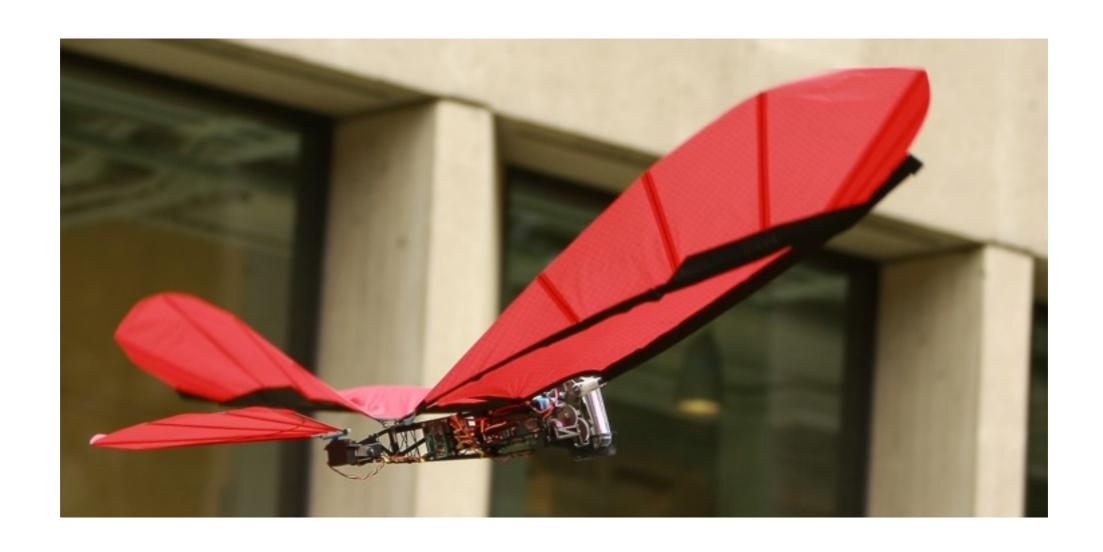
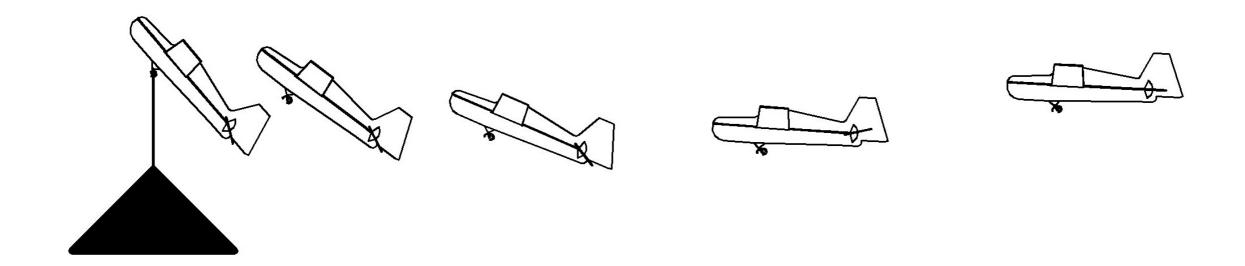
6.003: Signals and Systems

Feedback and Control

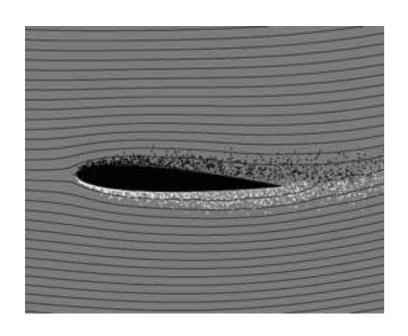


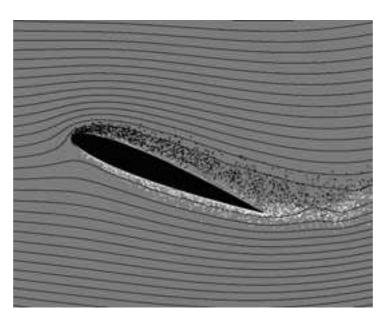
Example: Perching

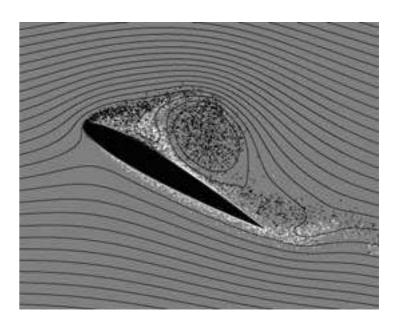
Can we make a fixed-wing UAV land on a perch like a bird?



