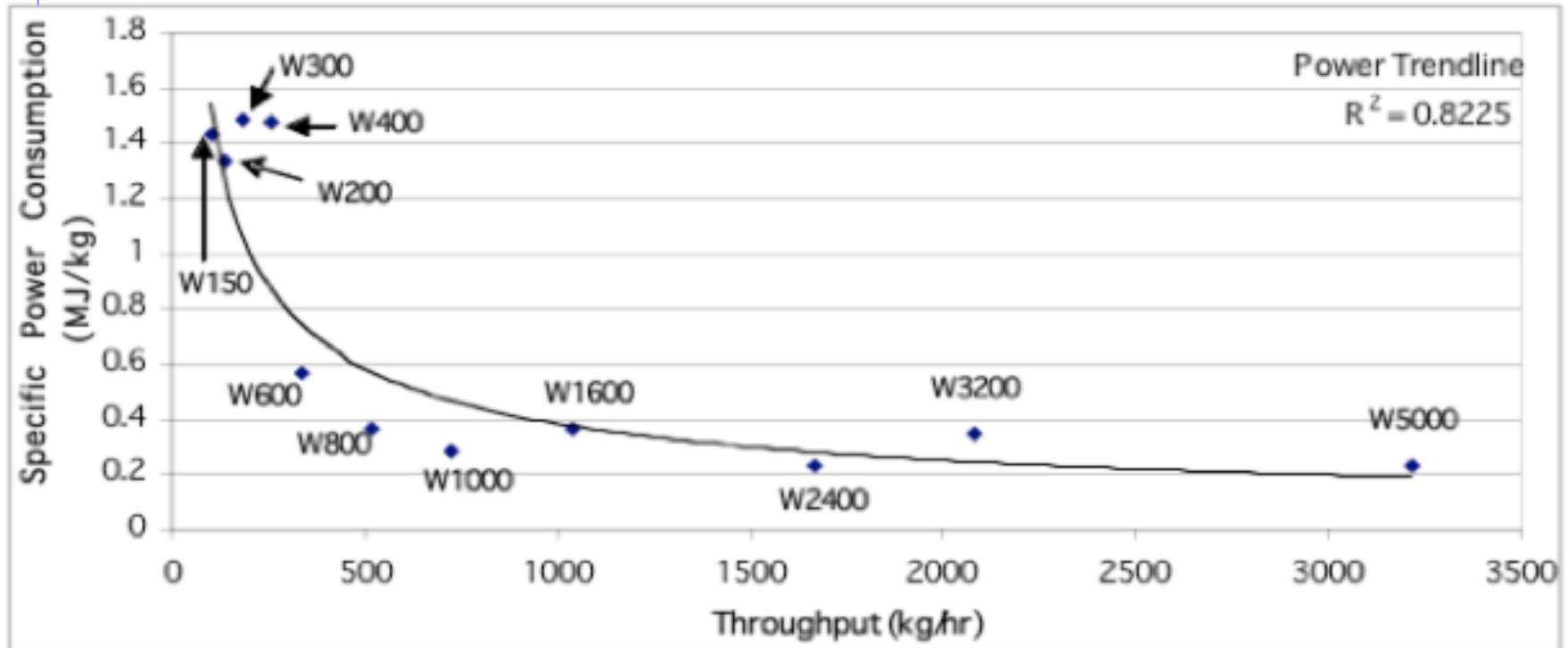
All-electrics have very low fixed energy costs (small idling power). SEC is constant as throughput increases.

$$SEC = p_v$$



Driers

- ◆ Used to dry internal moisture in hygroscopic polymers and external moisture in non-hygroscopic ones.
- ◆ It is done before extruding and injection molding.



Same as $\longrightarrow \frac{P}{\dot{m}} = \frac{E}{m} = SEC = \frac{P_{aux}}{\dot{m}} + k$

Source: [Thiriez]

LCI Summarized Results

ENERGY CONSUMPTION BY STAGE in MJ/kg of shot

Thermoplastic Production

	HDPE	LLDPE	LDPE	PP	PVC	PS	Generic by Amount		Extras	
							Consumed	Inj. Molded	PC	PET
avg	89.8	79.7	73.1	83.0	59.2	87.2	81.2	74.6	95.7	78.8
low	77.9	79.7	64.6	64.0	52.4	70.8	69.7	62.8	78.2	59.4
high	111.5	79.7	92.0	111.5	79.5	118.0	102.7	97.6	117.4	96.0

Polymer Delivery	avg	0.19
	low	0.12
	high	0.24

Compounder

	Internal Transport	Drying	Extrusion	Pelletizing	Building (lights, heating, ect.)
avg	0.09	0.70	3.57	0.16	0.99
low	-----	0.30	1.82	0.06	-----
high	-----	1.62	5.00	0.31	-----

