

**Massachusetts Institute of Technology**  
**Department of Electrical Engineering and Computer Science**  
**6.012**  
**Microelectronic Devices and Circuits**  
**Spring 2007**  
**Homework #6**  
**Out: 04/13/2007 Due: 04/20/2007**

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**Problem 1**

An npn transistor with area  $A_E = 2.5 \mu\text{m} \times 2.5 \mu\text{m}$  is biased in the forward active region, with the collector current  $I_C = 50 \mu\text{A}$ . The emitter, base and collector dimensions and doping are:

$N_{dE} = 10^{19} \text{cm}^{-3}$ ,  $W_E = 0.3 \mu\text{m}$ ,  $N_{aB} = 10^{17} \text{cm}^{-3}$ ,  $W_B = 0.25 \mu\text{m}$ , and  $N_{dC} = 10^{16} \text{cm}^{-3}$ ,  $W_C = 1.5 \mu\text{m}$ .

A) Draw a picture of the minority carrier concentration in the emitter and base (identify the minority carrier concentration at the base and emitter edges).

From page 36 of Professor Sodini's book:

$$\begin{aligned} \mu_{nB} &= 775 \text{cm}^2 / \text{Vs} & D_{nB} &= 20.03 \text{cm}^2 / \text{s} \\ \mu_{pE} &= 75 \text{cm}^2 / \text{Vs} & D_{pE} &= 1.939 \text{cm}^2 / \text{s} \end{aligned} \quad \text{Thus}$$

$$\beta_F = \frac{N_{dE} D_{nB} W_E}{N_{aB} D_{pE} W_B} = 1240 \quad \text{And} \quad I_B = \frac{I_C}{\beta_F} = 40.323 \text{nA} \quad \text{Also} \quad I_B = q A_E \frac{D_{pE}}{W_E} \frac{n_i^2}{N_{dE}} e^{V_{BE}/V_{th}}$$

Therefore  $V_{BE} = 0.7616\text{V}$

$$\text{Thus} \quad p_{nE}(0^-) = 6.23 \cdot 10^{13} \text{cm}^{-3} \quad \text{and} \quad n_{pB}(0^+) = 6.23 \cdot 10^{15} \text{cm}^{-3}$$

$$p_{nE}(-W_E) = 10 \text{cm}^{-3} \quad \text{and} \quad n_{pB}(W_B) = 0 \text{cm}^{-3}$$

B) Find the base-emitter bias  $V_{BE}$ .

$$V_{BE} = 0.7616\text{V}$$

C) Find the base current  $I_B$ .

$$I_B = \frac{I_C}{\beta_F} = 40.323 \text{nA}$$

D) For the npn BJT biased as above, given that  $V_{An} = 25$  V, find the transconductance  $g_m$ , the input resistance  $r_\pi$ , and the output resistance  $r_o$ .

$$g_m = \frac{I_C}{V_{th}} = 1.93 \text{ mS}; \quad r_\pi = \frac{\beta_F}{g_m} = 641 \text{ k}\Omega; \quad r_o = \frac{V_A}{I_C} = 500 \text{ k}\Omega$$

E) For the npn BJT biased as above, given that the emitter-base depletion region width is  $x_{BE} = 0.05$   $\mu\text{m}$ , what is the minority electron charge storage in the base  $Q_{NB}(V_{BE})$  at this operating point?

$$|Q_{nB}| = qA \int_{Base} n(x) dx = 1/2 qA n_{pB}(0^-)(W_B - x_{BE}) = 6.24 \cdot 10^{-16} \text{ C}$$

F) What is  $C_\pi$  at this operating point?

$$C_\pi = A \frac{\epsilon_{Si}}{x_d} + g_m \frac{W_B^2}{2D_{nB}} = 12.9 \text{ fF} + 19.3 \text{ fF} = 32.2 \text{ fF}$$

## Problem 2

In this problem we will consider an important development of the late 1980s, the SiGe alloy base BJT. This Hetero Bipolar Transistor (HBT) is usually fabricated as an npn BJT with a base made of SiGe to increase the intrinsic carrier concentration in the base and with Si collector and emitter. The emitter, base, and collector dimensions are:

$N_{dE} = 5 \times 10^{19} \text{ cm}^{-3}$ ,  $W_E = 0.25 \text{ }\mu\text{m}$ ,  $N_{aB} = 10^{18} \text{ cm}^{-3}$ ,  $W_B = 0.25 \text{ }\mu\text{m}$ , and  $N_{dC} = 10^{17} \text{ cm}^{-3}$ ,  $W_C = 1.5 \text{ }\mu\text{m}$ . Note that at room temperature the intrinsic carrier concentration of SiGe is  $n_{iSiGe} = 5 \times 10^{10} \text{ cm}^{-3}$ .

For this problem assume that the concentration of Ge is low thus the mobility, dielectric constant of the SiGe base film remain unchanged from that of Si.

