Publishers) Ltd.
W.C.2
AFRICA) Ltd.
GROVE
AUSTRALIA) Ltd.
L STREET
KE STREET
STREET
CANADA) Ltd.
RTH AVENUE, 6
NEW ZEALAND) Ltd.
LLANCE STREET
TREET

35 Wisconsin Avenue, 14

EXPERIMENTAL CRYOPHYSICS

Sec 7.9

Taconis Oscillations

Edited by

F. E. HOARE

Reader in Physics, University of Leeds

L. C. JACKSON

Professor of Physics, Royal Military College, Kingston, Ontario, Canada

N. KURTI

Reader in Physics, University of Oxford; Senior Research Fellow, Brasenose College, Oxford

LONDON
BUTTERWORTHS
1961

LIQUEFIED GASES

ntage of simplicity and the disvhich is not robust. Unicellular ices. In one, the density of this d to be 0.04 g/cm³. Hence, it id liquid helium, as well as, of or which cork also works well. ither by direct viewing through palsa wood rod to the float and sen (Babiskin, 1950). Another using a pivoted float whose cting the surface can be made Rasor, 1954).

ndication at one level only has yen liquefier at the Clarendon essentially of two tubes, one chamber and the other at the to a type of hydrodynamical on the liquid level reaches the

ic constants of the liquid and neasurement for research pureneral liquid level indication as for sensing element a cylinion of the height of the liquid; ich both indicates and records 1.0 per cent. This instrument air pressure to a pneumatically predetermined point.

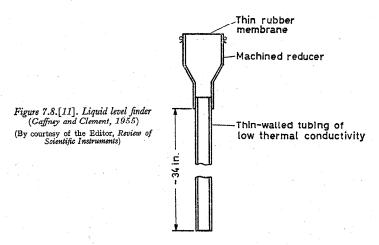
sensing element, based on the olved in hot wire gauges such rement and devices used for nents, a fine platinum wire is t (Wexler and Corak, 1951). stance (provided the resistivity the heat transfer conditions. en a solid body and a boiling and the vapour in equilibrium e voltage drop across the wire the liquid. For fine platinum t a five-fold voltage difference : in the liquid or the vapour. ients, with which levels can be nclude the accurate maintentwo points over a period of ents at the end of 'dip' sticks aid nitrogen and helium.

on resistors have been used.

r and robustness of response

7.8. LIQUID LEVEL INDICATORS

Perhaps the simplest among widely used level indicators is one based on the observation that when the cold end of a tube containing an oscillating gas column (see the next section) passes from the vapour into the liquid, the frequency of oscillation decreases by about 30 per cent, and the intensity of the oscillation decreases by about 60 per cent (Gaffney and Clement, 1955). Figure 7.8.[11] indicates the construction of the device.



Inconel (or German silver) tubing, $\frac{3}{32}$ in. O.D., 0.008 in. wall, has been found to work well. If a tube of much smaller diameter is used, air may freeze inside the tube and stop the oscillations. If tubes of much larger diameter are used, the oscillations may become so intense that the liquid level is disturbed, the level thus becoming uncertain. Small sections cut from surgical gloves make rugged and sufficiently sensitive membranes; they should be about 1 in. in diameter. The liquid level, either hydrogen or helium, is found by holding the thumb or forefinger over the rubber membrane and noting the point at which an abrupt frequency-intensity change occurs. With care, helium levels can be measured to within 1 mm by this technique.

In a consideration of methods of liquid level determination, the following very simple procedures should not be overlooked. The contents of storage containers of liquid oxygen, air and nitrogen, which are appreciably denser than liquid hydrogen and helium, are frequently followed by simply weighing the container and its contents. A technique applicable to all liquids is to use slit-silvered Dewar vessels which permit direct viewing of the liquid level.

