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22.616. Problem Set #6 Solutions

1. Ambipolar Potential in a Magnetized plasma Column

The radial current accounts for viscosity and inertial rotation

$$J_r = \frac{C}{B} \left(-\frac{1}{r} \frac{\partial}{\partial r} r n_i m_i \eta_i \frac{\partial}{\partial r} V_{i\theta} + n_i m_i \frac{\partial}{\partial t} V_{i\theta} \right)$$

By ambipolarity, intrinsically, $J_r = 0$. i.e.

$$\frac{\partial}{\partial t} V_{i\theta} = \eta_i \frac{1}{r} \frac{\partial}{\partial r} r \frac{\partial}{\partial r} V_{i\theta}$$

it is a diffusion equation in cylindrical system.

~~At~~ A general solution is

$$V_{i\theta} = \sum_n A_n e^{-K_n^2 t} J_0 \left(\frac{K_n}{\eta_i} r \right)$$

when $t \rightarrow \infty$, Asymptotically, $V_{i\theta} = 0$.

Usually (main term)

$$V_{i\theta} = \frac{c E_x B}{B^2} + \frac{b \times \nabla P_i}{n_i m_i \omega_i}$$

$$= -\frac{CE_r}{B} + \frac{1}{n_i m_i \omega_i} \frac{dP_i}{dr} = 0$$

So $E_r = \frac{B}{n_i m_i \omega_i C} \frac{dP_i}{dr}$. i.e.

$$-\frac{d\phi}{dr} = \frac{1}{n_i e_i} \frac{dP_i}{dr} = \frac{1}{e_i} \frac{dT_i}{dr}$$

$$\Rightarrow e_i \phi(r) = \bar{T}_i(r) , (\text{Assume at edge } e_i \phi(a) = T_i(a) = 0)$$

Therefore in this steady state $\nabla \phi = 0$, the net rotation is only from electrons will die away. The electron ~~velocity~~ will contribute to current Net rotation.

$$V_{e\theta} = \frac{c E \times B}{B} + \frac{b \times \nabla P_e}{\text{Nearest}} \quad \text{will contribute to current Net rotation.}$$

Note the friction induced radial Electron and ion flow cancel each other. to keep the ambipolarity.

2. self-Adjoint property of Collision operator

$$C_e(\hat{f}) = \frac{\Gamma}{2} \frac{\partial^2}{\partial v^2} \cdot \int d^3v' f_0 f_0' \underline{\underline{U}} \cdot \left(\frac{\partial}{\partial v} \hat{f} - \frac{\partial}{\partial v'} \hat{f}' \right)$$

$$\int d^3v \hat{g} C_e(\hat{f}) = \frac{\Gamma}{2} \int d^3v \hat{g} \frac{\partial}{\partial v} \cdot \int d^3v' f_0 f_0' \underline{\underline{U}} \cdot \left(\frac{\partial}{\partial v} \hat{f} - \frac{\partial}{\partial v'} \hat{f}' \right)$$

Integrate by parts (Assume \hat{f} & \hat{g} is reasonably behaved at ∞)

$$\int d^3v \hat{g} C_e(\hat{f}) = -\frac{\Gamma}{2} \int d^3v d^3v' f_0 f_0' \frac{\partial \hat{g}}{\partial v} \cdot \underline{\underline{U}} \cdot \left(\frac{\partial}{\partial v} \hat{f} - \frac{\partial}{\partial v'} \hat{f}' \right) \quad (1)$$

make change $v \rightleftharpoons v'$, $\underline{\underline{U}}$ is symmetric about v and v'

$$\int d^3v \hat{g} C_e(\hat{f}) = -\frac{\Gamma}{2} \int d^3v d^3v' f_0 f_0' \left(-\frac{\partial \hat{g}}{\partial v'} \right) \cdot \underline{\underline{U}} \cdot \left(\frac{\partial}{\partial v} \hat{f} - \frac{\partial}{\partial v'} \hat{f}' \right) \quad (2)$$

$$\frac{\textcircled{1} + \textcircled{2}}{2} \Rightarrow$$

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$$\int d^3v \hat{g} C_e(\hat{f}) = -\frac{1}{4} \int d^3v d^3v' f_0 f_0' \left(\frac{\partial \hat{g}}{\partial v} - \frac{\partial \hat{g}'}{\partial v'} \right) \cdot \underline{U} \cdot \left(\frac{\partial \hat{f}}{\partial v} - \frac{\partial \hat{f}'}{\partial v'} \right)$$