A) Find  $\alpha_F$  and the forward active current gain  $\beta_F$  for the npn SiGe HBT (SiGe Base Transistor) and npn BJT (Si Base) at room temperature.

$$\begin{aligned} \mu_{nB} &= 325 \text{ cm}^2 / \text{Vs} & D_{nB} &= 8.4 \text{ cm}^2 / \text{s} \\ \mu_{pE} &= 50 \text{ cm}^2 / \text{Vs} & D_{pE} &= 1.29 \text{ cm}^2 / \text{s} \end{aligned} \quad \text{Thus}$$

$$\beta_{FSiGe} = \frac{N_{dE} D_{nB} n_{iSiGe}^2 W_E}{N_{aB} D_{pE} n_{iSi}^2 W_B} = 8125 \quad \text{And} \quad \alpha_{FSiGe} = \frac{\beta_{FSiGe}}{1 + \beta_{FSiGe}} = 0.99988$$

$$\beta_{FSi} = \frac{N_{dE} D_{nB} W_E}{N_{aB} D_{pE} W_B} = 325 \quad \text{And} \quad \alpha_{FSi} = \frac{\beta_{FSi}}{1 + \beta_{FSi}} = 0.9969$$

B) What is the ratio between forward active current gains for the npn SiGe HBT and the corresponding npn BJT?

$$\frac{\beta_{FSiGe}}{\beta_{FSi}} = \frac{n_{iSiGe}^2}{n_{iSi}^2} = 25$$

C) Determine the base doping of the npn BJT that will yield the same value of  $\beta_F$  as in the npn SiGe HBT. (Note that the mobility depend on the doping, thus changing the doping would change the mobility. You should converge to the solution through few iterations)

For  $N_{aB} = 9.2 \cdot 10^{16} \text{ cm}^{-3}$  the mobility is  $\mu_{nB} = 750 \text{ cm}^2 / \text{Vs}$

$$\beta_{FSi} = \beta_{FSiGe} = \frac{N_{dE} D_{nB} W_E}{N_{aB} D_{pE} W_B} = 8150$$

### Problem 3

A p<sup>+</sup>np bipolar transistor has the geometry and doping profile described below. For all the following questions the BJT is operating in a common-emitter mode in the forward active region.

BJT Data:

$D_{pB} = 5 \text{ cm}^2/\text{s}$ ;  $D_{nE} = 10 \text{ cm}^2/\text{s}$ ;  $W_E = 500 \text{ nm}$ ;  $A = 25 \text{ } \mu\text{m}^2$ ;  $N_{aE} = 10^{19} \text{ cm}^{-3}$ ;  $N_{dB} = 10^{17} \text{ cm}^{-3}$ ;  $N_{aC} = 10^{16} \text{ cm}^{-3}$ .

A) We want the current gain  $\beta_F$  to be 100, what should be the value for the base thickness  $W_B$ ? Neglect depletion region widths.

$$\beta_F = \frac{N_{aE} D_{pB} W_E}{N_{dB} D_{nE} W_B} \quad \text{Therefore} \quad W_B = \frac{N_{aE} D_{pB} W_E}{N_{dB} D_{nE} \beta_F} = 250 \text{ nm}$$

B) What is the saturation current  $I_s$  for the emitter-base p-n diode?

$$I_E = qA_E \frac{D_{pB}}{W_B} \frac{n_i^2}{N_{aB}} e^{V_{EB}/V_{th}} = I_s e^{V_{EB}/V_{th}} \quad \text{Therefore} \quad I_s = qA_E \frac{D_{pB}}{W_B} \frac{n_i^2}{N_{dB}} = 8 \cdot 10^{-18} \text{ A}$$

C) What should be the EB voltage to obtain a collector current of  $I_C = 100 \text{ } \mu\text{A}$ ?

$$I_C = I_s e^{V_{EB}/V_{th}} \quad \text{Therefore} \quad V_{EB} = V_{th} \cdot \ln\left(\frac{I_C}{I_s}\right) = -0.78 \text{ V}$$

D) What is the transconductance at  $I_C = 100 \text{ } \mu\text{A}$ ?

$$g_m = \frac{I_C}{V_{th}} = 3.87 \text{ mS}$$

E) What is the capacitance  $C_\pi$  at  $I_C = 100 \text{ } \mu\text{A}$ ?

$$C_\pi = \sqrt{2} C_{j0} A_E + g_m \frac{W_B^2}{2D_{pB}} = 32.7 \text{ fF} + 242 \text{ fF} = 275 \text{ fF}$$

$$C_{j0} = 92.5 \text{ nF} / \text{cm}^2$$

F) What is the input resistance at  $I_C = 100 \text{ } \mu\text{A}$ ?

$$R_{in} = R_\pi = \frac{\beta_F}{g_m} = 25.8 \text{ k}\Omega$$

G) What is the output resistance at  $I_C = 100 \text{ } \mu\text{A}$  given an Early Voltage  $V_A = 30 \text{ V}$ ?

$$R_O = \frac{V_A}{I_C} = \frac{30V}{100\mu A} = 300k\Omega$$

H) In forward active regime find the frequency limit set by the base diffusion transit time?