7.9. THERMAL OSCILLATIONS

It has long been recognized that the gas in a tube, the closed end of which is hot and the open end of which is cool, can go into spontaneous oscillation. In fact, in Lord Rayleigh's classic work, *The Theory of Sound*, reference

(Clement and Gaffney, 1955) t range of tube diameters. When observed that at first the inten decreases as the volume of the

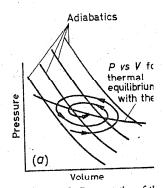


Figure 7.9.[12]. Representation of the gradient too small to sustain thermal o.

noting that the initial increase gas at the hot end. As the volu the characteristics of an open tion in the tube to one unfavo foregoing makes plausible the of a tube in minimizing the s 1953; Clement and Gaffney, 19

7.10. FABRICATION TE

While fabrication techniques depending on their application illustrated by outlining the p tainer like that shown in Fig. soldering a low conductivity n upper copper spinning of what vary in thickness from about 1 for containers of 100-l. capacit and under sections of the joir Next the inner sphere is compl to the upper one. These are ar Soldering is accomplished by neat filleted solder band arous band around the joint. The free of spinning soap and dir oxide. This surface, as well buffed on a wheel, and the

7. STORAGE AND TRANSFER OF LIQUEFIED GASES

is made to the observation of this phenomenon by glass blowers and a physical picture is given for the mechanism of these oscillations. In low temperature apparatus, conditions for such oscillations are frequently present. While they always add heat to the low temperature portions of the apparatus and are therefore undesirable, there is at least one reported instance when such oscillations were used to good effect, namely, to stir liquid and vapour in experiments in which the 3He/4He equilibrium ratios in the two phases were being determined (Taconis, Beenakker, Nier and Aldrich, 1949).

Keesom (1942) has commented on the Leiden experience in this connection; the heat transport effect for liquid helium was noted as was the fact that this phenomenon interfered with measurements of the ratio of specific heats at liquid hydrogen temperatures. It has been observed that spontaneous oscillations can increase the evaporation rate of storage containers by a factor of one thousand (Wexler, 1951). Squire (1953) has commented on some of the properties of these oscillations. More recent work (Clement and Gaffney, 1955), prompted by difficulties in using a particular transfer tube, reported additional descriptive observations; this work has led

to the simple level finder described above.

While both a qualitative description of the mechanism of thermal oscillations in low temperature apparatus has been given and a quantitive treatment attempted (Kramers, 1949), the physical picture remains essentially that given by Rayleigh. Consider a tube closed at the room temperature end, open at the low temperature end and terminating in either the vapour or liquid phase. It may be assumed from the geometry that the tube is a quarter-wave resonant tube with a pressure node at the cold, open end and a pressure antinode at the hot, closed end. During the compression phase, the motion of gas is towards the closed, hot end of the tube. The gas undergoing compression and moving towards the hot end heats because of the work being done on it. If the temperature gradient is sufficiently steep along the wall of the tube, the heated gas will find itself in contact with a section of wall at a still higher temperature, so that heat will flow into the gas, thereby increasing the pressure and energy content further. During the expansion phase, the reverse process occurs, the gas rejecting heat to the wall at low temperature.

This process may be visualized (Garfunkel, 1957) by referring to Figure 7.9.[12], wherein are plotted pressure-volume adiabatics for an element of mass of the gas undergoing oscillation. Two cases are considered. In Figure 7.9.[12]b the temperature gradient is steep enough for the heat exchange of the gas with the wall to reinforce both the expansions and contractions of the gas. The P-V loop will expand until dissipation of energy external to the gas, e.g. by sound radiation, is just equal to the area of the loop. If the temperature gradient is not steep enough, the P-V loop tends to collapse as the result of the heat exchange between the gas and the wall as shown in Figure 7.9.[12]a. From the figures it is clear that in addition to an appropriate temperature gradient, the thermal contact between the gas and the wall must be neither too good, in which case a single line would be traced out on the P-V diagram, nor too poor, in which case insufficient heat will pass between the gas and the tube. This explains the observation

F LIQUEFIED GASES

nenon by glass blowers and a m of these oscillations. In low oscillations are frequently pretween temperature portions of the tere is at least one reported into deffect, namely, to stir liquid ³He/⁴He equilibrium ratios in Taconis, Beenakker, Nier and