Subtotal	avg	5.51
	low	3.25
	high	8.01

Polymer Delivery	avg	0.19
	low	0.12
	high	0.24

Injection Molder

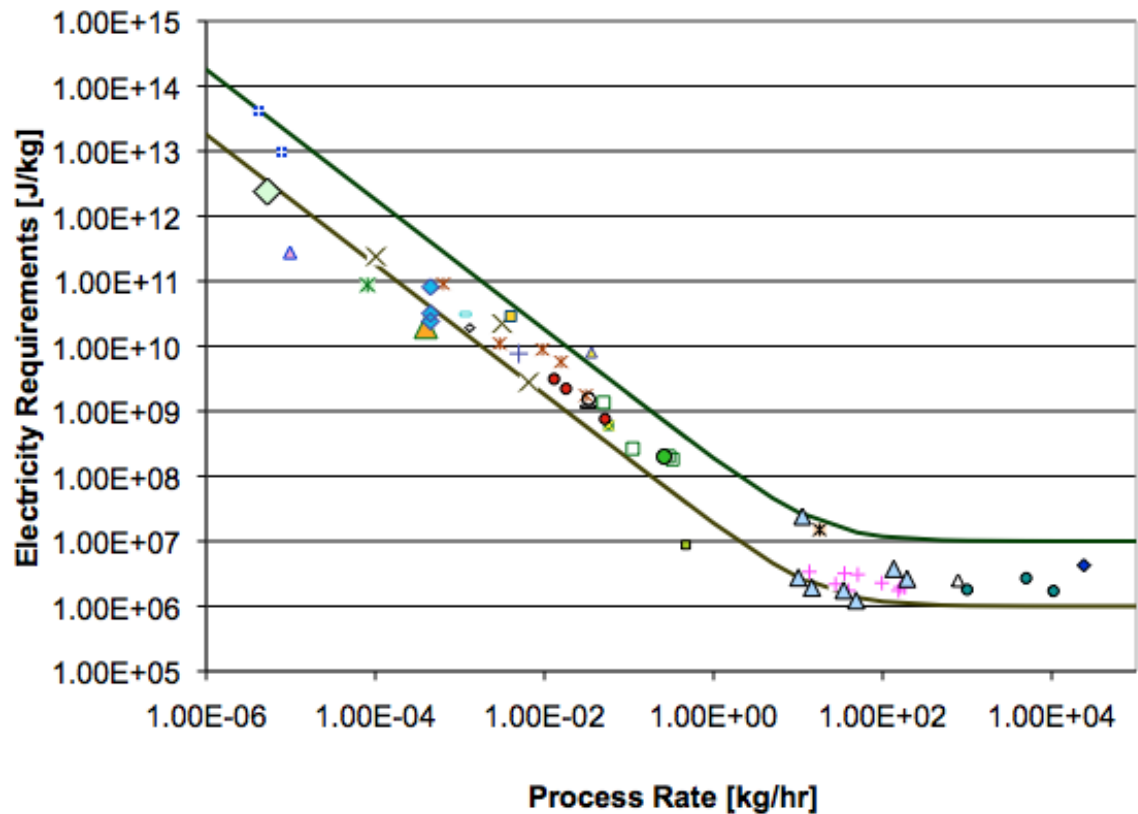
	Internal Transport	Drying	Injection Molding (look below)	Scrap (Granulating)	Building (lights, heating, ect.)
avg	0.04	0.70	↓	0.05	0.99
low	-----	0.30		0.03	-----
high	-----	1.62		0.12	-----

		Injection Molding - Choose One		
		Hydraulic	Hybrid	All-Electric
	avg	11.29	5.56	4.89
	low	3.99	3.11	1.80
	high	69.79	8.45	15.29
Subtotal	avg	13.08	7.35	6.68
	low	5.35	4.47	3.17
	high	72.57	11.22	18.06

TOTAL w/ Generic Inj. Molded Polymer		Hydraulic	Hybrid	All-Electric
	avg	93.60	87.87	87.20
	low	71.65	70.77	69.46
	high	178.68	117.34	124.18

TOTAL w/b Polymer Prod		Hydraulic	Hybrid	All-Electric
	avg	18.97	13.24	12.57
	low	8.84	7.96	6.66
	high	81.04	19.70	26.54

Notes Drying - the values presented assume no knowledge of the materials' hygroscopia. In order words, they are averages between hygroscopic and non-hygroscopic values. For hygroscopic materials such as PC and PET additional drying energy is needed (0.65 MJ/kg in the case of PC and 0.52 MJ/kg in the case of PET)
Pelletizing - in the case of pelletizing an extra 0.3 MJ/kg is needed for PP
Granulating - a scarp rate of 10% is assumed



◆ Injection Molding [20]	▲ Machining[18]	■ Finish Machining [29,33]	✕ CVD [6,29,34]
✕ Sputtering[29,34]	■ Grinding[22]	□ Abrasive Waterjet[23]	○ Wire EDM [29,32]
○ Drill EDM [29, 35]	▲ Laser DMD [33]	⊞ Thermal Oxidation [6]	● Melters [26]
● Cupola Melter [26]	● Carbon Nanofiber Production[12]	+ PECVD of an Oxide Film [28]	— PECVD of a Nitride Film [28]
● Dry Etching of an Oxide Film [28]	○ Dry Etching of a Nitride Film [28]	■ Sputtering of AlCu [29,34]	▲ Carbon Nanotube Production[28]
▲ Brazing [37,38]	✕ PCB Soldering [40]	● Friction Stir Weld[52]	● HiPco/SWNT [44,45]
✕ Arc/SWNT [45]	▲ CVD/SWNT [45]	— Upper Bound	— Lower bound

Do Polymers get recycled?