This is a symmetric form about \hat{g} & \hat{f} , so.

$$\int d^3v \hat{g} C_e(\hat{f}) = \int d^3v \hat{f} C_e(\hat{g}), \text{ (self-adjoint!)}$$

3. Conservation laws for linearized Collision operator

Use the self-adjointness of C_e .

$$\int d^3v \begin{bmatrix} 1 \\ mv \\ \frac{1}{2}mv^2 \end{bmatrix} C_e(\hat{f}) = \int d^3v \hat{f} C_e \left(\begin{bmatrix} 1 \\ mv \\ \frac{1}{2}mv^2 \end{bmatrix} \right)^*$$

$$C_e \left(\begin{bmatrix} 1 \\ mv \\ \frac{1}{2}mv^2 \end{bmatrix} \right) = \frac{1}{2} \frac{\partial}{\partial v} \cdot \int d^3v' f_0 f_0' \underline{U} \cdot \left(\frac{\partial}{\partial v} \begin{bmatrix} 1 \\ mv \\ \frac{1}{2}mv^2 \end{bmatrix} - \frac{\partial}{\partial v'} \begin{bmatrix} 1 \\ mv' \\ \frac{1}{2}mv'^2 \end{bmatrix} \right)$$

$$\text{Ex. } \frac{\partial}{\partial v} 1 - \frac{\partial}{\partial v'} 1 = 0$$

$$\frac{\partial}{\partial v} v - \frac{\partial}{\partial v'} v' = \underline{I} - \underline{I}' = 0$$

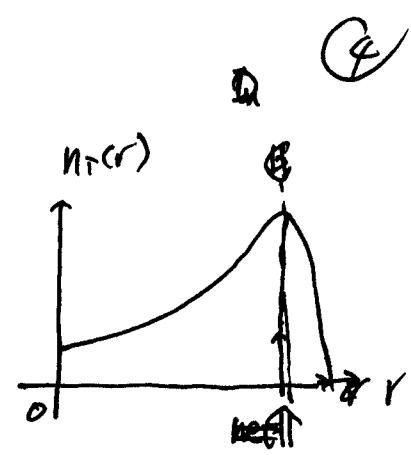
$$\frac{\partial}{\partial v} \frac{1}{2}mv^2 - \frac{\partial}{\partial v'} \frac{1}{2}mv'^2 = m(v - v'), \text{ but } \underline{U} \cdot (v - v') = 0$$

$$\text{So } \int d^3v \hat{f} C_e \left(\begin{bmatrix} 1 \\ mv \\ \frac{1}{2}mv^2 \end{bmatrix} \right) = 0 \Rightarrow \int d^3v \begin{bmatrix} 1 \\ mv \\ \frac{1}{2}mv^2 \end{bmatrix} C_e(\hat{f}) = 0$$

4. Solution:

The radial ion flux is

$$\vec{P}_i = -n_i \frac{T_i}{m_i S_i^2 T_{i2}} \left(\frac{P'_i}{P_i} - \frac{T_2}{z T_i} \frac{P'_2}{P_2} - \frac{3}{2} \frac{T'_c}{T_c} \right)$$



From the ambipolarity condition

$$\sum_a e_a P_a = e (I'_i + z \vec{P}'_2 - \vec{P}'_e)$$

$$\text{But } \vec{P}_e \propto n_e \frac{T_e}{m_e S_e T_e} \ll \vec{P}_i, \text{ so } \vec{P}'_2 = -\frac{1}{z} \vec{P}'_i.$$

This is to say, if we can make ions flow in, the impurities would flow out.