The "Perching" Problem











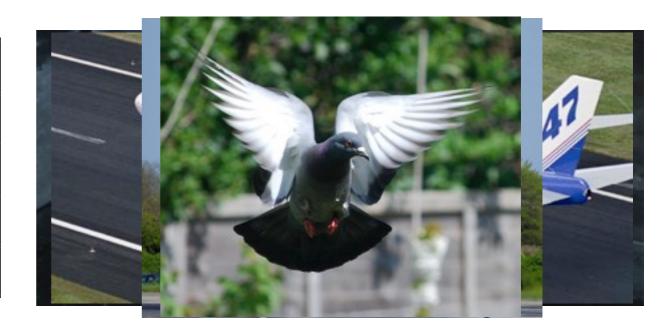
Dimensionless Analysis

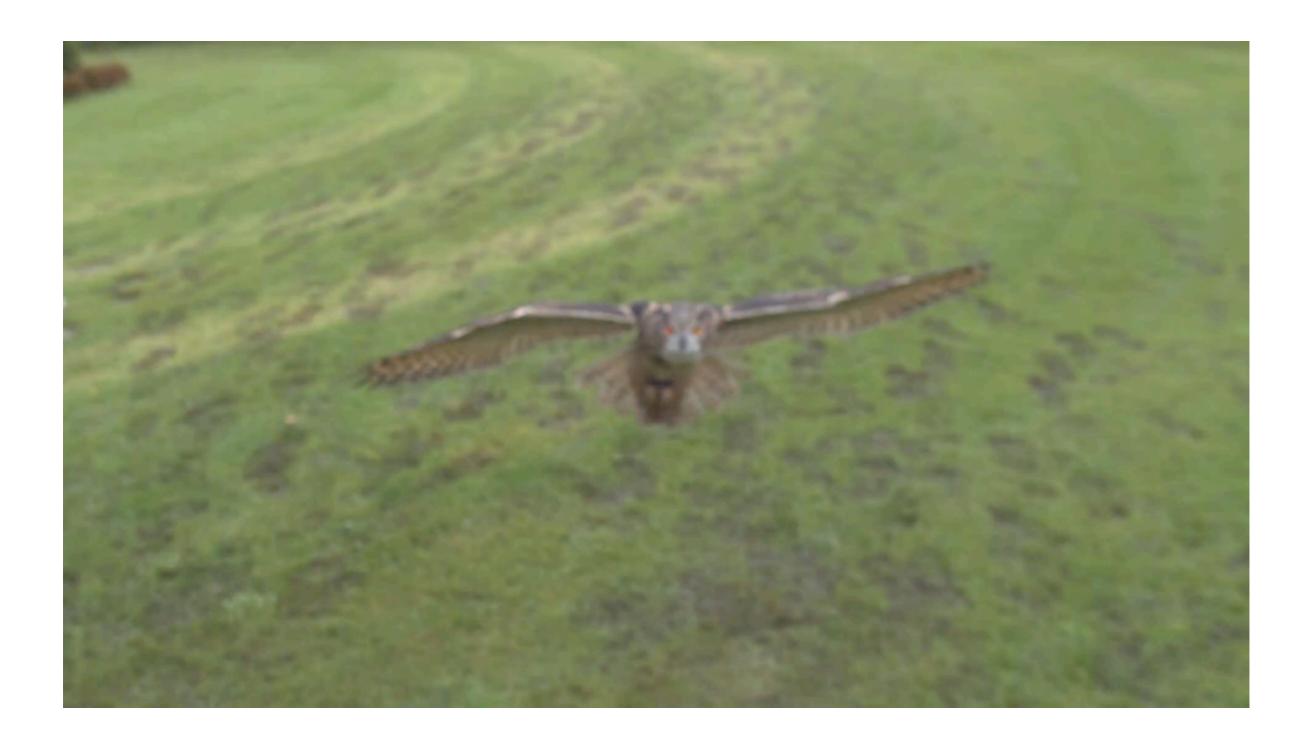
- Bird or plane...
 - with mass m, wing area S, operating in a fluid with density ρ
 - which requires a distance x to slow from V_0 to V_f
- Distance-averaged drag coefficient, C_{D:}

$$\langle C_D \rangle = \frac{2m}{\rho Sx} \ln \left(\frac{V_0}{V_f} \right)$$

A few (very preliminary) reference points:

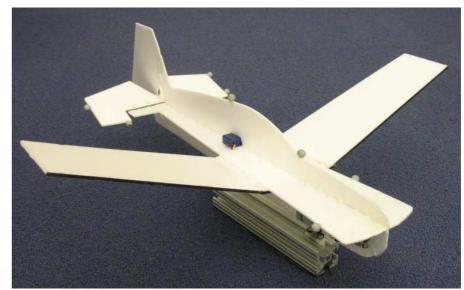
Vehicle	Average C _D
Boeing 747	0.16
X-31	0.3
Cornell Perching Plane	0.25
Common Pigeon	10

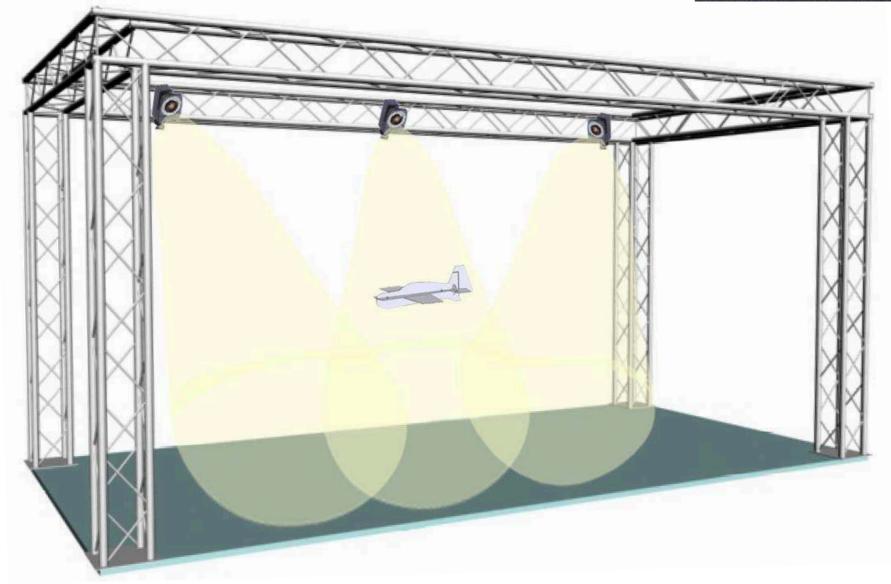




Experiment Design

- Glider (no propellor)
- Flat plate wings
- Dihedral (passive roll stability)
- Offboard sensing and control