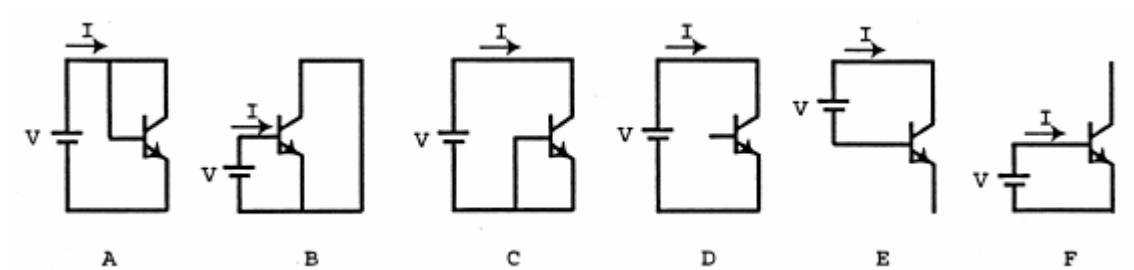
The BJT needs to be in the forward active region.

$$V_{BE} < 0 \text{ and } V_{BC} > 0$$

$$f_T = \frac{1}{\tau_F} = \frac{1}{\frac{W_B^2}{2D_{pB}}} = 16GHz$$

#### Problem 4

The figure below shows six possible ways of connecting an npn bipolar transistor that may yield a diode-like behavior. Using the Ideal Non-Linear Hybrid- $\pi$  Model, write the I-V characteristics of the two-terminal device in each configuration. Express your results as a function of  $I_S$ ,  $\beta_F$ , and  $\beta_R$ .



Configuration A

$$V_{BE} = V \text{ and } V_{BC} = 0$$

$$I = \frac{I_S}{\beta} \left( e^{V_{BE}/V_{th}} - 1 \right) + I_S \left( e^{V_{BE}/V_{th}} - 1 \right) \text{ Therefore } I = I_S \frac{1 + \beta_F}{\beta_F} \left( e^{V/V_{th}} - 1 \right)$$

$$\text{For } \beta_F \gg 1 \quad I \cong I_S \left( e^{V_{BE}/V_{th}} - 1 \right)$$

Configuration B

$$V_{BE} = V \text{ and } V_{BC} = V \text{ (because there is a short circuit between E and C)}$$

$$I = \frac{I_S}{\beta_F} \left( e^{V_{BE}/V_{th}} - 1 \right) + \frac{I_S}{\beta_R} \left( e^{V_{BE}/V_{th}} - 1 \right) \quad \text{Therefore } I = \frac{I_S}{\beta_F} \left( e^{V/V_{th}} - 1 \right) + \frac{I_S}{\beta_R} \left( e^{V/V_{th}} - 1 \right)$$

For  $\beta_F \gg \beta_R$

$$I \cong \frac{I_S}{\beta_R} \left( e^{V_{BE}/V_{th}} - 1 \right)$$

Configuration C

$V_{BE} = 0$  and  $V_{BC} = -V$

$$I = -\frac{I_S}{\beta_R} \left( e^{-V/V_{th}} - 1 \right) + I_S \left( 1 - e^{-V/V_{th}} \right) \quad \text{Therefore } I = -I_S \frac{\beta_R + 1}{\beta_R} \left( e^{-V/V_{th}} - 1 \right)$$

Configuration D

$V = V_{BC} - V_{BE}$

$$\frac{I_S}{\beta_R} \left( e^{V_{BC}/V_{th}} - 1 \right) + \frac{I_S}{\beta_F} \left( e^{V_{BE}/V_{th}} - 1 \right) \quad \text{Therefore } \frac{I_S}{\beta_R} \left( e^{V_{BE} - V/V_{th}} - 1 \right) + \frac{I_S}{\beta_F} \left( e^{V_{BE}/V_{th}} - 1 \right)$$

$$\text{Therefore } e^{V_{BE}/V_{th}} = \frac{\frac{1}{\beta_R} - \frac{1}{\beta_F}}{e^{-V/V_{th}} - \frac{1}{\beta_F}} \quad \text{Therefore } I = \left( \frac{\frac{1}{\beta_R} - \frac{1}{\beta_F}}{e^{-V/V_{th}} - \frac{1}{\beta_F}} \right) \left( 1 - e^{-V/V_{th}} + \frac{1}{\beta_F} \right) - \frac{1}{\beta_F}$$

Configuration E

$V = -V_{BC}$  and  $V_{BE} = \phi_{BE}$

No net current flow through the base/emitter junction since the emitter is open. The BJT is working as a diode.

$$I = \frac{I_S}{\beta_R} \left( e^{-V/V_{th}} - 1 \right)$$

## Configuration E

$$V = V_{BE} \text{ and } V_{BC} = \phi_{BC}$$

No net current flow through the base/collector junction since the emitter is open. The BJT is working as a diode.

$$I = \frac{I_S}{\beta_F} \left( e^{V/V_{th}} - 1 \right)$$