If we take $\frac{P'_i}{P_i} - \frac{T_2}{z T_i} \frac{P'_2}{P_2} - \frac{3}{2} \frac{T'_c}{T_c} > 0$, ion will flow inward.

Assume $T_2 \sim T_i$, then $(\ln n_i - \frac{1}{2} \ln n_2)' > (\ln T_i (\frac{1}{2} + \frac{1}{z}))'$

$$\therefore \text{If } z \gg 1: \quad \frac{n_i(r)}{n_i(0)} > \left(\frac{n_2(r)}{n_2(0)} \right)^{\frac{1}{z}} \left(\frac{T_i(r)}{T_i(0)} \right)^{\frac{1}{2} - \frac{1}{z}} \quad \dots \text{ (1)}$$

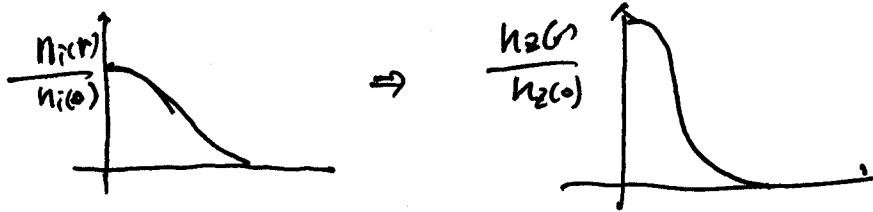
So if we can add some net neutral source at the tokamak edge to make a density (pressure) profile to satisfy Condition 1). The particles will flow in until a steady state is reached.

$$\vec{P}_i = 0. \quad \frac{n_i(r)}{n_i(0)} = \left(\frac{n_2(r)}{n_2(0)} \right)^{\frac{1}{z}} \left(\frac{T_i(r)}{T_i(0)} \right)^{\frac{1}{2} - \frac{1}{z}}$$

For Helium ash, $z=2$

$$\frac{n_i(r)}{n_i(0)} = \left(\frac{n_z(r)}{n_z(0)} \right)^{\frac{1}{2}} \Rightarrow \left(\frac{n_z(r)}{n_z(0)} \right) = \left(\frac{n_i(r)}{n_i(0)} \right)^2$$

Assume the steady state ion distribution is



So there is a big accumulation of ions ⁱⁿ at the center.
impurities (He)

However, for high z Impurities, e.g. Carbon, $z=6$

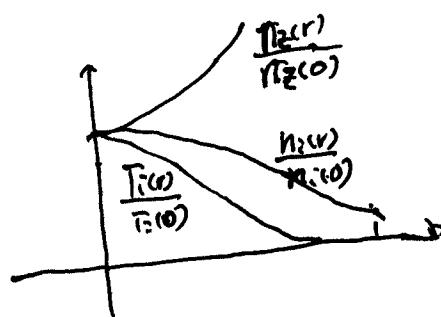
$$\frac{n_z(r)}{n_z(0)} = \left(\frac{n_i(r)}{n_i(0)} \right)^6 \left(\frac{T_i(r)}{T_i(0)} \right)^{-2}$$

There is a good chance that we can make $n_z(a) > n_i(0)$

For example, we can take $\frac{n_i(r)}{n_i(0)} = \frac{1}{1+4\frac{r^2}{a^2}}$

But if we make up a temperature profile, s.t. $\frac{T_i(r)}{T_i(0)} = \frac{1}{(1+4\frac{r^2}{a^2})^4}$

Then $\frac{n_z(r)}{n_z(0)} = \left(1 + \frac{4r^2}{a^2} \right)^2$, there would be no accumulation
of impurities in the center.