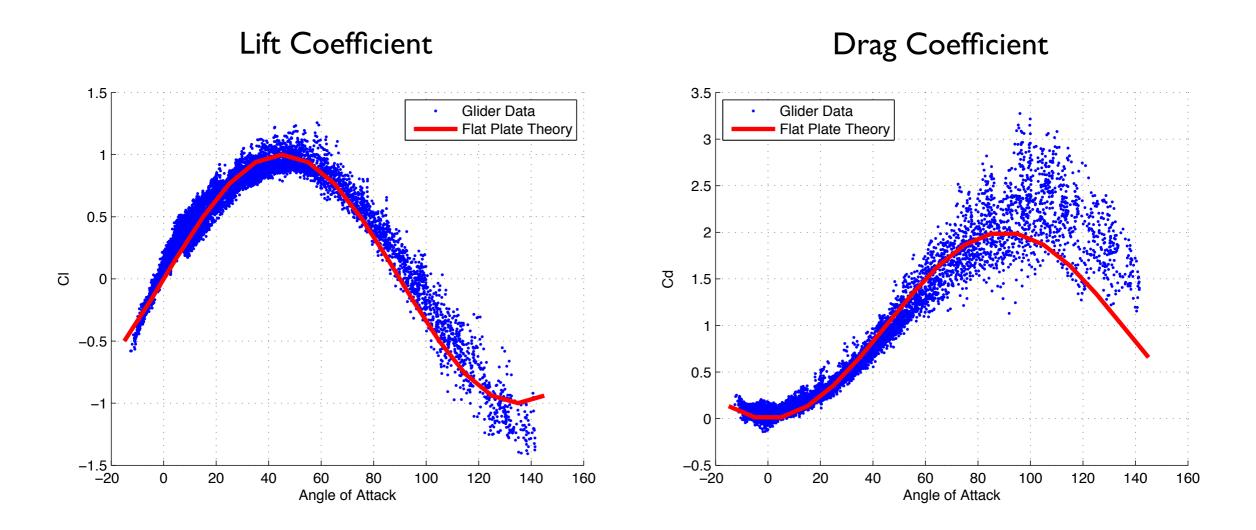


System Identification

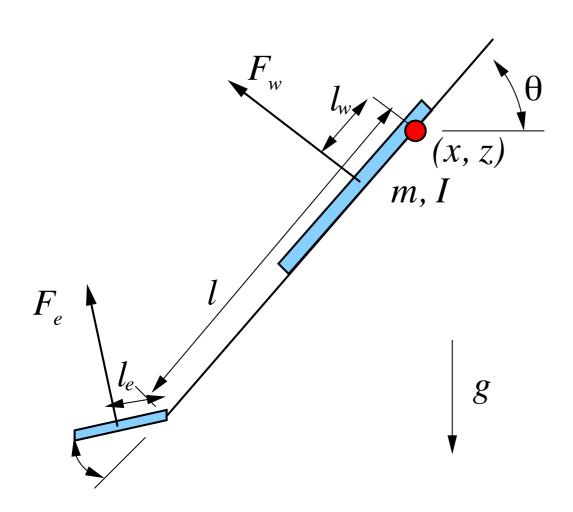
- Nonlinear rigid-body vehicle model
- Linear actuator model (+ saturations, delay)
- Real flight data (no wind tunnel)



System Identification



A Dynamic Model



- Planar dynamics
- Aerodynamics fit from data
- State: $\mathbf{x} = [x, y, \theta, \phi, \dot{x}, \dot{y}, \dot{\theta}]$
- Actuator: $\mathbf{u} = \dot{\phi}$

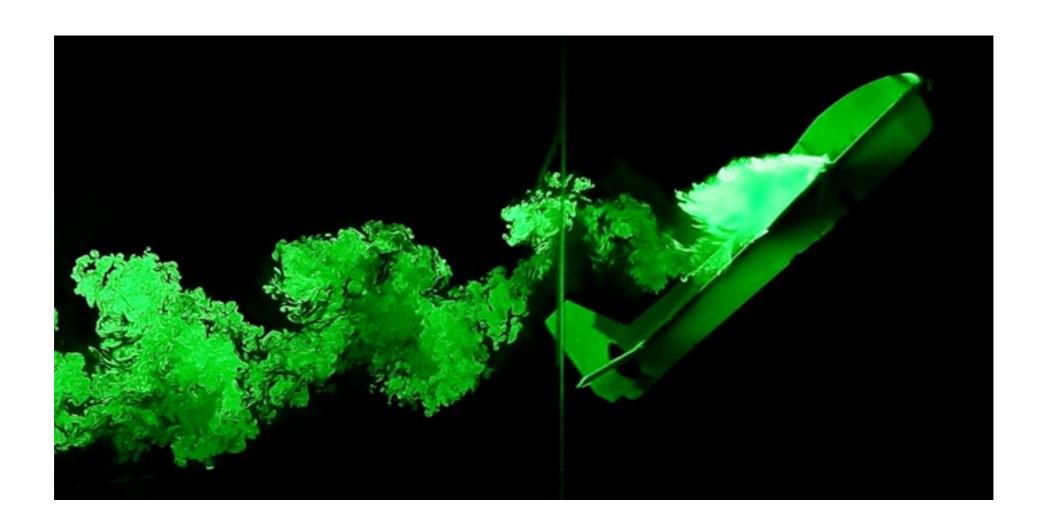
Perching Results

- Enters motion capture @ 6m/s
- Perch in < 3.5*m* away
- Entire trajectory < Is

Requires separation!



