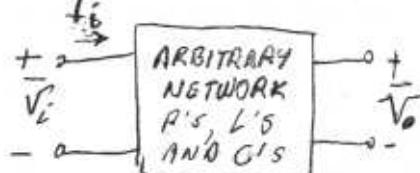


## NOTES FOR 6.002 LECTURE #18, APRIL 15, 2003

### THE S-PLANE AND ITS USES

IF A NETWORK IS COMPRISED OF LUMPED ELEMENTS ( $R, L, C$ ) THE TRANSFER FUNCTION AND THE INPUT IMPEDANCE OR ADMITTANCE WILL ALWAYS HAVE THE FORM OF RATIOS OF POLYNOMIALS IN  $S$  ( $s+j\omega$ ).

IF DRIVEN BY A VOLTAGE:



$\frac{\bar{V}_o}{\bar{V}_i}$ , THE VOLTAGE TRANSFER RATIO AND:

$\frac{I_o}{V_i}$ , THE INPUT ADMITTANCE

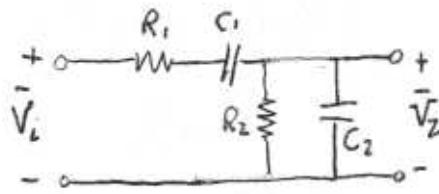
WILL BE RATIOS OF POLYNOMIALS IN  $S$ . FOR EXAMPLE:

$$\frac{\bar{V}_o}{\bar{V}_i} = \frac{s^n + k_{n-1}s^{n-1} + \dots + k_0}{s^m + l_{m-1}s^{m-1} + \dots + l_0}$$

THE NUMERATOR WILL HAVE  $n$  ROOTS EACH OF WHICH IS A ZERO - A FREQUENCY AT WHICH THE TRANSFER FUNCTION IS 0.

THE DENOMINATOR WILL HAVE  $m$  ROOTS, EACH OF WHICH IS A POLE - A FREQUENCY AT WHICH THE TRANSFER FUNCTION BLOWS UP.

### EXAMPLE I (CIRCUIT DISCUSSED IN LECTURE 17)



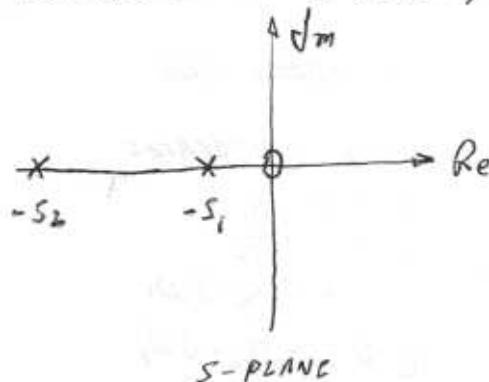
$$\frac{\bar{V}_o}{\bar{V}_i} = \frac{R_2 \parallel \frac{1}{C_2 s}}{R_2 \parallel \frac{1}{C_2 s} + R_1 + \frac{1}{C_1 s}} = \frac{s/R_1 C_2}{(s+s_1)(s+s_2)}$$

THE ROOT OF THE NUMERATOR IS  $s=0$

$s_1, s_2$  ARE POSITIVE REAL NUMBERS

THE ROOTS OF THE DENOMINATOR ARE  $s=-s_1, s=-s_2$

SHOWN ON THE S-PLANE, THE ROOTS ARE



○ DENOTES A ZERO

✗ DENOTES A POLE

S-PLANE

### INTERPRETATION OF POLES AND ZEROS:

$$\bar{V}_2 (s + s_1)(s + s_2) = \bar{V}_1 s \left( \frac{1}{R_1 C_2} \right)$$

WHEN  $s = 0$  (THE ZERO)  $\bar{V}_2 \equiv 0$  FOR EVERY  $\bar{V}_1$

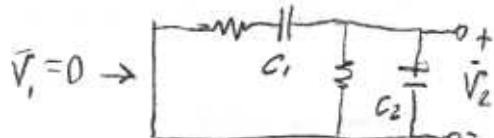
AT THE FREQUENCY OF A ZERO, THE OUTPUT IS ZERO

SUPPOSE  $\bar{V}_1 \equiv 0$ . UNDER WHAT CONDITIONS CAN  $\bar{V}_2$  BE NON-ZERO?

WHEN  $s = -s_1$  OR  $-s_2$ ,  $\bar{V}_2$  CAN BE NON-ZERO WITH NO INPUT.

CIRCUIT IS:

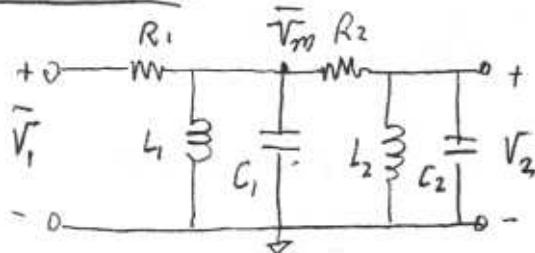
$$V_2(t) = k_1 e^{-s_1 t} + k_2 e^{-s_2 t}$$



$-s_1$  AND  $-s_2$  ARE THE NATURAL (UNFORCED) FREQUENCIES OF THE NETWORK.

[DROP SOME ENERGY INTO  $C_1$  OR  $C_2$  AND THE CURRENTS AND VOLTAGES EVERYWHERE IN THE NETWORK WILL RESPOND AS SUMS OF  $e^{-s_1 t}$  AND  $e^{-s_2 t}$ .

