6.003: Signals and Systems

Continuous-Time Systems

September 20, 2011

Multiple Representations of Discrete-Time Systems

Discrete-Time (DT) systems can be represented in different ways to more easily address different types of issues.

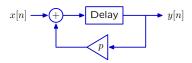
Verbal descriptions: preserve the rationale.

"Next year, your account will contain p times your balance from this year plus the money that you added this year."

Difference equations: mathematically compact.

$$y[n+1] = x[n] + py[n]$$

Block diagrams: illustrate signal flow paths.



Operator representations: analyze systems as polynomials.

$$(1 - p\mathcal{R})Y = \mathcal{R}X$$

Multiple Representations of Continuous-Time Systems

Similar representations for Continuous-Time (CT) systems.

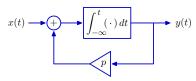
Verbal descriptions: preserve the rationale.

"Your account will grow in proportion to your balance plus the rate at which you deposit."

Differential equations: mathematically compact.

$$\frac{dy(t)}{dt} = x(t) + py(t)$$

Block diagrams: illustrate signal flow paths.

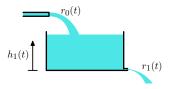


Operator representations: analyze systems as polynomials.

$$(1 - p\mathcal{A})Y = \mathcal{A}X$$

Differential Equations

Differential equations are mathematically precise and compact.



We can represent the tank system with a differential equation.

$$\frac{dr_1(t)}{dt} = \frac{r_0(t) - r_1(t)}{\tau}$$

You already know lots of methods to solve differential equations:

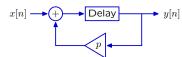
- general methods (separation of variables; integrating factors)
- homogeneous and particular solutions
- inspection

Today: new methods based on **block diagrams** and **operators**, which provide new ways to think about systems' behaviors.

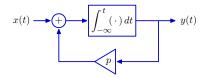
Block Diagrams

Block diagrams illustrate signal flow paths.

DT: adders, scalers, and delays – represent systems described by linear difference equations with constant coefficients.



CT: adders, scalers, and integrators – represent systems described by a linear differential equations with constant coefficients.



Delays in DT are replaced by integrators in CT.

Operator Representation

CT Block diagrams are concisely represented with the ${\mathcal A}$ operator.

Applying $\mathcal A$ to a CT signal generates a new signal that is equal to the integral of the first signal at all points in time.

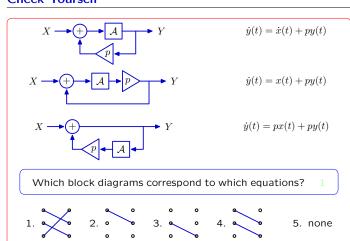
$$Y = AX$$

is equivalent to

$$y(t) = \int_{-\infty}^{t} x(\tau) \, d\tau$$

for all time t.

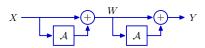
Check Yourself



Evaluating Operator Expressions

As with \mathcal{R} , \mathcal{A} expressions can be manipulated as polynomials.

Example:



$$w(t) = x(t) + \int_{-\infty}^{t} x(\tau)d\tau$$

$$y(t) = w(t) + \int_{-\infty}^{t} w(\tau)d\tau$$

$$y(t) = x(t) + \int_{-\infty}^{t} x(\tau)d\tau + \int_{-\infty}^{t} x(\tau)d\tau + \int_{-\infty}^{t} \left(\int_{-\infty}^{\tau_2} x(\tau_1)d\tau_1\right)d\tau_2$$

$$W = (1 + \mathcal{A}) X$$

$$Y = (1 + A) W = (1 + A)(1 + A) X = (1 + 2A + A^{2}) X$$

Evaluating Operator Expressions

Expressions in ${\mathcal A}$ can be manipulated using rules for polynomials.

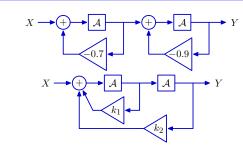
• Commutativity: A(1-A)X = (1-A)AX

• Distributivity: $A(1-A)X = (A-A^2)X$

• Associativity: $((1-\mathcal{A})\mathcal{A})(2-\mathcal{A})X = (1-\mathcal{A})(\mathcal{A}(2-\mathcal{A}))X$

Check Yourself

Determine k_1 so that these systems are "equivalent."

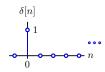


1. 0.7 2. 0.9 3. 1.6 4. 0.63 5. none of these

Elementary Building-Block Signals

Elementary DT signal: $\delta[n]$.

$$\delta[n] = \begin{cases} 1, & \text{if } n = 0; \\ 0, & \text{otherwise} \end{cases}$$



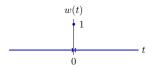
- simplest non-trivial signal (only one non-zero value)
- shortest possible duration (most "transient")
- useful for constructing more complex signals

What CT signal serves the same purpose?