Flow visualization

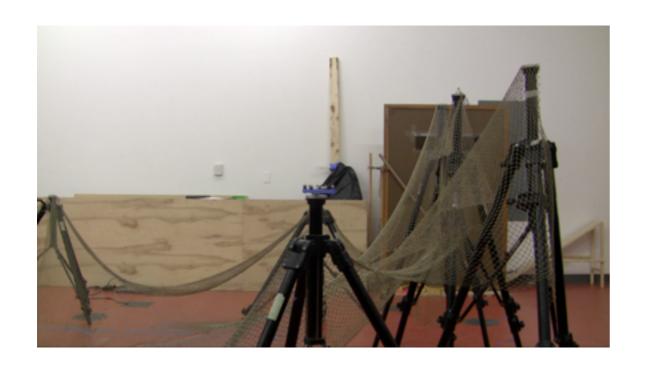


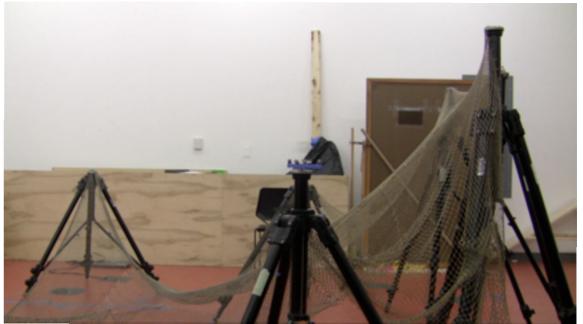
Dimensionless Analysis

Vehicle	Average C _D
Boeing 747	0.16
X-31	0.3
Cornell Perching Plane	0.25
Common Pigeon	10
Our glider	1.1
Cobra maneuver (Mig)	0.9

Feedback is essential...

- to compensate for initial condition errors, disturbances, and imperfect model
- agile airplanes are open loop unstable





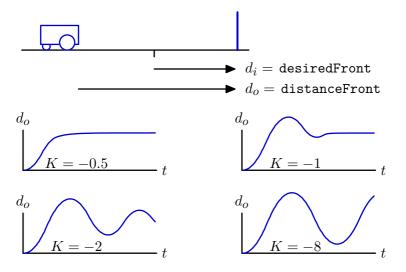
open loop feedback

Today's goal

Use systems theory to gain insight into how to control a system.

Example: wallFinder System

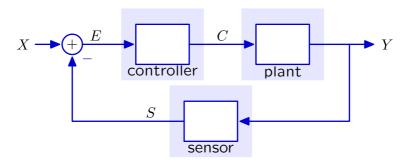
Approach a wall, stopping a desired distance d_i in front of it.



What causes these different types of responses?

Structure of a Control Problem

(Simple) Control systems have three parts.



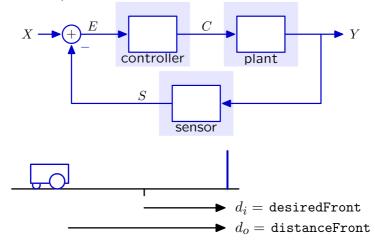
The **plant** is the system to be controlled.

The **sensor** measures the output of the plant.

The **controller** specifies a command C to the plant based on the *difference* between the input X and sensor output S.

Analysis of wallFinder System

Cast wallFinder problem into control structure.

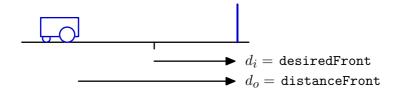


proportional controller:
$$v[n]=Ke[n]=Kig(d_i[n]-d_s[n]ig)$$
 locomotion: $d_o[n]=d_o[n-1]-Tv[n-1]$

sensor with no delay: $d_s[n] = d_o[n]$

Analysis of wallFinder System: Block Diagram

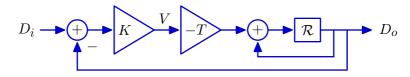
Visualize as block diagram.



proportional controller: $v[n] = Ke[n] = K(d_i[n] - d_s[n])$

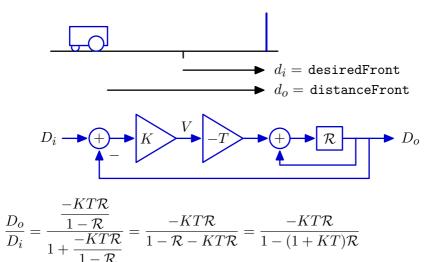
locomotion: $d_o[n] = d_o[n-1] - Tv[n-1]$

sensor with no delay: $d_s[n] = d_o[n]$



Analysis of wallFinder System: System Function

Solve.

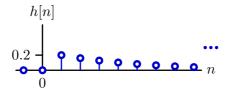


Analysis of wallFinder System: Poles

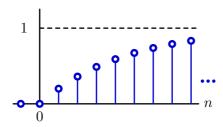
The system function contains a single **pole** at z = 1 + KT.

$$\frac{D_o}{D_i} = \frac{HTR}{1 - (1 + KT)R}$$

Unit-sample response for KT = -0.2:



Unit-step response s[n] for KT = -0.2:



What determines the speed of the response? Could it be faster?

Check Yourself

Find KT for fastest convergence of unit-sample response.

$$\frac{D_o}{D_i} = \frac{-KT\mathcal{R}}{1 - (1 + KT)\mathcal{R}}$$

- 1. KT = -2
- 2. KT = -1
- 3. KT = 0
- 4. KT = 1
- 5. KT = 2
- 0. none of the above

Check Yourself

Find KT for fastest convergence of unit-sample response.

$$\frac{D_o}{D_i} = \frac{-KT\mathcal{R}}{1 - (1 + KT)\mathcal{R}}$$

If KT = -1 then the pole is at z = 0.

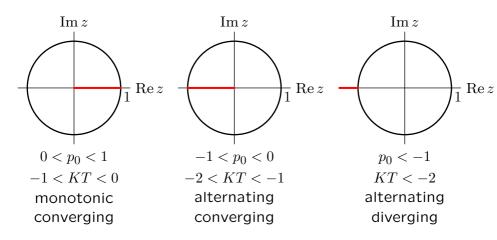
$$\frac{D_o}{D_i} = \frac{-KT\mathcal{R}}{1 - (1 + KT)\mathcal{R}} = \mathcal{R}$$

Unit-sample response has a single non-zero output sample, at n=1.

