

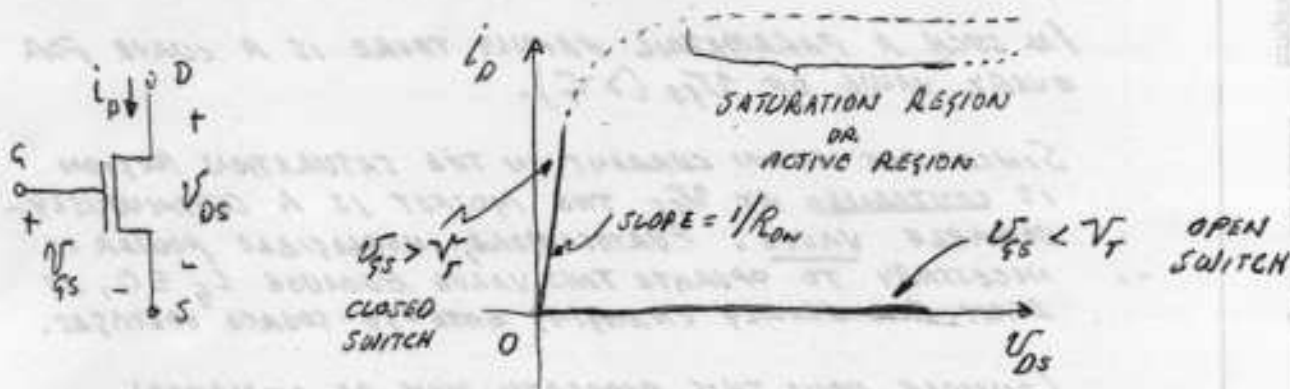
NOTES FOR 6.002 LECTURE # 7 THURSDAY, FEBRUARY 27, 2003

READ: 7.1 THROUGH 7.4

THE MOSFET HAS USES OTHER THAN AS A SWITCH.

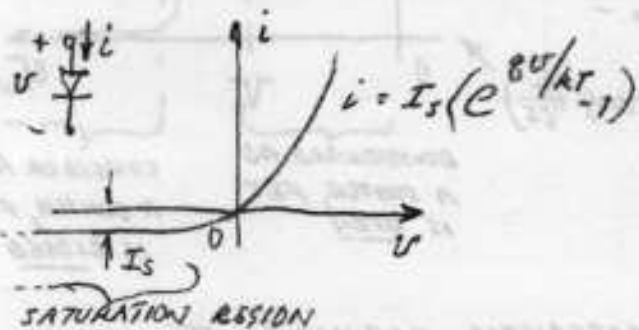
(DEMO # 1)

OUTPUT (OR DRAIN) CHARACTERISTICS:



FOR  $V_{GS} > V_T$  AND  $V_{DS}$  LARGE ENOUGH, THE DRAIN CURRENT  $I_D$  FLATTENS OFF OR BECOMES NEARLY CONSTANT, THIS IS REFERRED TO AS THE SATURATION REGION OF OPERATION.

COMPARE USE OF THE PHRASE IN THE SEMICONDUCTOR DIODE:



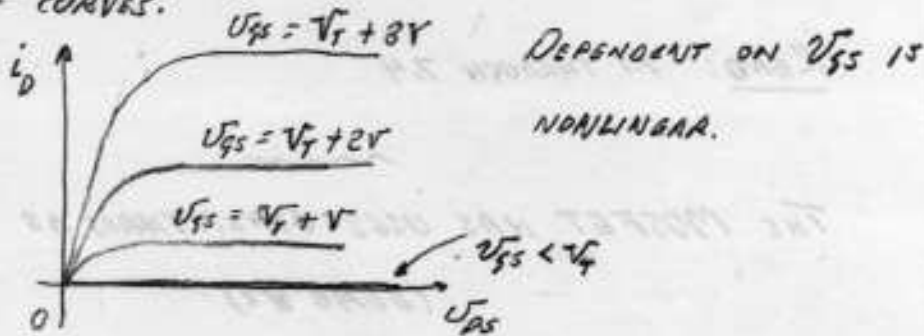
FOR  $v \ll -\frac{kT}{q}$  ("REVERSE BIAS") THE CURRENT IS CONSTANT AT  $i = -I_s$  - THE SATURATION CURRENT.

FOR THE FET, THE DRAIN CURRENT IN THE SATURATION REGION IS CONTROLLED BY THE GATE-TO-SOURCE VOLTAGE

(DEMO # 2)

EACH CURVE OF  $I_D$  VS  $V_{DS}$  CORRESPONDS TO A PARTICULAR VALUE OF  $V_{GS}$ .