Elementary CT Building-Block Signal

Consider the analogous CT signal: w(t) is non-zero only at t=0.

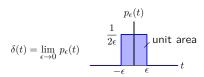
$$w(t) = \begin{cases} 0 & t < 0 \\ 1 & t = 0 \\ 0 & t > 0 \end{cases}$$

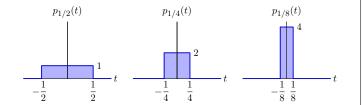


Is this a good choice as a building-block signal?

Unit-Impulse Signal

The unit-impulse signal acts as a pulse with unit area but zero width.





Unit-Impulse Signal

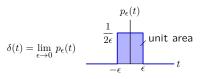
The unit-impulse function is represented by an arrow with the number 1, which represents its area or "weight."



It has two seemingly contradictory properties:

- ullet it is nonzero only at t=0, and
- its definite integral $(-\infty, \infty)$ is one!

Both of these properties follow from thinking about $\delta(t)$ as a limit:



Unit-Impulse and Unit-Step Signals

The indefinite integral of the unit-impulse is the unit-step.

$$u(t) = \int_{-\infty}^{-t} \delta(\lambda) \, d\lambda = \begin{cases} 1; & t \geq 0 \\ 0; & \text{otherwise} \end{cases}$$

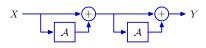


Equivalently

$$\delta(t) \longrightarrow \mathcal{A} \longrightarrow u(t)$$

Impulse Response of Acyclic CT System

If the block diagram of a CT system has no feedback (i.e., no cycles), then the corresponding operator expression is "imperative."



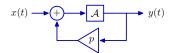
$$Y = (1 + A)(1 + A) X = (1 + 2A + A^{2}) X$$

If
$$x(t) = \delta(t)$$
 then

$$y(t) = (1 + 2\mathcal{A} + \mathcal{A}^2)\,\delta(t) = \delta(t) + 2u(t) + tu(t)$$

CT Feedback

Find the impulse response of this CT system with feedback.



Method 1: find differential equation and solve it.

$$\dot{y}(t) = x(t) + py(t)$$

Linear, first-order difference equation with constant coefficients.

Try
$$y(t) = Ce^{\alpha t}u(t)$$
.

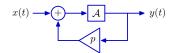
Then
$$\dot{y}(t) = \alpha C e^{\alpha t} u(t) + C e^{\alpha t} \delta(t) = \alpha C e^{\alpha t} u(t) + C \delta(t)$$
.

Substituting, we find that $\alpha Ce^{\alpha t}u(t) + C\delta(t) = \delta(t) + pCe^{\alpha t}u(t)$.

Therefore
$$\alpha = p$$
 and $C = 1 \rightarrow y(t) = e^{pt}u(t)$.

CT Feedback

Find the impulse response of this CT system with feedback.



Method 2: use operators.

$$Y = \mathcal{A}(X + pY)$$
$$\frac{Y}{X} = \frac{\mathcal{A}}{1 - p\mathcal{A}}$$

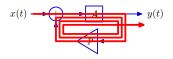
Now expand in ascending series in
$$\mathcal{A}$$
:
$$\frac{Y}{X} = \mathcal{A}(1 + p\mathcal{A} + p^2\mathcal{A}^2 + p^3\mathcal{A}^3 + \cdots)$$

If
$$x(t) = \delta(t)$$
 then

$$\begin{split} y(t) &= \mathcal{A}(1 + p\mathcal{A} + p^2\mathcal{A}^2 + p^3\mathcal{A}^3 + \cdots) \, \delta(t) \\ &= (1 + pt + \frac{1}{2}p^2t^2 + \frac{1}{6}p^3t^3 + \cdots) \, u(t) = e^{pt}u(t) \,. \end{split}$$

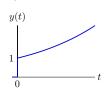
CT Feedback

We can visualize the feedback by tracing each cycle through the cyclic signal path.



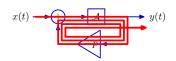
$$y(t) = (A + pA^2 + p^2A^3 + p^3A^4 + \cdots) \delta(t)$$

= $(1 + pt + \frac{1}{2}p^2t^2 + \frac{1}{6}p^3t^3 + \cdots) u(t) = e^{pt}u(t)$

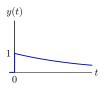


CT Feedback

Making p negative makes the output converge (instead of diverge).