Analysis of wallFinder System: Poles

The poles of the system function provide insight for choosing K.

$$\frac{D_o}{D_i} = \frac{-KT\mathcal{R}}{1 - (1 + KT)\mathcal{R}} = \frac{(1 - p_o)\mathcal{R}}{1 - p_o\mathcal{R}} \; ; \quad p_0 = 1 + KT$$



Check Yourself

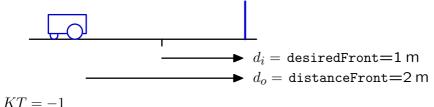
Find KT for fastest convergence of unit-sample response.

$$\frac{D_o}{D_i} = \frac{-KT\mathcal{R}}{1 - (1 + KT)\mathcal{R}}$$

- 1. KT = -2
- 2. KT = -1
- 3. KT = 0
- 4. KT = 1
- 5. KT = 2
- 0. none of the above

Analysis of wallFinder System

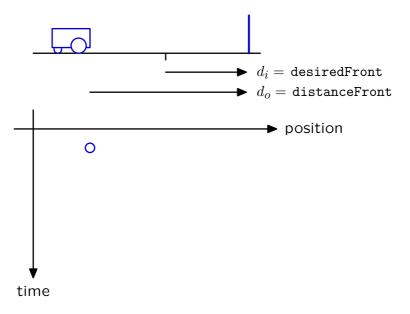
The optimum gain K moves robot to desired position in **one** step.

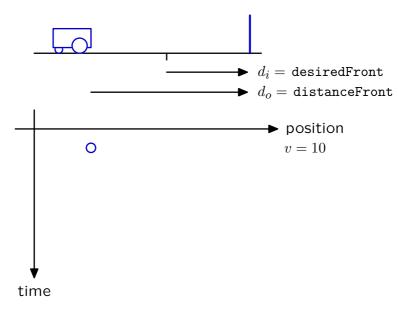


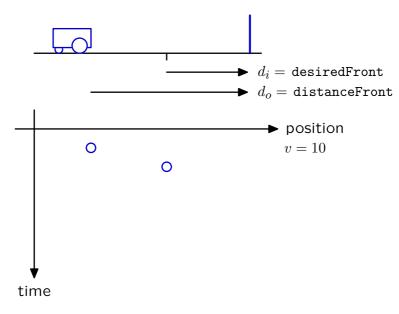
$$K=-rac{1}{T}=-rac{1}{1/10}=-10$$

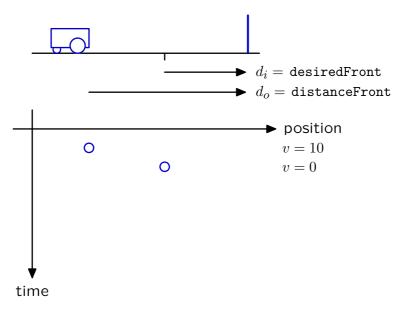
$$v[n]=Kig(d_i[n]-d_o[n]ig)=-10ig(1-2ig)=10 \text{ m/s}$$

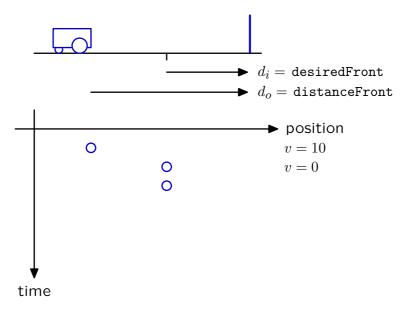
exactly the right speed to get there in one step!

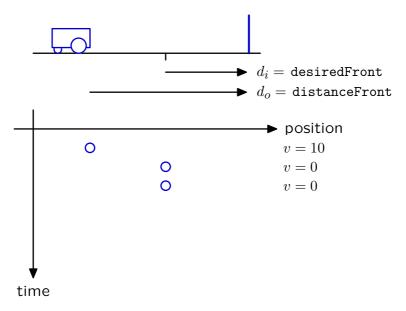


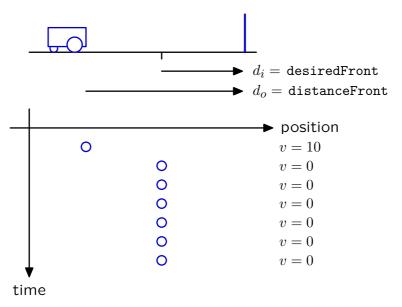






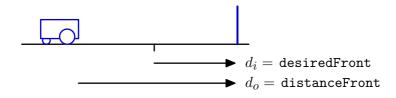






Analysis of wallFinder System: Adding Sensor Delay

Adding delay tends to destabilize control systems.



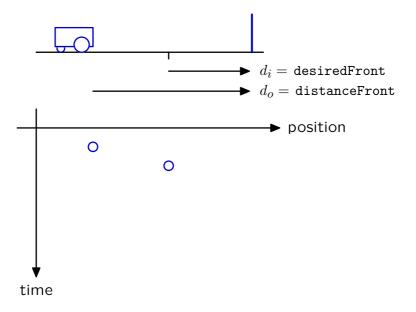
proportional controller:
$$v[n] = Ke[n] = K(d_i[n] - d_s[n])$$

locomotion:
$$d_o[n] = d_o[n-1] - Tv[n-1]$$

sensor with delay: $d_s[n] = d_o[n-1]$

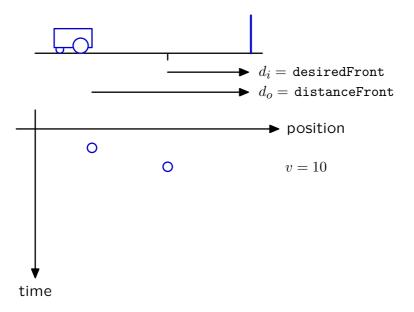
Analysis of wallFinder System: Adding Sensor Delay

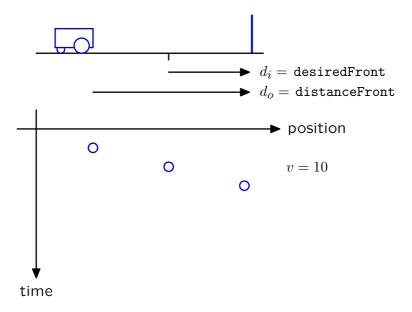
Adding delay tends to destabilize control systems.