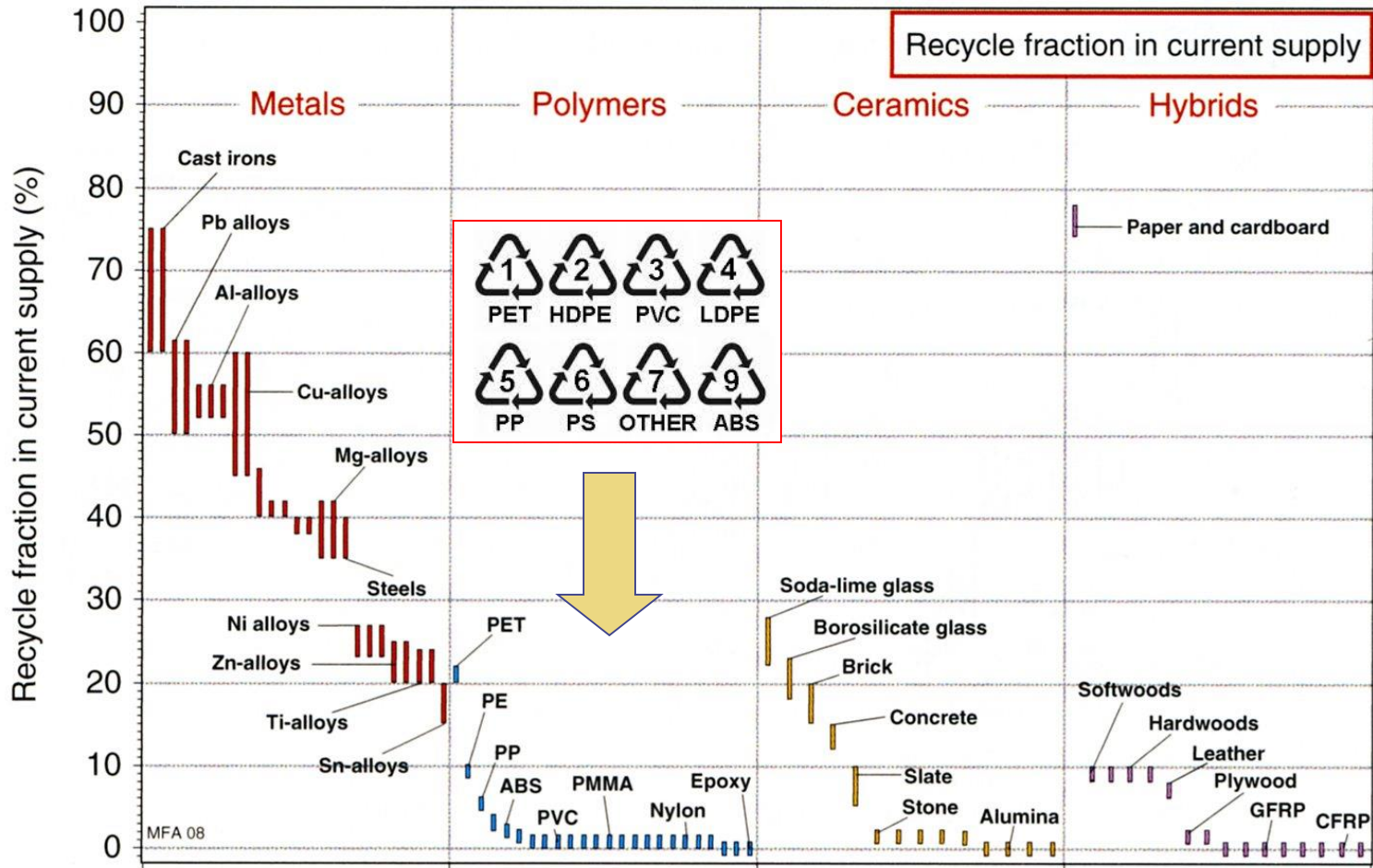
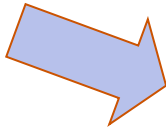


FIGURE 6.13 Recycle fraction bar chart.

Ref Ashby 2009

The printer goes in the hopper...



And comes out....



Readings (first 3) & Refs

- ◆ Tadmore and Gogos
 - Molding and Casting pp 584 -610
- ◆ Boothroyd Dewhurst
 - Design for Injection Molding pp 319 - 359
- ◆ Kalpakjian Ch 7 & 19
- ◆ [Thiriez et al, "An Environmental Analysis of Injection Molding"](#)
- ◆ ["Injection Molding Case Study"](#) (Gas Assist)