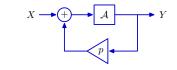


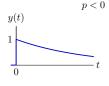
$$\begin{split} y(t) &= \left(\mathcal{A} - p\mathcal{A}^2 + p^2\mathcal{A}^3 - \frac{p^3\mathcal{A}^4}{6} + \cdots\right)\delta(t) \\ &= \left(1 - pt + \frac{1}{2}p^2t^2 - \frac{1}{6}p^3t^3 + \cdots\right)u(t) = e^{-pt}u(t) \end{split}$$

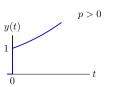


Convergent and Divergent Poles

The fundamental mode associated with p converges if p < 0 and diverges if p > 0.

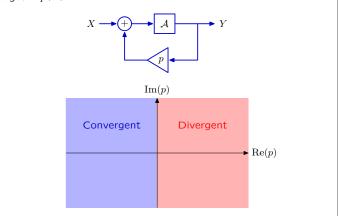






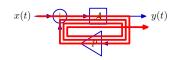
Convergent and Divergent Poles

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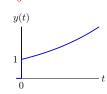


CT Feedback

In CT, each cycle adds a new integration.



$$\begin{split} y(t) &= (\mathcal{A} + p\mathcal{A}^2 + p^2\mathcal{A}^3 + p^3\mathcal{A}^4 + \cdots) \, \delta(t) \\ &= (1 + pt + \frac{1}{2}p^2t^2 + \frac{1}{6}p^3t^3 + \cdots) \, u(t) = e^{pt}u(t) \end{split}$$



DT Feedback

In DT, each cycle creates another sample in the output.

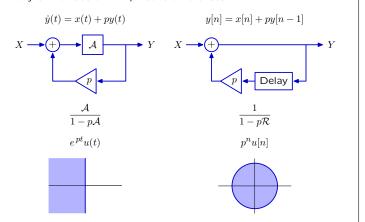


 $y[n] = (1 + p\mathcal{R} + p^2\mathcal{R}^2 + p^3\mathcal{R}^3 + \frac{p^4\mathcal{R}^4}{p^4} + \cdots) \delta[n]$ = $\delta[n] + p\delta[n-1] + p^2\delta[n-2] + p^3\delta[n-3] + \frac{p^4\delta[n-4]}{p^4} + \cdots$



Summary: CT and DT representations

Many similarities and important differences.



Check Yourself

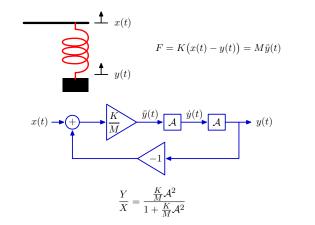
Which functionals represent convergent systems?

$$\begin{array}{ccc} \frac{1}{1 - \frac{1}{4}\mathcal{R}^2} & & \frac{1}{1 - \frac{1}{4}\mathcal{A}^2} \\ \\ \frac{1}{1 + 2\mathcal{R} + \frac{3}{4}\mathcal{R}^2} & & \frac{1}{1 + 2\mathcal{A} + \frac{3}{4}\mathcal{A}^2} \end{array}$$

1.
$$\sqrt[4]{x}$$
 2. $\sqrt[4]{x}$ 3. $\sqrt[4]{y}$ 4. $\sqrt[4]{x}$ 5. none of these

Mass and Spring System

Use the $\ensuremath{\mathcal{A}}$ operator to solve the mass and spring system.



Mass and Spring System

Factor system functional to find the poles.

$$\frac{Y}{X} = \frac{\frac{K}{M}\mathcal{A}^2}{1 + \frac{K}{M}\mathcal{A}^2} = \frac{\frac{K}{M}\mathcal{A}^2}{(1 - p_0\mathcal{A})(1 - p_1\mathcal{A})}$$

$$1 + \frac{K}{M}A^2 = 1 - (p_0 + p_1)A + p_0p_1A^2$$

The sum of the poles must be zero.

The product of the poles must be K/M.

$$p_0 = j\sqrt{\frac{K}{M}} \quad p_1 = -j\sqrt{\frac{K}{M}}$$

Mass and Spring System

Alternatively, find the poles by substituting $\mathcal{A} \to \frac{1}{s}.$ The poles are then the roots of the denominator.

$$\frac{Y}{X} = \frac{\frac{K}{M}\mathcal{A}^2}{1 + \frac{K}{M}\mathcal{A}^2}$$

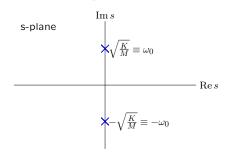
Substitute $\mathcal{A} \to \frac{1}{s}$:

$$\frac{Y}{X} = \frac{\frac{K}{M}}{s^2 + \frac{K}{M}}$$

$$s = \pm j\sqrt{\frac{K}{M}}$$

Mass and Spring System

The poles are complex conjugates.