Leiden experience in this conl helium was noted as was the measurements of the ratio of res. It has been observed that apporation rate of storage con-1951). Squire (1953) has comoscillations. More recent work difficulties in using a particular observations; this work has led

ne mechanism of thermal oscilbeen given and a quantitive physical picture remains essenbe closed at the room temperaand terminating in either the d from the geometry that the a pressure node at the cold, t, closed end. During the comthe closed, hot end of the tube. ng towards the hot end heats temperature gradient is suffie heated gas will find itself in temperature, so that heat will ure and energy content further. ocess occurs, the gas rejecting

el, 1957) by referring to Figure le adiabatics for an element of cases are considered. In Figure enough for the heat exchange e expansions and contractions dissipation of energy external lual to the area of the loop. If h, the P-V loop tends to colween the gas and the wall as it is clear that in addition to ermal contact between the gas which case a single line would poor, in which case insufficient This explains the observation

7.9. THERMAL OSCILLATIONS

(Clement and Gaffney, 1955) that thermal oscillations are restricted to a range of tube diameters. When a cavity is added at the closed end it is observed that at first the intensity of the oscillations increases and then decreases as the volume of the cavity increases. This can be explained by

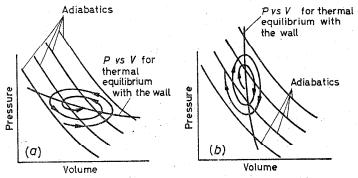


Figure 7.9.[12]. Representation of thermal oscillations in the P-V plane: (a) temperature gradient too small to sustain thermal oscillations; (b) temperature gradient sufficient to sustain thermal oscillations

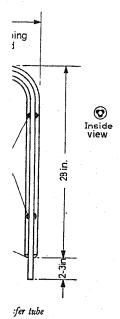
noting that the initial increase in volume permits larger displacements of gas at the hot end. As the volume increases, however, this end approaches the characteristics of an open end, thereby changing the mode of vibration in the tube to one unfavourable for sustained oscillations. Again the foregoing makes plausible the efficacy of closing the low temperature end of a tube in minimizing the strength of the thermal oscillations (Squire, 1953; Clement and Gaffney, 1955).

7.10. FABRICATION TECHNIQUES FOR METAL VESSELS

While fabrication techniques for metal Dewar vessels vary considerably, depending on their application, many of the techniques used may be illustrated by outlining the procedure used in the fabrication of a container like that shown in Figure 7.4.[6]b. The first step consists of soft soldering a low conductivity neck tube, of stainless steel or inconel, to the upper copper spinning of what will become the inner sphere. The spinnings vary in thickness from about $\frac{1}{32}$ in. for containers of 5-10-1. capacity to $\frac{1}{16}$ in. for containers of 100-l. capacity. Solder fillets are run in on both the upper and under sections of the joint between the spinning and the neck tube. Next the inner sphere is completed by soldering the lower half of the sphere to the upper one. These are arranged to fit tightly in the absence of solder. Soldering is accomplished by pre-tinning the joining surfaces, running a neat filleted solder band around the joint, and then puddling a soft solder band around the joint. The outer surface of the inner sphere is washed free of spinning soap and dipped in a weak acid solution to remove the oxide. This surface, as well as the outer surface of the neck tube, is buffed on a wheel, and the surfaces are then hand polished with a fine

LIQUEFIED GASES

sfer tubes are fabricated. Two .D. and the other 12 mm O.D., ed on to the inner tube in the fitted with a 5-mm constricted



off at one end. The inner tube aled together with a ring seal. 1g. The bending of both tubes with a soft flame (gas and air ring the heat to penetrate into be to permit bending. A relatine full inside diameter of the both bends is the same. The

1 Fairbank, 1947) that helium ugh Pyrex than through soft nd transfer tubes going 'soft' ized by removing the helium One simple way of accomplishm space after the run is compermitted to warm up. When

7.11. LOW TEMPERATURE APPLICATIONS OF GLASS WORKING TECHNIQUES a Dewar vessel or transfer tube goes soft, the vacuum space is flushed with dry nitrogen and the space is repumped.