SUCH FUNCTIONAL RELATIONSHIPS ARE REPRESENTED BY A PARAMETRIC FAMILY OF CURVES.

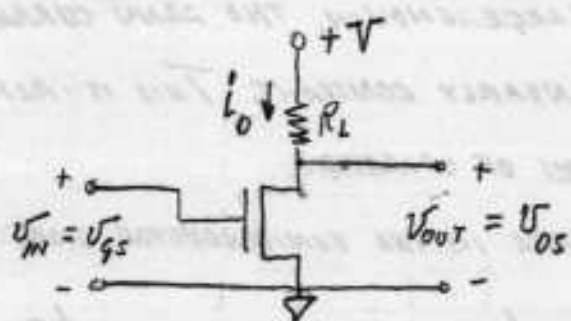


(DEMO #3)

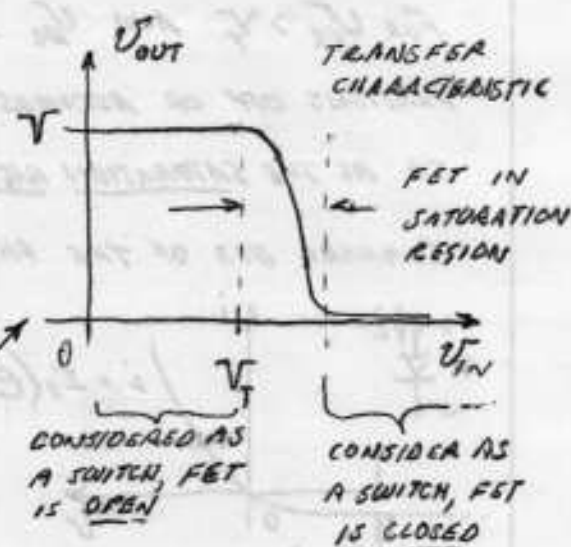
IN SUCH A PARAMETRIC FAMILY THERE IS A CURVE FOR EVERY VALUE OF  $V_{GS} (> V_T)$ .

SINCE THE DRAIN CURRENT IN THE SATURATION REGION IS CONTROLLED BY  $V_{GS}$  THE MOSFET IS A CONTINUOUSLY-VARIABLE VALVE. FURTHERMORE, NEGLIGIBLE POWER IS NECESSARY TO OPERATE THIS VALVE BECAUSE  $I_G \approx 0$ , AT LEAST FOR SLOWLY CHANGING GATE-TO-SOURCE VOLTAGES.

CONSIDER HOW THIS PROPERTY MAY BE EMPLOYED:



(CONSIDER SLOWLY INCREASING  $V_{GS}$ )

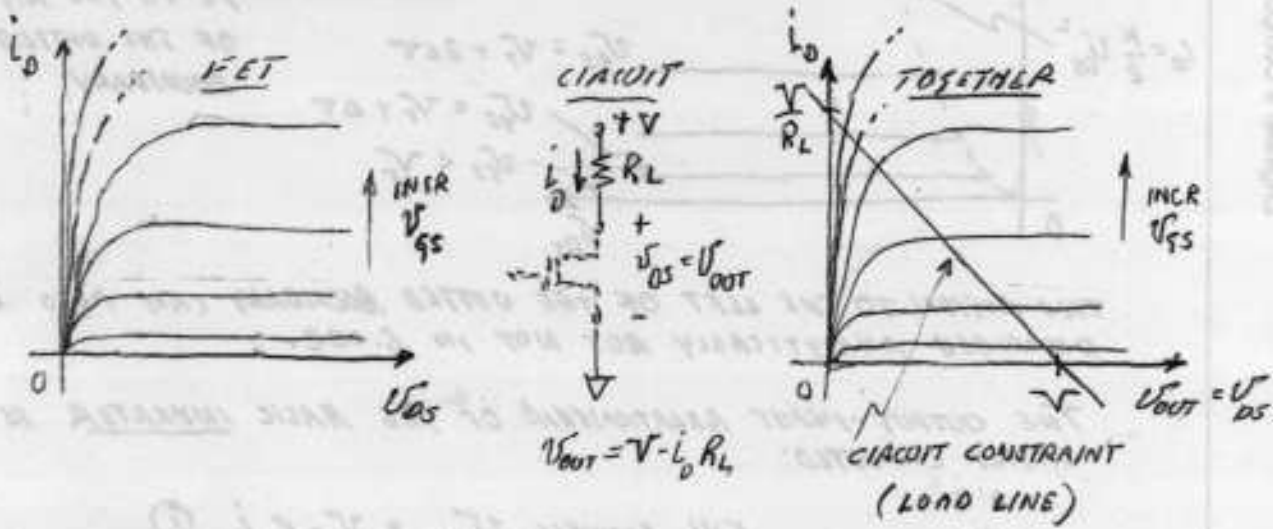


HOW IS A TRANSFER CHARACTERISTIC DERIVED? TWO WAYS:

I GRAPHICAL ANALYSIS USING THE PARAMETRIC OUTPUT OR DRAIN CHARACTERISTICS.

