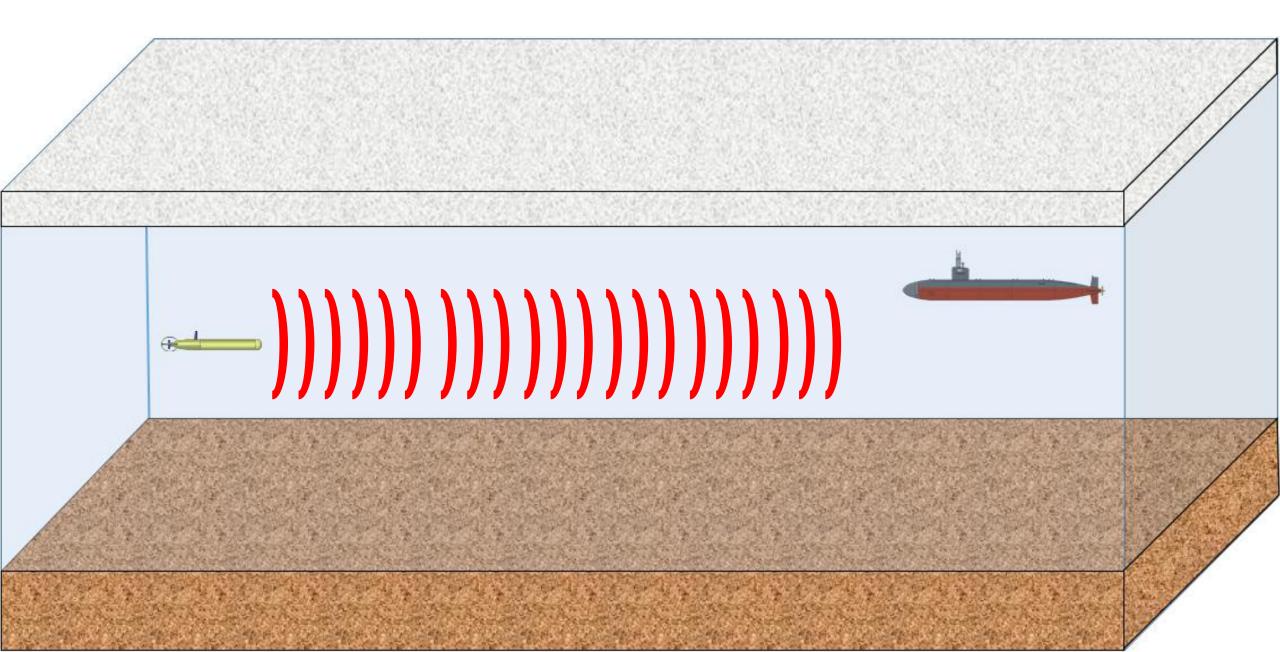




Wael Hajj Ali

# Why ocean acoustics?

- Underwater sound propagation
- Commercial interests:
  - Submerged cables
  - Resources
- Marine Science



## Governing equations - I:

• For single frequency continuous wave, the inhomogeneous wave pressure equation:

$$\rho \nabla \cdot \left(\frac{1}{\rho} \nabla P\right) + k^2 P = 0$$

• Propagation from a point source – use cylindrical coordinates:

$$\left[\frac{\partial^2}{\partial r^2} + \frac{1}{r}\frac{\partial}{\partial r} + \frac{1}{r^2}\rho\frac{\partial}{\partial\theta}\left(\frac{1}{\rho}\frac{\partial}{\partial\theta}\right) + \rho\frac{\partial}{\partial z}\left(\frac{1}{\rho}\frac{\partial}{\partial z}\right) + k^2\left(r,\theta,z\right)\right]P = 0$$

## Governing equations - II:

• Postulate solution to be of the form:

$$P(r,\theta,z) = u(r,\theta,z) H_0^{(1)}(k_0 r)$$

• Parabolic equation for the outgoing wave:

$$\frac{\partial \psi}{\partial r} = \left(-ik_0 + ik_0\sqrt{1 + X^+ + Y^+}\right)\psi$$

Where:

$$X^{+} = n^{2} \left( r, \theta, z \right) - 1 + \frac{1}{k_{0}^{2}} \rho \frac{\partial}{\partial z} \left( \frac{1}{\rho} \frac{\partial}{\partial z} \right)$$
$$Y^{+} = \frac{1}{k_{0}^{2} r^{2}} \rho \frac{\partial}{\partial \theta} \left( \frac{1}{\rho} \frac{\partial}{\partial \theta} \right)$$