### EXAMPLE II



TO DETERMINE  $\bar{V}_2 / \bar{V}_1$ , DEFINE

$\bar{V}_m$  AND WRITE A PAIR OF NODE EQUATIONS:

$$\text{KCL} \begin{cases} \bar{V}_m \left( \frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{L_1 s} + C_1 s \right) - \bar{V}_2 \frac{1}{R_2} = \bar{V}_1 \left( \frac{1}{R_1} \right) \\ -\bar{V}_m \left( \frac{1}{R_2} \right) + \bar{V}_2 \left( \frac{1}{R_2} + \frac{1}{L_2 s} + C_2 s \right) = 0 \end{cases}$$

SOLVE THE NODE EQUATIONS FOR  $\bar{V}_2 / \bar{V}_1$ . FOR A SPECIFIC SET OF ELEMENT VALUES, THE SOLUTION IS OF THE FORM:

$$(1) \quad \frac{\bar{V}_2}{\bar{V}_1} = K \frac{s^2}{s^4 + \alpha s^3 + \beta s^2 + \gamma s + \delta} = K \frac{s^2}{(s + s_1)(s + s_2)(s + s_3)(s + s_4)}$$

WHERE  $s_1$  AND  $s_2$  ARE REAL NUMBERS AND

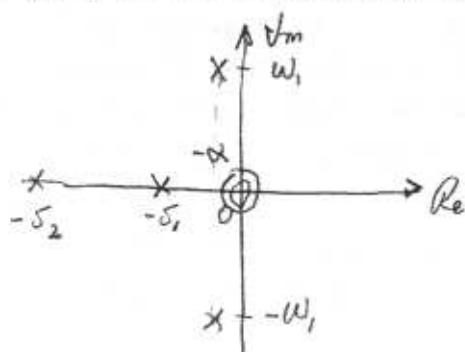
$s_3$  AND  $s_4$  ARE COMPLEX CONJUGATES

ZEROS ARE 0 AND 0, POLES ARE:

$$\begin{cases} s_1 = -s_1 \\ s_2 = -s_2 \\ s_3 = -\alpha_1 + j\omega_1 \\ s_4 = -\alpha_1 - j\omega_1 \end{cases}$$

(3)

THE POLE-ZERO DIAGRAM IS:



THE BODE DIAGRAM CAN BE CONSTRUCTED FROM THE LOCATIONS OF THE POLES AND ZEROS.

AND THE GENERAL FORM OF THE NATURAL (UNFORCED) TRANSIENT RESPONSE IS:

$$U_2(t) = k_1 e^{-s_1 t} + k_2 e^{-s_2 t} + k_3 e^{-\alpha t} \sin \omega_n t + k_4 e^{-\alpha t} \cos \omega_n t$$

THE TRANSFER FUNCTION CAN ALSO BE USED TO DETERMINE THE DIFFERENTIAL EQUATION RELATING  $U_2$  TO  $U_1$ .

IN CROSS MULTIPLIED FORM THE VOLTAGE TRANSFER RATIO (0 on p 3) IS:

$$\bar{V}_2 (s^4 + \alpha s^3 + \beta s^2 + \gamma s + \delta) = K s^2 \bar{V}_1$$

IF THE EXCITATION IS  $\bar{V}_1(t) = \bar{V}_1 e^{st}$ , THE RESPONSE IN THE STEADY STATE MUST BE:  $\bar{V}_2(t) = \bar{V}_2 e^{st}$

IN AS MUCH AS EACH DIFFERENTIATION OF  $\bar{V}_2 e^{st}$  YIELDS 5 TIMES THE ORIGINAL FUNCTION, THE DIFFERENTIAL EQUATION MUST BE:

$$\frac{d^4 \bar{V}_2}{dt^4} + \alpha \frac{d^3 \bar{V}_2}{dt^3} + \beta \frac{d^2 \bar{V}_2}{dt^2} + \gamma \frac{d \bar{V}_2}{dt} + \delta \bar{V}_2 = K \frac{d^2 \bar{V}_1}{dt^2}$$

FINALLY, THE S-PLANE DIAGRAM CAN BE USED TO VISUALIZE THE FREQUENCY RESPONSE. TWO APPROACHES:

A) FOR EXAMPLE I DEFINE NUMERATOR AND DENOMINATOR VECTORS:

$$\bar{A}(s) = \frac{1}{R_1 C_2} \frac{(s - \omega)}{(j\omega + s_1)(j\omega + s_2)}$$

FOCUS ON CHANGES AS  $\omega$  INCREASES FROM ZERO.

B) CONSIDER UNIFORM ELASTIC RUBBER SHEET MODEL - SLICE ALONG THE IMAGINARY AXIS.

- (4)
- IN SUMMARY:
- 1) THE POLE-ZERO DIAGRAM CONTAINS COMPLETE INFORMATION ABOUT THE TIME DOMAIN AND FREQUENCY DOMAIN BEHAVIOR OF A LINEAR NETWORK OR A LINEAR SYSTEM, EXCEPT FOR A SCALE FACTOR  
(E.G. IN EXAMPLE I, THE S-PLANE CONTAINS NO INFORMATION ABOUT  $1/(R_1 C_2)$ )
  - 2) THE POLE-ZERO DIAGRAM CAN BE USED TO CONSTRUCT THE TRANSFER FUNCTION WHICH GOVERNS THE FREQUENCY-DOMAIN BEHAVIOR.
  - 3) IT CAN BE USED TO FORMULATE THE NATURAL (UNFORCED) TRANSIENT RESPONSE.
  - 4) IT CAN BE USED TO FORMULATE THE DIFFERENTIAL EQUATION OF THE CIRCUIT OR SYSTEM.
  - 5) IT CAN BE USED FOR VISUALIZATION OF THE FREQUENCY RESPONSE.