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5. Diamagnetic Fluxes.

$$nmv_x y = n \int d^3v m v_y f_i = \frac{nm}{\pi} \int d^3v v_y^2 (A_1 + A_2 (\frac{mv^2}{2T} - \frac{5}{2})) f_m$$

$$1^0 \int d^3v v_y^2 f_m = \frac{1}{3} \int d^3v v^2 \frac{n}{(2\pi T/m)^{3/2}} e^{-\frac{mv^2}{2T}}$$

$$= \frac{n}{3} \left(\frac{m}{2\pi T}\right)^{3/2} \times 4\pi \int_0^\infty dv v^4 e^{-\frac{mv^2}{2T}}$$

let $x = \sqrt{\frac{m}{2T}} v$, then

$$\int d^3v v_y^2 f_m = \frac{4\pi n}{3} \left(\frac{m}{2\pi T}\right)^{3/2} \left(\frac{2T}{m}\right)^{5/2} \int_0^\infty dx x^4 e^{-x^2}$$

$$= \frac{nI}{m}$$

$$2^0 A \cdot \int d^3v v_y^2 (\frac{mv^2}{2T} - \frac{5}{2}) f_m$$

$$= \frac{1}{3} \int d^3v v^2 (\frac{mv^2}{2T} - \frac{5}{2}) f_m$$

$$= \frac{4\pi n}{3} \left(\frac{m}{2\pi T}\right)^{3/2} \int_0^\infty dv v^4 (\frac{mv^2}{2T} - \frac{5}{2}) e^{-\frac{mv^2}{2T}}$$

(let $x = \sqrt{\frac{m}{2T}} v$, then)

$$= \frac{4\pi n}{3} \left(\frac{m}{2\pi T}\right)^{3/2} \left(\frac{2T}{m}\right)^2 \int_0^\infty dx x^4 (x^2 - \frac{5}{2}) e^{-x^2}$$

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~~Part~~ let $t = x^2$, then

$$\int_0^\infty dt x^4 \left(x^2 - \frac{5}{2}\right) e^{-x^2} \\ = \frac{1}{2} \int_0^\infty dt t^{3/2} \left(t - \frac{5}{2}\right) e^{-t}$$

$$= \frac{1}{2} \left(\Gamma\left(\frac{7}{2}\right) - \frac{5}{2} \Gamma\left(\frac{5}{2}\right) \right)$$

$$= 0$$

so. we have $\int d^3v v_y^2 \left(\frac{mv^2}{2T} - \frac{5}{2}\right) f_m = 0$

Then

$$nm v_y^2 = \frac{m}{\Sigma} \frac{nT}{m} A_1 = \frac{\rho}{\Sigma} A_1 \propto A_1$$

6. Generalized Flux-Fraction Relations

Take the energy ^{flux} moment of the leading order kinetic equation

$$\nabla \cdot \underline{v} \times \underline{b} \cdot \frac{\partial}{\partial \underline{v}} f \approx C(f, f)$$

$$\Rightarrow \int d^3v \frac{1}{2} mv^2 \nabla \cdot \underline{v} \times \underline{b} \cdot \frac{\partial}{\partial \underline{v}} f = \int d^3v \frac{1}{2} mv^2 \nabla \cdot C(f, f)$$

$$\text{But } \left(\int d^3v \frac{1}{2} mv^2 \nabla \cdot \underline{v} \times \underline{b} \cdot \frac{\partial}{\partial \underline{v}} f \right)_i$$

$$= \frac{\Sigma m}{2} \int d^3v \nabla^i v^j v_i \sum_{jkl} v_k b_l \frac{\partial f}{\partial v_j}$$

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Integrate by parts

$$\stackrel{D}{=} -\frac{\Sigma m}{2} \int d^3v f \sum_{jkl} b_l \frac{\partial}{\partial v_j} (v^2 v_i v_k)$$

$$= -\frac{\Sigma m}{2} \int d^3v f \sum_{jkl} b_l (2v_j v_k v_R + v^2 \delta_{ij} v_k + v^2 \delta_{jk} v_i)$$

$$(\sum_{jkl} \delta_{jk} \delta_{ik} = 0, \sum_{jkl} b_l v_j v_k = \underline{v} \cdot (\underline{v} \times \underline{b}) = 0)$$