7.11.6. GLASS-TO-METAL SEALS

Glass-to-metal seals are very useful in low temperature research. They simplify the assembly of apparatus, eliminate the necessity for having, in the warm regions of the vacuum system, fabric-covered wires which can desorb gas, and make it possible to cool lead wires directly in the refrigerant bath. Both tube and wire seals are required. A number of successful metal and glass combinations have been used (Corak and Wexler, 1953), including copper Housekeeper seals, zirconium-to-glass, and tungsten-to-glass. About Kovar-to-glass seals there is disagreement as to their usefulness, some investigators reporting excellent results (Lane, 1947) and others reporting unreliable results (Corak and Wexler, 1953). It is possible that the difference in experience reflects differences in performance of seals of this type depending upon the composition of the Kovar and of the sealing glass.

BIBLIOGRAPHY

BARR, W. E. and Anhorn, V. J., 1949, Scientific and Industrial Glass Blowing and Laboratory Techniques, Instruments Publishing Co., Pittsburgh. This publication gives a comprehensive survey of glass-working techniques. Although it contains little concerned explicitly with the construction of apparatus for low temperature work, the techniques for glass manipulation are fully described and make it a very useful book.

Meissner, W., 1926, Handbuch der Physik, Vol. XI., Springer, Berlin. A short review of several devices for use at low temperatures including descriptions of simple valves for liquefied gases, a level indicator depending for its action upon the hydrostatic pressure difference over a free surface and at the bottom of

a liquid and the rubber balloon technique for transfer.

Report of the Oxygen Research Committee, 1923, H.M.S.O., London. This contains much information which is still useful. The emphasis is upon the storage and transport of liquid oxygen, but constructional details for metal Dewar flasks are of use in other connections.

ROBERTSON, A. J. B., FABIAN, D. J., CROCKER, A. J. and DEWING, J., 1957, Laboratory Glass-working for Scientists, Butterworths, London. The intention of the authors of this book is to describe glass-working techniques within the capabilities of amateurs. The methods given differ in some cases from those which would be employed by professionals.

Van Lammeren, J. A., 1941, Technik der tiefen Temperaturen, Springer, Berlin. A wide survey of low temperature investigations and procedures, mainly those of the Kamerlingh Onnes Laboratory, Leiden. Few details of constructional

methods are given.

Wheeler, E. L., 1958, Scientific Glasshlowing, Interscience Publishers, New York, London. A very straightforward account of glass working. Gives a list of modern commercially obtainable glasses and their characteristics. Equipment is dealt with in some detail and a list of American suppliers is given. Chapters on elementary metal working and electrical heaters are included.

163

REFERENCES

Babiskin, J., 1950, Rev. sci. Instrum., 21, 941

BLACKMAN, M., EGERTON, A. and TRUTER, E. V., 1947, Proc. Roy Soc., A, 194, 147

Biondi, M. A., 1956, Phys. Rev., 102, 964

Birmingham, B. W., Brown, E. H., Class, C. R. and Schmidt, A. F., 1957, J. Res. nat. Bur. Stand., 58, 243

CLEMENT, J. R. and GAFFNEY, J., 1955, Proceedings of the 1954 Cryogenic Engineering

Conference, Rep. nat. Bur. Stand., 3517, p. 227

CORAK, W. S. and WEXLER, A., 1953, Rev. sci. Instrum., 24, 994

CROFT, A. J. and JONES, G. O., 1950, Brit. J. appl. Phys., 1, 137

Dash, J. G. and Boorse, A. H., 1951, Phys. Rev., 82, 851

DESIRANT, M. C. and HORVARTH, W. J., 1948, Rev. sci. Instrum., 19, 718

Estermann, I. and Zimmerman, J. E., 1952, J. appl. Phys., 23, 578

FELDMEIER, J. R. and SERIN, B., 1948, Rev. sci. Instrum., 19, 916

GAFFNEY, J. and CLEMENT, J. R., 1955, Rev. sci. Instrum., 26, 620

GARFUNKEL, M. P., 1957, Westinghouse Res. Lab. Res. Memo., 6-94466-5-M3

GIAUQUE, W. F., 1947, Rev. sci. Instrum., 18, 852

GRILLY, E. R., 1953, Rev. sci. Instrum., 24, 1

JOHNSTON, H. L., GONZALEZ, O. D. and WHITE, D., 1951, Rev. sci. Instrum., 22, 702