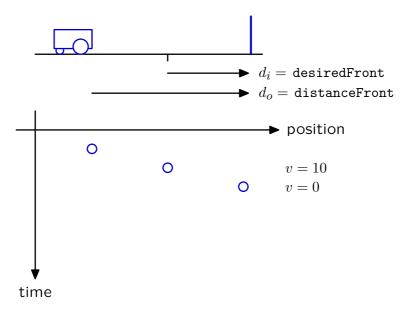


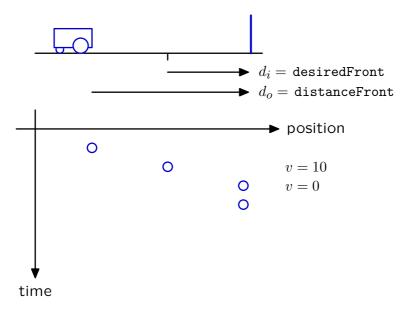
Analysis of wallFinder System: Adding Sensor Delay

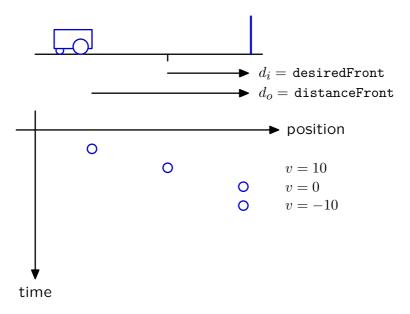
Adding delay tends to destabilize control systems.

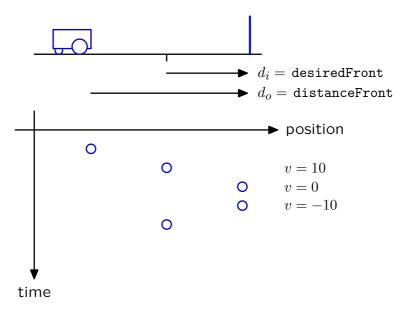


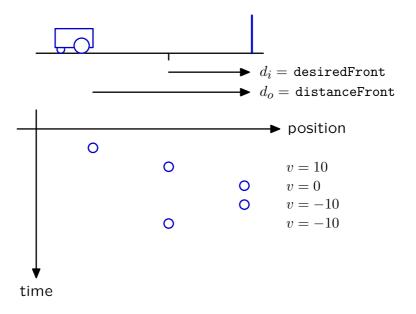


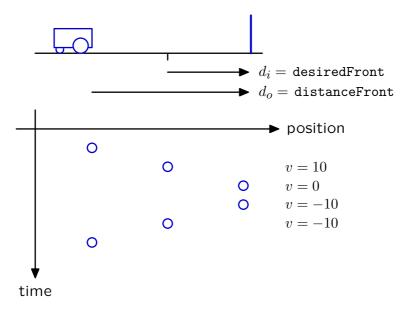


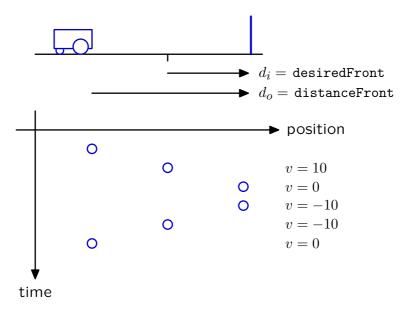


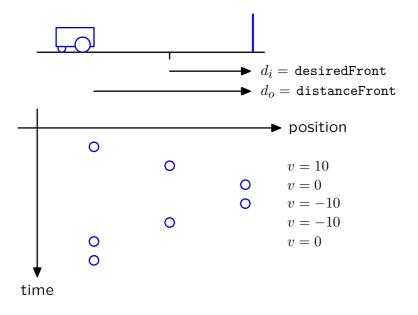






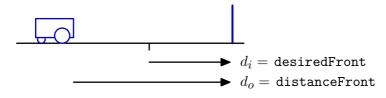






Analysis of wallFinder System: Block Diagram

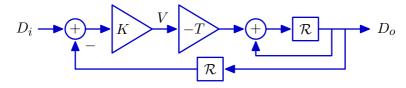
Incorporating sensor delay in block diagram.



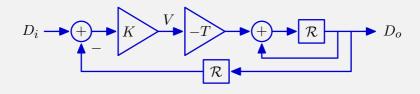
proportional controller: $v[n] = Ke[n] = K(d_i[n] - d_s[n])$

Iocomotion: $d_o[n] = d_o[n-1] - Tv[n-1]$

sensor with delay: $d_s[n] = d_o[n-1]$



Find the system function $H = \frac{D_o}{D_i}$.



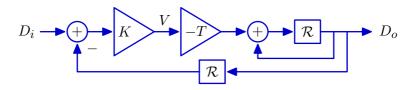
1. $\frac{KTR}{1-R}$

 $2. \frac{1177}{1 + \mathcal{R} - KT\mathcal{R}}$

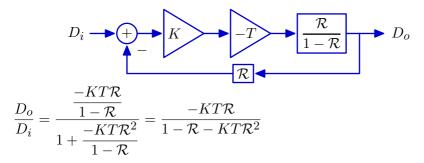
3. $\frac{KTR}{1-R} - KTR$

- 4. $\frac{-KTR}{1-R-KTR}$
- 5. none of the above

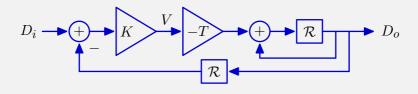
Find the system function $H = \frac{D_o}{D_i}$.