$$= -\frac{\Sigma m}{2} \int d^3v f \sum_{jkl} b_l v^2 v_k$$

$$\stackrel{D}{=} -\frac{\Sigma m}{2}$$

Therefore we can write above result in vector form

$$\int d^3v \frac{1}{2} m v^2 \underline{v} \cdot \underline{Q} \times \underline{b} \cdot \frac{\partial}{\partial \underline{v}} f = \cancel{\underline{b} \times} \underline{b} \times \int d^3v \frac{1}{2} m v^2 \underline{v}$$

$$= \Sigma Q_x \underline{x} \times \underline{b} = \Sigma Q_x \underline{Q}_x \underline{Q}_y \underline{Q}_z$$

$$\Rightarrow \Sigma Q_x = + \int d^3v \frac{1}{2} m v^2 Q_y C_e(f, f)$$

$$= + \int d^3v \frac{1}{2} m v^2 Q_y C_e(\hat{f})$$

$$(f = \hat{f} + 1) f_0 ?$$

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7. (like-particle (Ion) Collision Fluxes

Assume the kinetic equation for the guiding center distribution

$$\frac{\partial f}{\partial t} = C_0(f, f) + C_2(f, f)$$

where C_0 is the "velocity" operator

$$C_0(f, f) \equiv \frac{P^i}{2} \frac{\partial}{\partial v^i} \int d^3v' \stackrel{U}{=} \left(\frac{\partial}{\partial v^i} - \frac{\partial}{\partial v'^i} \right) f f'$$

$$C_2(f, f) = \frac{\partial}{\partial x^i} \int d^3v' D(v, v') \left(\frac{\partial f}{\partial x^i} f' - f \frac{\partial f'}{\partial x^i} \right)$$

$$D(v, v') \equiv P^{ii} e_g \cdot U \cdot \frac{e_g}{\Delta^2}$$

Zeroth order

$$C_0(f_0, f_0) = 0 \Rightarrow f_0 = f_M \text{ (sufficient)}$$

Second order:

$$\begin{aligned} \frac{\partial f_0}{\partial t} &\approx C_2(f_0, f_0) + C_0(f_0, f_2) + C_0(f_2, f_0) \\ &= C_0(f_{\frac{1}{2}}, f_2) + C_0(f_{\frac{1}{2}}, f_2) + C_2(f_M, f_M) \\ &= C_0(\hat{f}_2) + C_2(f_{\frac{1}{2}}, f_{\frac{1}{2}}) \quad \dots \text{--- } (1) \end{aligned}$$

~~Take the Notice~~ Notice $\int d^3v \left(\frac{1}{2} mv^2 \right) C_0(\hat{f}_2) = 0$, proved in prob 3.

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1° Take the particle moment of Eq(1).

$$\frac{\partial n}{\partial t} = \int d^3v C_1(f, \hat{f}_2) + \int d^3v C_2(f_g, f_{g+})$$

$$= \int d^3v G(f_g, f_{g+})$$

Write as $\frac{\partial n}{\partial t} + \frac{\partial}{\partial x} P_i = 0$, then P_{i0} is defined as

$$P_i = - \int d^3v d^3v' D(v, v') \left(\frac{\partial f_{g0}}{\partial x} f_{g+}' - f_{g+} \frac{\partial f_{g0}}{\partial x} \right)$$

2°. Take the energy moment of Eq(1).

$$\frac{\partial}{\partial t} \int \frac{1}{2} mv^2 f_m d^3v = \int d^3v \frac{1}{2} mv^2 G(f_g, f_{g+}) \quad \text{---}$$

$$\text{i.e. } \frac{\partial}{\partial t} \frac{3}{2} n T_i = \frac{\partial}{\partial x} \int d^3v d^3v' \frac{1}{2} mv^2 D(v, v') \left(\frac{\partial f_{g+}}{\partial x} f_{g+}' - f_{g+} \frac{\partial f_{g0}}{\partial x} \right)$$

$$= \frac{\partial}{\partial x} \frac{5}{2} T_i \int d^3v d^3v' D(v, v') \left(\frac{\partial f_{g+}}{\partial x} f_{g+}' - f_{g+} \frac{\partial f_{g0}}{\partial x} \right)$$