The corresponding fundamental modes have complex values.

fundamental mode 1: $e^{j\omega_0t}=\cos\omega_0t+j\sin\omega_0t$

fundamental mode 2: $e^{-j\omega_0 t} = \cos \omega_0 t - j \sin \omega_0 t$

Mass and Spring System

Real-valued inputs always excite combinations of these modes so that the imaginary parts cancel.

Example: find the impulse response.

$$\begin{split} \frac{Y}{X} &= \frac{\frac{K}{M}\mathcal{A}^2}{1 + \frac{K}{M}\mathcal{A}^2} = \frac{\frac{K}{M}}{p_0 - p_1} \left(\frac{\mathcal{A}}{1 - p_0 \mathcal{A}} - \frac{\mathcal{A}}{1 - p_1 \mathcal{A}} \right) \\ &= \frac{\omega_0^2}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} - \frac{\mathcal{A}}{1 + j\omega_0 \mathcal{A}} \right) \\ &= \frac{\omega_0}{2j} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) - \frac{\omega_0}{2j} \left(\frac{\mathcal{A}}{1 + j\omega_0 \mathcal{A}} \right) \\ &= \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) - \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 + j\omega_0 \mathcal{A}} \right) \\ &= \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) - \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) \\ &= \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) - \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) \\ &= \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) - \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) \\ &= \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) - \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) \\ &= \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) - \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) \\ &= \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) - \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) \\ &= \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) - \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) \\ &= \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) - \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) \\ &= \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) - \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) \\ &= \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) - \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) \\ &= \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) - \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) \\ &= \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) - \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) \\ &= \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) - \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) \\ &= \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) - \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) \\ &= \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) - \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) \\ &= \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) - \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) \\ &= \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) \\ &= \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) \\ &= \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) \\ &= \frac{\omega_0}{2j\omega_0} \left(\frac{\mathcal{A}}{1$$

The modes themselves are complex conjugates, and their coefficients are also complex conjugates. So the sum is a sum of something and its complex conjugate, which is real.

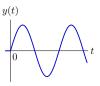
Mass and Spring System

The impulse response is therefore real.

$$\frac{Y}{X} = \frac{\omega_0}{2j} \left(\frac{\mathcal{A}}{1 - j\omega_0 \mathcal{A}} \right) - \frac{\omega_0}{2j} \left(\frac{\mathcal{A}}{1 + j\omega_0 \mathcal{A}} \right)$$

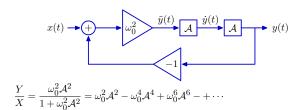
The impulse response is

$$h(t) = \frac{\omega_0}{2j} e^{j\omega_0 t} - \frac{\omega_0}{2j} e^{-j\omega_0 t} = \omega_0 \sin \omega_0 t \, ; \quad t>0 \label{eq:hamiltonian}$$



Mass and Spring System

Alternatively, find impulse response by expanding system functional.



If $x(t) = \delta(t)$ then

$$y(t) = \omega_0^2 t - \omega_0^4 \frac{t^3}{3!} + \omega_0^6 \frac{t^5}{5!} - + \cdots, \ t \ge 0$$

Mass and Spring System

Look at successive approximations to this infinite series.

$$\frac{Y}{X} = \frac{\omega_0^2 \mathcal{A}^2}{1 + \omega_0^2 \mathcal{A}^2} = \omega_0^2 \mathcal{A}^2 \sum_{l=0}^{\infty} \left(-\omega_0^2 \mathcal{A}^2 \right)^l$$

If $x(t) = \delta(t)$ then

$$y(t) = \sum_{l=0}^{\infty} \omega_0^2 \left(-\omega_0^2\right)^l A^{2l+2} \delta(t)$$
$$= \omega_0^2 t - \omega_0^4 \frac{t^3}{3!} + \omega_0^6 \frac{t^5}{5!} - \omega_0^8 \frac{t^7}{7!}$$



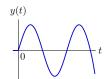
Mass and Spring System

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$$\frac{Y}{X} = \frac{\omega_0^2 \mathcal{A}^2}{1 + \omega_0^2 \mathcal{A}^2} = \omega_0^2 \mathcal{A}^2 \sum_{l=0}^{\infty} \left(-\omega_0^2 \mathcal{A}^2 \right)^l$$

If $x(t) = \delta(t)$ then

$$\begin{split} y(t) &= \sum_{l=0}^{\infty} \omega_0^2 \left(-\omega_0^2 \right)^l \mathcal{A}^{2l+2} \delta(t) \\ &= \omega_0^2 t - \omega_0^4 \frac{t^3}{3!} + \omega_0^6 \frac{t^5}{5!} - \omega_0^8 \frac{t^7}{7!} + \omega_0^{10} \frac{t^9}{9!} - + \dots = \omega_0 \sin \omega_0 t \end{split}$$



Summary: CT and DT representations

Many similarities and important differences.