II ANALYTIC APPROACH USING A NONLINEAR MODEL DERIVED FROM DETAILED ANALYSIS OF THE PHYSICAL DEVICE, TAKING INTO ACCOUNT MATERIALS, STRUCTURE, AND THE EQUATIONS GOVERNING THE FLOWS OF CHARGE CARRIERS IN A SEMICONDUCTOR

**I GRAPHICAL ANALYSIS:** THE DRAIN CHARACTERISTICS (CURVES) IMPOSE, FOR EVERY VALUE OF  $V_{GS}$  A CONSTRAINT ON  $I_D$  VS  $V_{DS}$  IN THE FORM  $I_D = f(V_{DS})$ . THE CIRCUIT EXTERNAL TO THE FET IMPOSE A CONSTRAINT ON THE SAME VARIABLES: THAT IS KVL REQUIRES  $V = I_D R_L + V_{DS}$  ← A LINEAR EQUATION IN THESE VARIABLES



FOR EVERY VALUE OF  $V_{GS} = V_{IN}$  THERE IS A SPECIFIC CURVE OF  $I_{DS}$  VS  $V_{DS} = V_{OUT}$  (ONLY A FEW OF THE INFINITE FAMILY ARE SHOWN) WHERE THAT SPECIFIC CURVE CROSSES THE LOAD LINE IMPOSED BY KVL. THIS UNIQUELY <sup>DETERMINES</sup> THE VALUES OF  $I_D$  AND  $V_{OUT} = V_{DS}$  AT WHICH THE CIRCUIT CONSTRAINT AND THE FET CONSTRAINT ARE SIMULTANEOUSLY SATISFIED.

THE TRANSFER CHARACTERISTIC CAN BE READ OFF THE OUTPUT CHARACTERISTICS, INTERSECTION BY INTERSECTION, (DEMO #4)

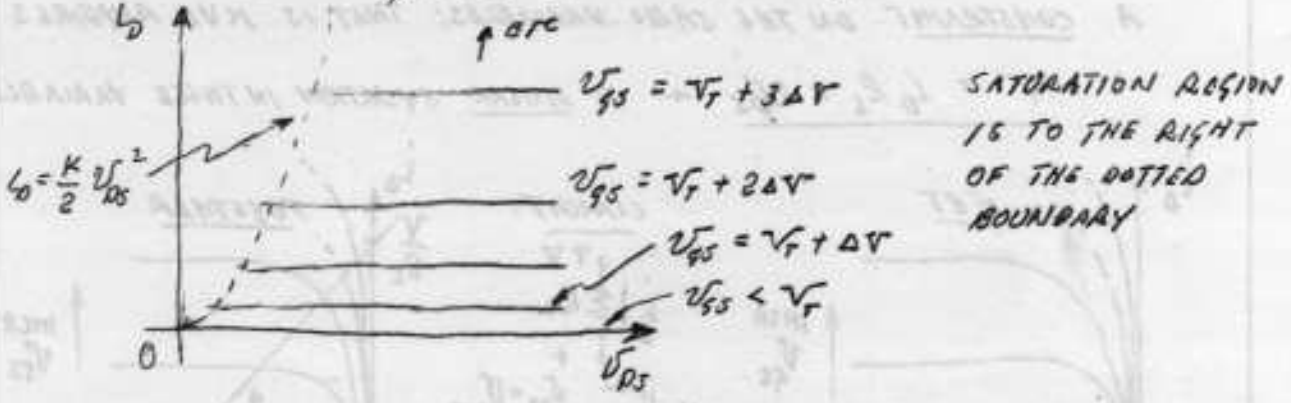
**II ANALYSIS OF THE PHYSICAL ELECTRONICS YIELDS:**

$$I_D = \begin{cases} 0 & \text{FOR } V_{GS} < V_T \\ \frac{K}{2} (V_{GS} - V_T)^2 & \text{FOR } \begin{cases} V_{GS} > V_T \\ V_{DS} > V_{GS} - V_T \end{cases} \end{cases} \quad \begin{matrix} \text{BOTH MUST} \\ \text{BE} \\ \text{SATISFIED} \end{matrix}$$