$$+ \frac{\partial}{\partial x} T_i \int d^3v d^3v' \left(\frac{mv^2}{2T_i} - \frac{5}{2} \right) D(v, v') \left(\frac{\partial f_{g+}}{\partial x} f_{g+}' - f_{g+} \frac{\partial f_{g0}}{\partial x} \right)$$

$$= - \frac{\partial}{\partial x} \frac{5}{2} T_i P_i + - \frac{\partial}{\partial x} Q_i$$

with

$$q_i = -\bar{T}_i \int d^3v d^3v' \left(\frac{mv^2}{2T_i} - \frac{5}{2} \right) D(v, v') \left(\frac{\partial f_0}{\partial \mathbf{x}} f'_0 - f_0 \frac{\partial f'_0}{\partial \mathbf{x}} \right)$$

$$\frac{q_i}{T_i} = -A_2$$

From above

$$\bar{T}_i = - \int d^3v d^3v' D(v, v') \left(\frac{\partial f_0}{\partial \mathbf{x}} f'_0 - f_0 \frac{\partial f'_0}{\partial \mathbf{x}} \right)$$

Change of variables $v \Leftrightarrow v'$, and $D(v, v') = D(v', v)$

$$\text{So } \bar{T}_i = - \int d^3v d^3v' D(v, v') \left(\frac{\partial f'_0}{\partial \mathbf{x}} f_0 - f'_0 \frac{\partial f_0}{\partial \mathbf{x}} \right)$$

$$\text{So } \bar{T}_i = -\bar{T}_i \Rightarrow \boxed{\bar{T}_i = 0}$$

$$f_0 = \frac{n}{(2\pi T_i/m)^3} e^{-\frac{mv^2}{2T_i}} \Rightarrow \frac{\partial f_0}{\partial \mathbf{x}} = \left(A_1 + \left(\frac{mv^2}{2T_i} - \frac{5}{2} \right) A_2 \right) f_0$$

$$\text{So } \frac{q_i}{T_i} = - \int d^3v d^3v' \left(\frac{mv^2}{2T_i} - \frac{5}{2} \right) D(v, v') f_0 f'_0 \left(\frac{\frac{1}{2}mv^2 - \frac{1}{2}mv'^2}{T_i^2} \right) A_2$$

$$\stackrel{(1)}{=} -A_2 \int d^3v d^3v' \left(\frac{mv^2}{2T_i} - \frac{5}{2} \right) D(v, v') f_0 f'_0 \left(\frac{\frac{1}{2}mv^2 - \frac{1}{2}mv'^2}{T_i^2} \right)$$

$$\stackrel{(2)}{=} -A_2 \int d^3v d^3v' \left(\frac{mv'^2}{2T_i} - \frac{5}{2} \right) D(v, v') f_0 f'_0 \frac{\frac{1}{2}mv'^2 - \frac{1}{2}mv^2}{T_i^2}$$

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$$\frac{g_i + 2}{2} = - A_2 \int d^3v d^3v' \frac{\left(\frac{1}{2}mv^2 - \frac{1}{2}mv'^2\right)^2}{2T_i^2} D(v, v') f_0 f_0'$$

In terms of the overall transport matrix

$$\begin{bmatrix} P_i \\ g_i / k_B T_i \end{bmatrix} = \frac{1}{n} \begin{bmatrix} -D & T_{12} \\ T_{21} & -\chi_i \end{bmatrix} \begin{bmatrix} A_1 \\ A_2 \end{bmatrix}$$

Since A_1 & A_2 are independent to each other $P_i = 0$

Then $D = T_{12} = 0$.

