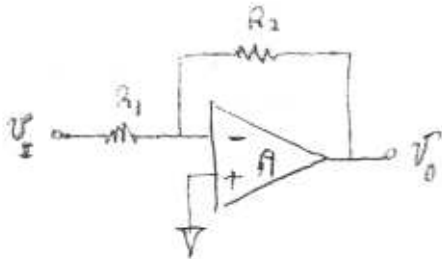


NOTES FOR 6.002 LECTURE # 21, TUESDAY, APRIL 29, 2003

OPERATIONAL AMPLIFIER STABILITY

READ 16.6 - 16.8

INVERTING CONNECTION:



$$V_+ - V_- = \frac{V_- - V_O}{R_2} \quad (\text{CURRENT MIRROR})$$

$$V_- = \frac{R_2}{R_1 + R_2} V_I + \frac{R_1}{R_1 + R_2} V_O \quad (\text{SUPERPOSITION})$$

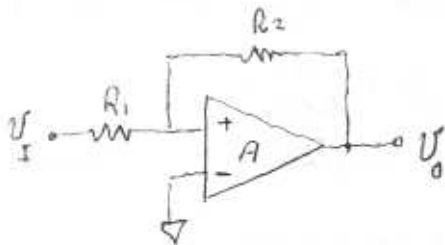
EITHER EQUATION TOGETHER WITH  $V_O = A(V_+ - V_-)$  AND  $V_+ = 0$  YIELDS

$$\frac{V_O}{V_I} = - \frac{A \frac{R_2}{R_1 + R_2}}{1 + A \frac{R_1}{R_1 + R_2}} \approx - \frac{R_2}{R_1} \quad \text{IF } A \frac{R_1}{R_1 + R_2} \gg 1$$

LOOP GAIN

ANY DISTURBANCE IS SUPPRESSED

WHAT HAPPENS IF THE INPUTS ARE INTERCHANGED?



IDENTICAL CONFIGURATION EXCEPT  $V_+$  AND  $V_-$  ARE INTERCHANGED

SAME ANALYSIS YIELDS:

$$\frac{V_O}{V_I} = \frac{A \frac{R_2}{R_1 + R_2}}{1 - A \frac{R_1}{R_1 + R_2}} \approx - \frac{R_2}{R_1} \quad \text{IF } A \frac{R_1}{R_1 + R_2} \gg 1$$

ANY DISTURBANCE IS AMPLIFIED

THE EQUILIBRIUM OF THE SECOND CIRCUIT, WITH POSITIVE FEEDBACK, IS UNSTABLE AND CANNOT BE SUSTAINED IN THE REAL WORLD

CONSIDER: INVERTED PENDULUM

ROLLER COASTER

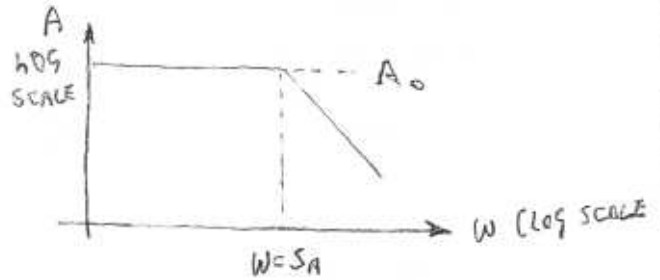
ELECTRIC BLANKET

INTRODUCE INTERNAL DYNAMICS:

$$\text{LET } A = A_0 \frac{s_a}{s + s_a} \quad s = j\omega$$

AND ASSUME THE VOLTAGE VARIABLES ARE COMPLEX AMPLITUDES.