Replace accumulator with equivalent block diagram.



Find the system function $H=rac{D_o}{D_i}$.



1. $\frac{KTR}{1-R}$

 $2. \frac{117R}{1 + R - KTR}$

3. $\frac{KTR}{1-R} - KTR$

- $4. \ \frac{-KTR}{1 R KTR}$
- 5. none of the above

Analyzing wallFinder: Poles

Substitute $\mathcal{R} \to \frac{1}{z}$ in the system functional to find the poles.

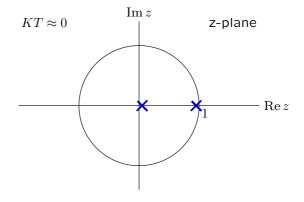
$$\frac{D_o}{D_i} = \frac{-KT\mathcal{R}}{1 - \mathcal{R} - KT\mathcal{R}^2} = \frac{-KT\frac{1}{z}}{1 - \frac{1}{z} - KT\frac{1}{z^2}} = \frac{-KTz}{z^2 - z - KT}$$

The poles are then the roots of the denominator.

$$z = \frac{1}{2} \pm \sqrt{\left(\frac{1}{2}\right)^2 + KT}$$

If KT is small, the poles are at $z \approx -KT$ and $z \approx 1 + KT$.

$$z = \frac{1}{2} \pm \sqrt{\left(\frac{1}{2}\right)^2 + KT} \approx \frac{1}{2} \pm \sqrt{\left(\frac{1}{2} + KT\right)^2} = 1 + KT, -KT$$



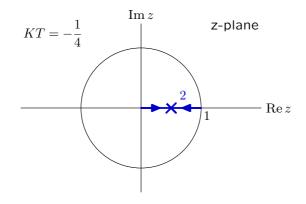
Pole near 0 generates fast response.

Pole near 1 generates slow response.

Slow mode (pole near 1) dominates the response.

As KT becomes more negative, the poles move toward each other and collide at $z=\frac{1}{2}$ when $KT=-\frac{1}{4}.$

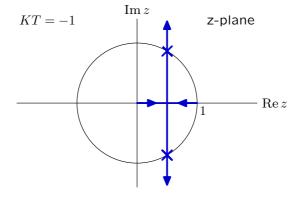
$$z = \frac{1}{2} \pm \sqrt{\left(\frac{1}{2}\right)^2 + KT} = \frac{1}{2} \pm \sqrt{\left(\frac{1}{2}\right)^2 - \frac{1}{4}} = \frac{1}{2}, \frac{1}{2}$$



Persistent responses decay. The system is stable.

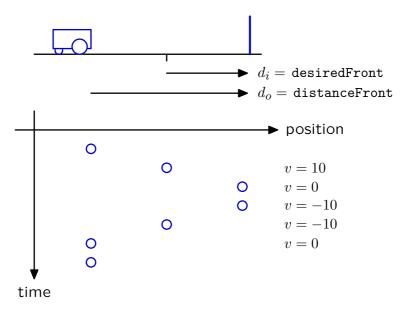
If KT < -1/4, the poles are complex.

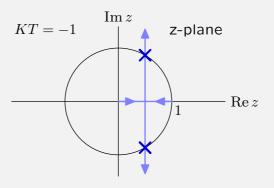
$$z = \frac{1}{2} \pm \sqrt{\left(\frac{1}{2}\right)^2 + KT} = \frac{1}{2} \pm j\sqrt{-KT - \left(\frac{1}{2}\right)^2}$$



Complex poles \rightarrow oscillations.

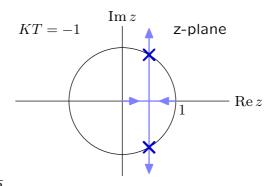
Same oscillation we saw earlier!



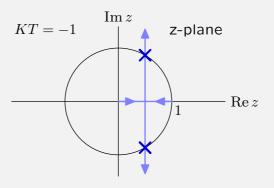


What is the period of the oscillation?

- 1. 1 2. 2 3. 3
- 4. 4 5. 6 0. none of above



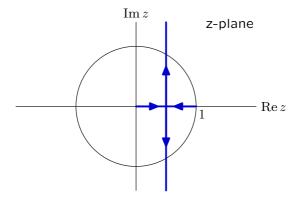
$$\begin{split} p_0 &= \frac{1}{2} \pm j \frac{\sqrt{3}}{2} = e^{\pm j\pi/3} \\ p_0^n &= e^{\pm j\pi n/3} \\ \underbrace{e^{\pm j0\pi/3}}_{1}, \ e^{\pm j\pi/3}, \ e^{\pm j2\pi/3}, \ e^{\pm j3\pi/3}, \ e^{\pm j4\pi/3}, \ e^{\pm j5\pi/3}, \ \underbrace{e^{\pm j6\pi/3}}_{e^{\pm j2\pi} = 1} \end{split}$$



What is the period of the oscillation?

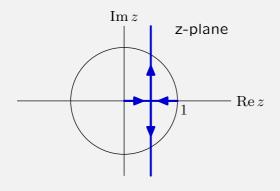
- 1. 1 2. 2 3. 3
- 4. 4 5. 6 0. none of above

The closed loop poles depend on the gain.