$K \left( \frac{A}{V^2} \right)$  IS A CONSTANT OF THE FET

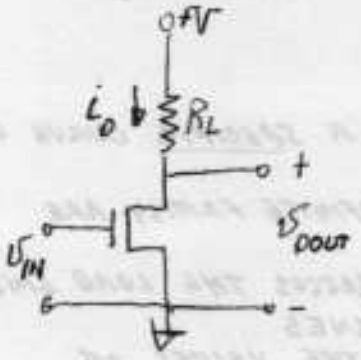
FOR THIS SUBJECT, THE SQUARE-LAW MODEL MUST BE TAKEN ON FAITH, JUST LIKE THE FET-AS-A-SWITCH MODEL AND THE EXPONENTIAL DIODE MODEL. ALL IS REVEALED IN 6.012!

ANALYTICAL  
 THE CORRESPONDING OUTPUT CHARACTERISTICS ARE:



THE REGION TO THE LEFT OF THE DOTTED BOUNDARY CAN ALSO BE DESCRIBED ANALYTICALLY BUT NOT IN 6.002.

THE OUTPUT-INPUT RELATIONSHIP OF THE BASIC INVERTER IS EASILY COMPUTED:



KVL REQUIRES  $V_{OUT} = V - R_L I_D$  ①

$$I_D = \begin{cases} 0 & \text{FOR } V_{GS} < V_T \\ \frac{K}{2} (V_{GS} - V_T)^2 & \begin{cases} V_{GS} > V_T \\ V_{DS} > V_{GS} - V_T \end{cases} \end{cases}$$
 ②

REPLACE  $V_{GS}$  BY  $V_{IN}$  AND SUBSTITUTE ②

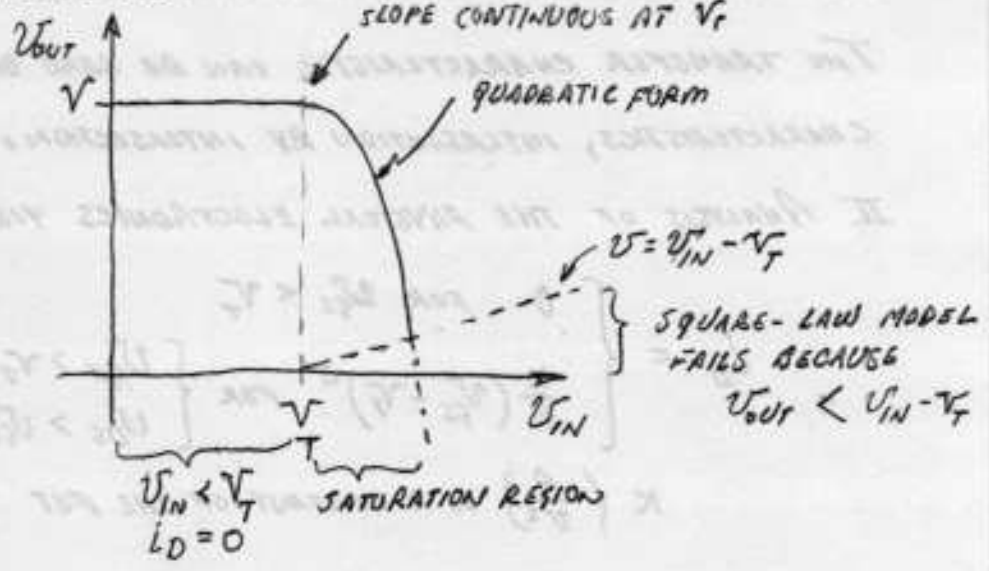
INTO ①

$$V_{OUT} = \begin{cases} V & \text{FOR } V_{IN} < V_T \\ V - \frac{K R_L}{2} (V_{IN} - V_T)^2 & \begin{cases} V_{IN} > V_T \\ V_{OUT} > V_{IN} - V_T \end{cases} \end{cases}$$

WHICH PLOTS AS

NOTE THAT SCALES ARE DIFFERENT

NOTE THAT "VOLTAGE GAIN" CAN BE ACHIEVED



$V_{IN} < V_T$   
 $I_D = 0$   
 SATURATION REGION

SQUARE-LAW MODEL FAILS BECAUSE  $V_{OUT} < V_{IN} - V_T$