A LOW PASS FILTER



SUBSTITUTE  $A(s)$  FOR  $A$  IN EXPRESSIONS PREVIOUSLY DEVELOPED

NEGATIVE FEEDBACK:

$$\frac{\bar{V}_o}{\bar{V}_i} = \frac{-A_0 \left( \frac{R_2}{R_1 + R_2} \right) \left( \frac{s_a}{s + s_a} \right)}{1 + A_0 \left( \frac{R_1}{R_1 + R_2} \right) \left( \frac{s_a}{s + s_a} \right)} = -A_0 \left( \frac{R_2}{R_1 + R_2} \right) \frac{s_a}{s + s_a + \underbrace{A_0 \left( \frac{R_1}{R_1 + R_2} \right) s_a}_{\text{LOOP GAIN}}}$$

$$\frac{\bar{V}_o}{\bar{V}_i} \approx -A_0 \frac{R_2}{R_1 + R_2} \left( \frac{s_a}{s + s_a A_0 \frac{R_1}{R_1 + R_2}} \right)$$

NOTE THAT TIME CONSTANT

OF RESPONSE OF THE AMPLIFIER IS NOW NOT  $\frac{1}{s_a}$  BUT  $\frac{1}{s_a} \times \frac{1}{A_0 \frac{R_1}{R_1 + R_2}}$  WHICH IS SMALLER BY A FACTOR OF  $1/A_0 \left( \frac{R_1}{R_1 + R_2} \right)$

THE BANDWIDTH OF THE AMPLIFIER IS LARGER BY THE SAME FACTOR

POSITIVE FEEDBACK: ANALYSIS IS IDENTICAL

$$\frac{\bar{V}_o}{\bar{V}_i} \approx A_0 \frac{R_2}{R_1 + R_2} \left( \frac{s_a}{s + s_a A_0 \frac{R_2}{R_1 + R_2}} \right)$$

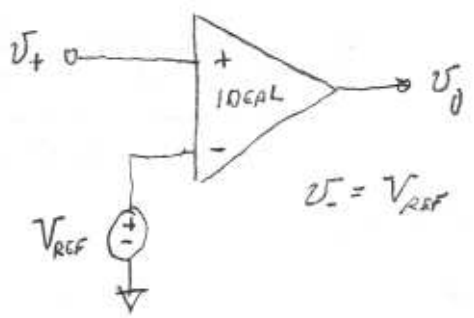
ROOT IS NOW IN THE RIGHT HALF PLANE

THE CHARACTERISTIC EQUATION IS  $s - s_a A_0 \frac{R_2}{R_1 + R_2}$

OR  $s = + s_a A_0 \frac{R_2}{R_1 + R_2}$  THE TRANSIENT RESPONSE IS  $e^{st}$

WHICH IS A GROWING EXPONENTIAL UNSTABLE!

AN OP-AMP CAN BE USED AS A COMPARATOR BY EXPLOITING THE LIMITS ( $\pm V_S$ , THE SUPPLY VOLTAGES) ON THE OUTPUT VOLTAGE.

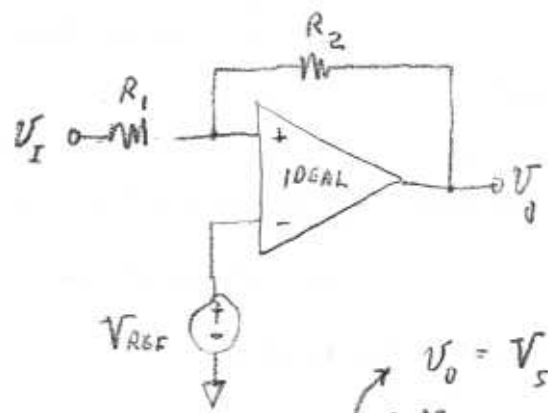


IF  $V_+ < V_{REF}$ ,  $V_0 = -V_S$

IF  $V_+ > V_{REF}$ ,  $V_0 = +V_S$

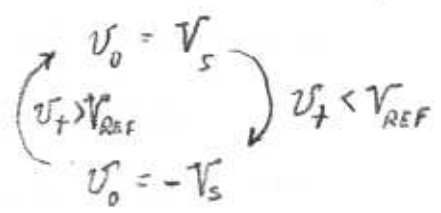
SLEW RATE IS USUALLY HIGH ( $\sim 20 \text{ V}/\mu\text{SEC}$ )

CONSIDER THE EFFECT OF POSITIVE FEEDBACK AROUND THE COMPARATOR:



$V_+ = V_I \frac{R_2}{R_1 + R_2} + V_0 \frac{R_1}{R_1 + R_2}$  (SUPERPOSITION)

IF  $V_+ > V_{REF}$ ,  $V_0 = +V_S$   
IF  $V_+ < V_{REF}$ ,  $V_0 = -V_S$  } TWO STABLE STATES



ASSUME CIRCUIT IS IN  $V_0 = -V_S$ . WHAT IS THE CONSTRAINT ON  $V_I$  TO STAY THERE?