If $KT: 0 \to -\infty$: then $z_1, z_2: 0, 1 \to \frac{1}{2}, \frac{1}{2} \to \frac{1}{2} \pm j\infty$

Find KT for fastest response.



closed-loop poles

$$\frac{1}{2} \pm \sqrt{\left(\frac{1}{2}\right)^2 + KT}$$

- 1. 0 2. $-\frac{1}{4}$ 3. $-\frac{1}{2}$

- 4. -1 5. $-\infty$ 0. none of above

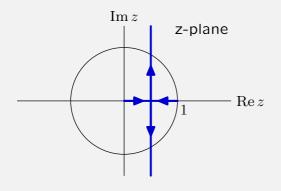
$$z = \frac{1}{2} \pm \sqrt{\left(\frac{1}{2}\right)^2 + KT}$$

The dominant pole always has a magnitude that is $\geq \frac{1}{2}$.

It is smallest when there is a double pole at $z = \frac{1}{2}$.

Therefore, $KT = -\frac{1}{4}$.

Find KT for fastest response.



closed-loop poles

$$\frac{1}{2} \pm \sqrt{\left(\frac{1}{2}\right)^2 + KT}$$

- 1. 0 2. $-\frac{1}{4}$ 3. $-\frac{1}{2}$

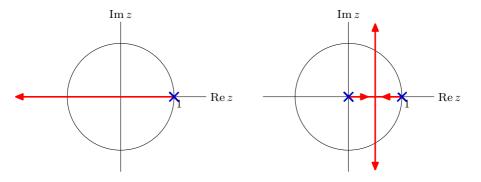
- 4. -1 5. $-\infty$ 0. none of above

Destabilizing Effect of Delay

Adding delay in the feedback loop makes it more difficult to stabilize.

Ideal sensor: $d_s[n] = d_o[n]$

More realistic sensor (with delay): $d_s[n] = d_o[n-1]$



Fastest response without delay: single pole at z = 0.

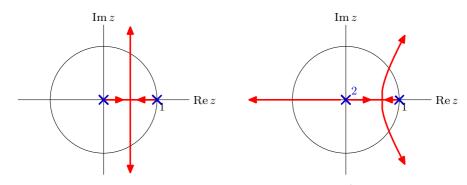
Fastest response with delay: double pole at $z = \frac{1}{2}$. much slower!

Destabilizing Effect of Delay

Adding more delay in the feedback loop is even worse.

More realistic sensor (with delay): $d_s[n] = d_o[n-1]$

Even more delay: $d_s[n] = d_o[n-2]$



Fastest response with delay: double pole at $z = \frac{1}{2}$.

Fastest response with more delay: double pole at z=0.682.

→ even slower

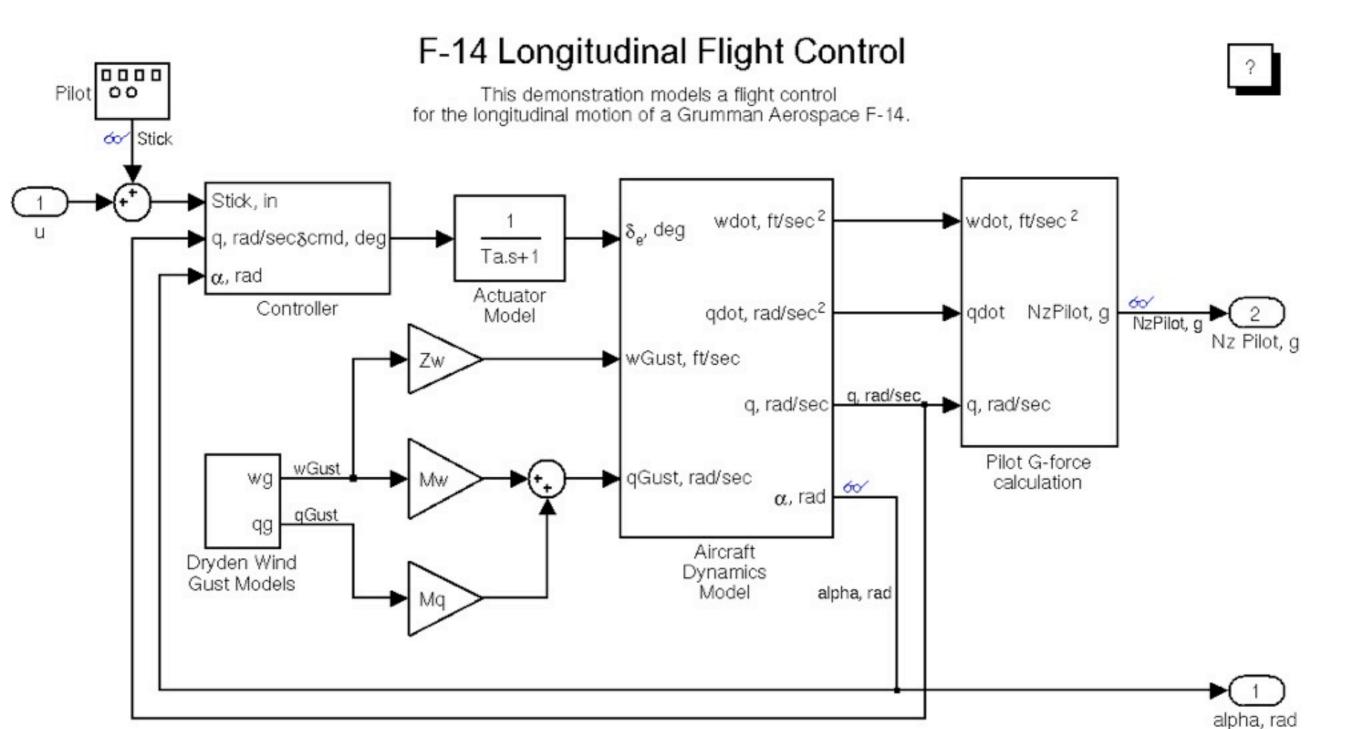
Feedback and Control: Summary

Feedback is an elegant way to design a control system.

Stability of a feedback system is determined by its dominant pole.

Delays tend to decrease the stability of a feedback system.





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