Also we have $\textcircled{A} T_{21} = 0$ through above calculation or Onsager Symmetry.

$$\chi_i = \frac{n_i}{2T_i^2} \int d^3v d^3v' \frac{\left(\frac{1}{2}mv^2 - \frac{1}{2}mv'^2\right)^2}{2T_i^2} D(v, v') f_0 f_0'$$

So only χ_i is not zero with

$$D(v, v') = \underline{g}_y \cdot \underline{U} \cdot \underline{g}_y \frac{P_{ii}}{S^2}$$

Calculation of χ_i

change of variables $(v, v') \rightarrow (v_1, v_2)$

$$v_1 = v - v', \quad v_2 = \frac{1}{2}(v + v') \text{ - therefore}$$

$$\chi_i = \frac{n_i T^{ii}}{2\pi^2 \Omega^2 T_i^2} \int d^3v \int d^3v' \frac{m_i^2}{|v - v'|} \left(\frac{1}{2}v^2 - \frac{1}{2}v'^2 \right)^2 \left(1 - \frac{(v_2 - v'_2)^2}{|v - v'|^2} \right)$$

$$\times \frac{n^2}{(2\pi T/m_i)^3} e^{-\frac{m}{2kT}(v^2 + v'^2)}$$

$$= \frac{n_i T^{ii}}{2\pi^2 \Omega^2 T_i^2} \frac{n_i m_i^5}{(2\pi T_i)^3} \int d^3v_1 \frac{1}{v_1} \int d^3v_2 (v_1 \cdot v_2)^2 \left(1 - \frac{e_y \cdot v_1 \cdot v_2 \cdot e_y}{v_1^2} \right) \cancel{\int d^3v'}$$

$$\times e^{-\frac{m}{kT}v_1^2 + \frac{m}{kT}v_2^2}$$

Note $\frac{1}{(\pi T/m)^{1/2}} \int_{-\infty}^{\infty} dv_x v_x^2 e^{-\frac{m}{kT}v_x^2} = \frac{T}{2m}$

$$\therefore \frac{1}{(\pi T/m)^{3/2}} \int d^3v_2 v_2^2 e^{-\frac{m}{kT}v_2^2} = \frac{1}{2} \frac{T}{m} \stackrel{!}{=}$$

$$\therefore \chi_i = \frac{n_i T^{ii}}{2\pi^2 \Omega^2 T_i^2} \frac{n_i m_i^5}{(2\pi T_i)^3} \frac{1}{2} \frac{T}{m} \underbrace{\int d^3v_1 v_1 \left(1 - \frac{v_1 \cdot v_2}{v_1^2} \right)}_{e^{-\frac{m}{kT}v_1^2}} e^{-\frac{m}{kT}v_1^2} \times \left(\pi \left(\frac{T}{m} \right)^{3/2} \right)^2$$

$$= \frac{T^{ii}}{2\pi^2 \Omega^2 T_i^2} \frac{n_i^2 m_i^5}{(2\pi T_i)^3} \frac{\pi^{3/2}}{2} \left(\frac{T}{m_i} \right)^{5/2} \times \frac{64\pi}{3} \left(\frac{T_i}{m_i} \right)^2$$

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$$\text{Note } \int d^3v_i v_i \left(1 - \frac{v_i^2}{v_p^2}\right) e^{-\frac{mv_i^2}{kT_i}} \\ = 4\pi \int_0^\infty dv_i v_i^3 \left(1 - \frac{1}{3}\right) e^{-\frac{mv_i^2}{3kT_i}} = \frac{64\pi}{3} \left(\frac{T_i}{m_i}\right)^2$$

Therefore we get

$$\chi_i = \frac{2n_i}{3\sqrt{\pi}} \frac{T_{ii}^{1/2}}{S_i^2} \left(\frac{m_i}{T_i}\right)^{1/2} n_i^2$$

$$\text{Notice } T_{ii} = \frac{4\pi Z e^4 / m_i}{m_i^2} = \frac{2v_{ii}}{n_i} \left(\frac{2T_i}{m_i}\right)^{3/2}$$

$$\text{So } \chi_i = \frac{4\pi^2}{3\sqrt{\pi}} v_{ii} \frac{n_i T_i}{m_i S_i^2}$$

$$\text{From the book } \frac{1}{T_i} = \frac{2\sqrt{2}}{3\sqrt{\pi}} v_{ii}, \quad (\text{Eq. 1.5})$$

$$\text{So. } \chi_i = 2 \frac{n_i^2 T_i}{m_i S_i^2} \frac{1}{T_i}$$

This is exactly Braginskii's result Eq 4.48