$V_+ < V_{REF}$  OR:  $(V_I \frac{R_2}{R_1 + R_2} - V_S \frac{R_1}{R_1 + R_2}) < V_{REF}$

EQUIVALENTLY:  $V_I < V_{REF} \left( \frac{R_1 + R_2}{R_2} \right) + V_S \frac{R_1}{R_2}$

ASSUME CIRCUIT IS IN THE STATE  $V_0 = +V_S$ . THE CORRESPONDING CONDITION TO STAY THERE IS:

$V_+ > V_{REF}$  OR:  $V_I > V_{REF} \left( \frac{R_1 + R_2}{R_2} \right) - V_S \frac{R_1}{R_2}$

CONDITION FOR STAYING IN STATE:

IN SUMMARY:

IN  $+V_S$  STATE:

$$V_I > V_{REF} \left( \frac{R_1 + R_2}{R_2} \right) - V_S \frac{R_1}{R_2}$$

$\uparrow V_I$  INCREASE

$\downarrow V_I$  DECREASES

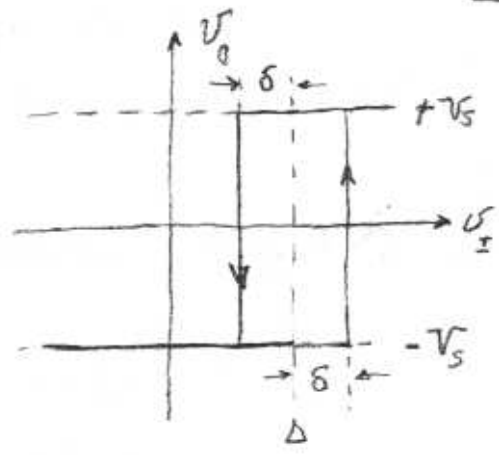
IN  $-V_S$  STATE:

$$V_I < V_{REF} \left( \frac{R_1 + R_2}{R_2} \right) + V_S \frac{R_1}{R_2}$$



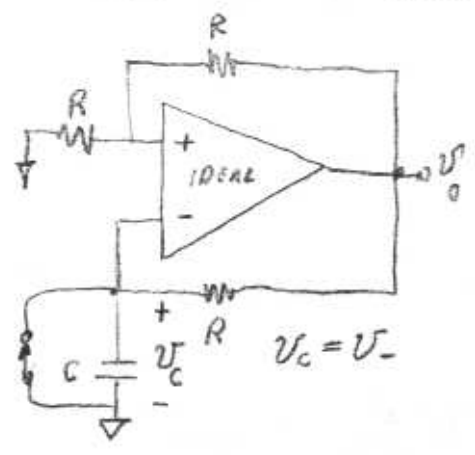
GRAPHICALLY:

HYSTERESIS  
BY INTENTION



A MEMBER OF A FAMILY OF CIRCUITS KNOWN AS "SCHMITT TRIGGERS"

THIS CIRCUIT, WITH BISTABILITY PRODUCED BY POSITIVE FEEDBACK, CAN EASILY BE MADE INTO A SIGNAL GENERATOR OR OSCILLATOR:



INITIALLY THE SWITCH IS CLOSED

ASSUME CIRCUIT IS IN  $+V_S$  STATE I.E.  $V_O = +V_S$

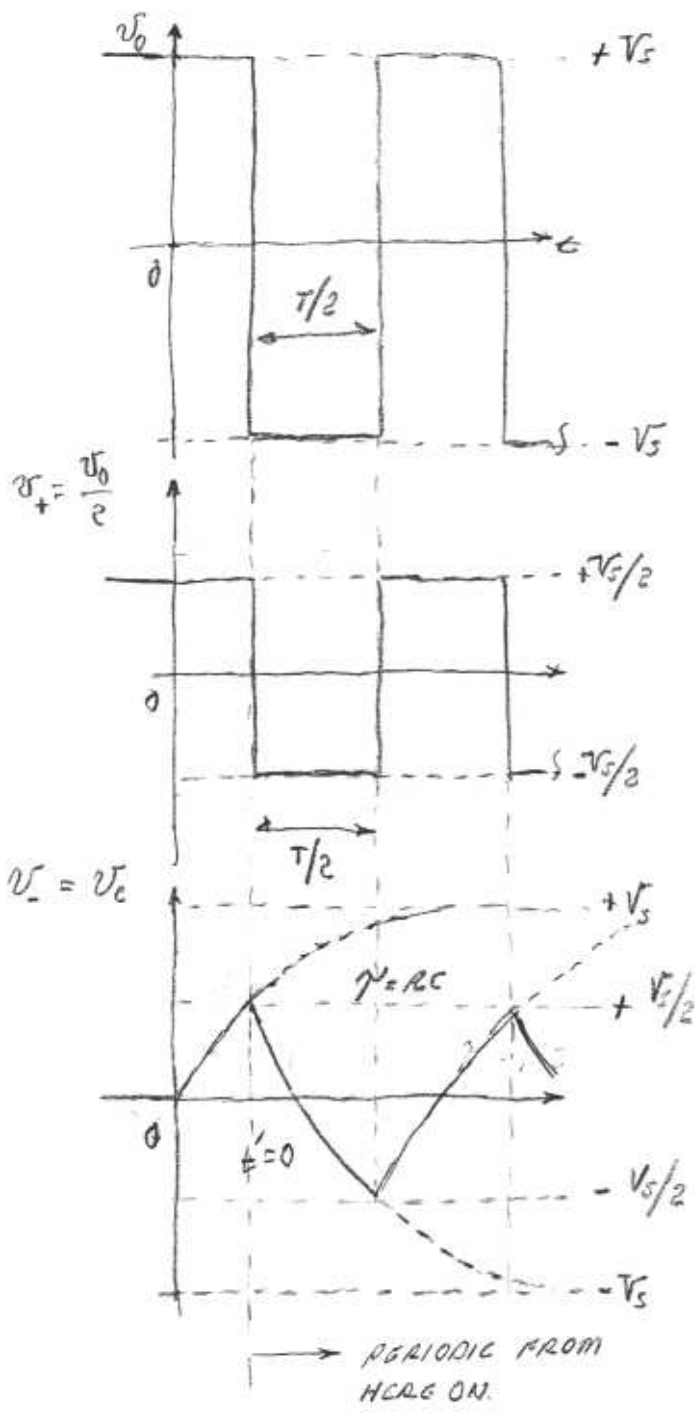
(WITH SWITCH CLOSED CIRCUIT LOOKS LIKE SCHMITT TRIGGER WITH  $V_{REF} = 0$ )

LET SWITCH OPEN AT  $t=0$   $V_C$  INCREASES TOWARD  $+V_S$ .

WHEN IT REACHES  $\frac{V_S}{2}$ ,  $V_C > V_+$  AND STATE CHANGES TO  $V_O = -V_S$

$V_C$  NOW DECREASES TOWARD  $-V_S$ , WITH THE STATE CHANGING AGAIN WHEN IT REACHES  $-\frac{V_S}{2}$  MAKING  $V_C < V_+$

AND THE CYCLE CONTINUES



TO DETERMINE THE PERIOD FOCUS ON INTERVAL MARKED  $T/2$  AND LET  $t' = 0$  AT START OF THIS INTERVAL. BY INSPECTION:

$$v_c(t') = -V_s + \frac{3}{2}V_s e^{-t'/\tau}$$

THIS INTERVAL ENDS WHEN

$$v_c(t') = -V_s/2 \text{ OR WHEN}$$

$$e^{-t'/\tau} = \frac{1}{3} \text{ AT THIS TIME } t' = T/2$$

$$\frac{T}{2} = \tau \ln 3$$

$$T = 2\tau \ln 3$$

THE CLOCK IN LAB #4 IS DIFFERENT IN DETAIL, BUT RELIES ON POSITIVE FEEDBACK AROUND AN AMPLIFIER, A FET INVERTER, WHICH SATURATES AT BOTH ENDS OF THE TRANSFER CHARACTERISTIC.

THE ANALYSIS PROCEEDS AS IN THE CIRCUIT ABOVE.