JONES, G. O. and LARSEN, A. H., 1948, 7. sci. Instrum., 25, 375

Jones, G. O. and Swenson, C. A., 1948, J. sci. Instrum., 25, 72

KAMERLINGH ONNES, H. and CROMMELIN, C. A., 1913, Versl. gewone Vergad. Akad. Amst., 21, 214

Keesom, W. H., 1942, Helium, Elsevier, Amsterdam, pp. 97, 174

Kitts, W. T. and Harler, F. L., 1954, Rev. sci. Instrum., 25, 926

Kramers, H. A., 1949, Physica, 's Grav, 15, 971

LANE, C. T., 1949, Rev. sci. Instrum., 20, 140

Lane, C. T. and Fairbank, H. A., 1947, Rev. sci. Instrum., 18, 552

LARSEN, A. H., SIMON, F. E. and SWENSON, C. A., 1948, Rev. sci. Instrum., 19, 266

Mendoza, E., 1954, Vacuum, 4, 476 (Published 1957)

RAMANATHAN, K. G., 1952, Proc. phys. Soc. Lond., A, 65, 532

RASOR, N. S., 1954, Rev. sci. Instrum., 25, 311

RAYLEIGH, LORD, 1896, The Theory of Sound, Vol. 2, Macmillan, New York, p. 230

Scott, R. B., 1957, J. Res. nat. Bur. Stand., 58, 317

Scott, R. B. and Cook, J. W., 1948, Rev. sci. Instrum., 19, 889

Scott, R. B., Ferguson, W. J. and Brickwedde, F. G., 1944, J. Res. nat. Bur. Stand., 33, 1

SQUIRE, C. F., 1953, Low Temperature Physics, McGraw-Hill, New York, p. 23

SYDORIAK, S. G. and SOMMERS, H. S. (Jr.), 1951, Rev. sci. Instrum., 22, 915

TACONIS, K. W., BEENAKKER, J. J. M., NIER, A. O. C. and Aldrich, L. T., 1949, Physica, 's Grav., 15, 733

WEXLER, A., 1951, J. appl. Phys., 22, 1463

WEXLER, A., 1954, Rev. sci. Instrum., 25, 442

WEXLER, A. and CORAK, W. S., 1950, Rev. sci. Instrum., 21, 583

WEXLER, A. and CORAK, W. S., 1951, Rev. sci. Instrum., 22, 941

WEXLER, A. and JACKET, H. S., 1951, Rev. sci. Instrum., 22, 282

WILLIAMS, W. E. (Jr.) and MAXWELL, E., 1954, Rev. sci. Instrum., 25, 111

Woolley, H. W., Scott, R. B. and Brickwedde, F. G., 1948, J. Res. nat. Bur. Stand., 41, 379

8. MAG

8.1.

This chapter is divided into the deals with the thermodynamic for producing temperatures be magnetic substances. Studies interest in solid state physics specimens of this kind. The sesome of the techniques for cook contact with the paramagnet smallness—on an absolute suspecimen of paramagnetic, a contact between solids. The special techniques, such as the

Although this chapter is coing temperatures below 1° K, in conjunction with ³He refrig

8.2. THE THERMODYI The most useful diagram for a zation processes is the family magnetic fields, Figure 8.2.[1]. tributions: that from the mag Usually they can be though

Figure 8.2.[1]. Entropy-tem ture diagram for a paramay salt in zero field and in 10 (schematic). A demagnetiz from 10 kG and T₁ is repres by BD

entropy at 1° K is small com importance for demagnetizat is short, that is, equality of sp after a change in either. It is the magnetic field during mapared with this relaxation t