## Governing equations - III:

• For narrow angle propagation:

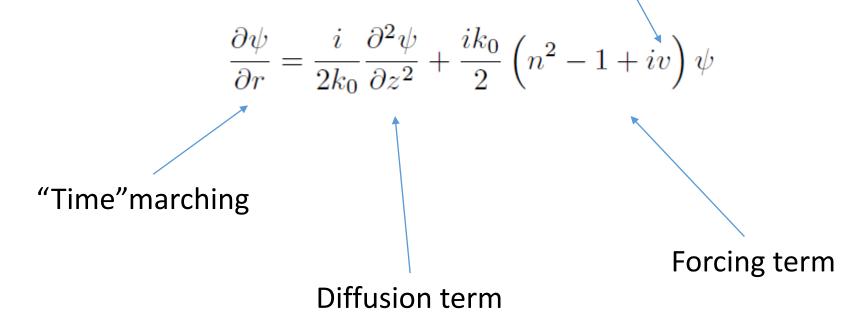
$$\sqrt{1 + X^+ + Y^+} \approx 1 + \frac{1}{2}X^+ + \frac{1}{2}Y^+$$

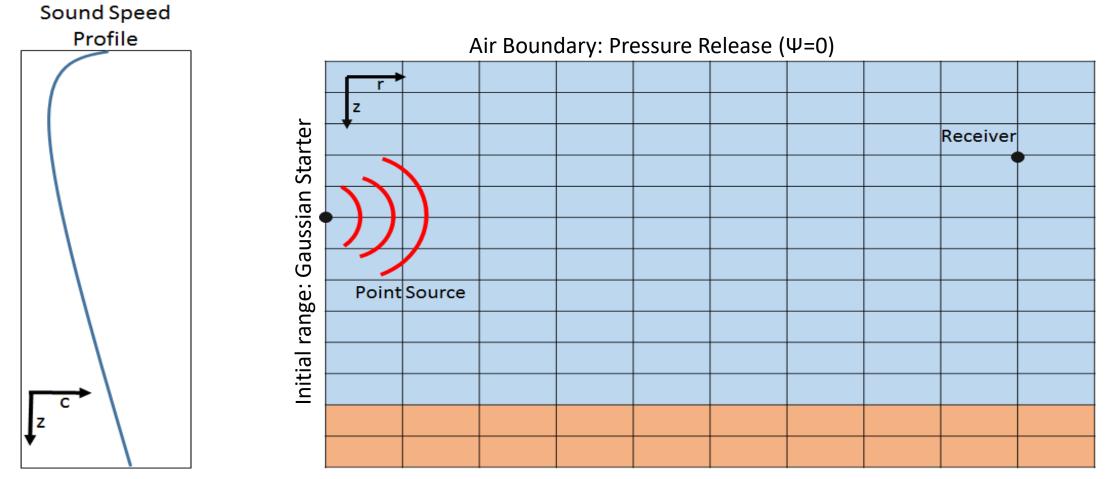
• Variable-Density Parabolic equation (Tappert, 1977):

$$\frac{\partial \psi}{\partial r} = \frac{\rho i}{2k_0} \left( \frac{\partial}{\partial z} \left( \frac{1}{\rho} \frac{\partial \psi}{\partial z} \right) + \frac{1}{r^2} \frac{\partial}{\partial \theta} \left( \frac{1}{\rho} \frac{\partial \psi}{\partial \theta} \right) \right) + \frac{ik_0}{2} \left( n^2 - 1 \right) \psi$$

F. D. Tappert. The parabolic approximation method. In J. B. Keller and J. S. Papadakis, editors, Wave Propagation and Underwater Acoustics, volume 70 of Lecture Notes in Physics, Berlin Springer Verlag, page 224, 1977

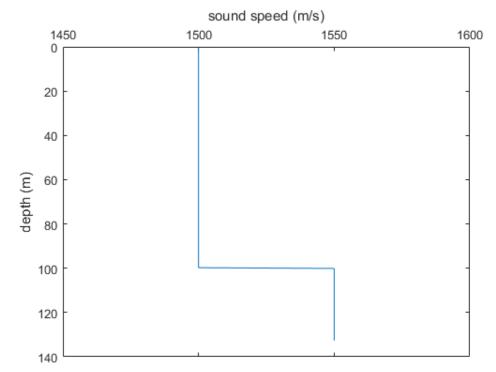
• Governing equation reduces to (with attenuation):





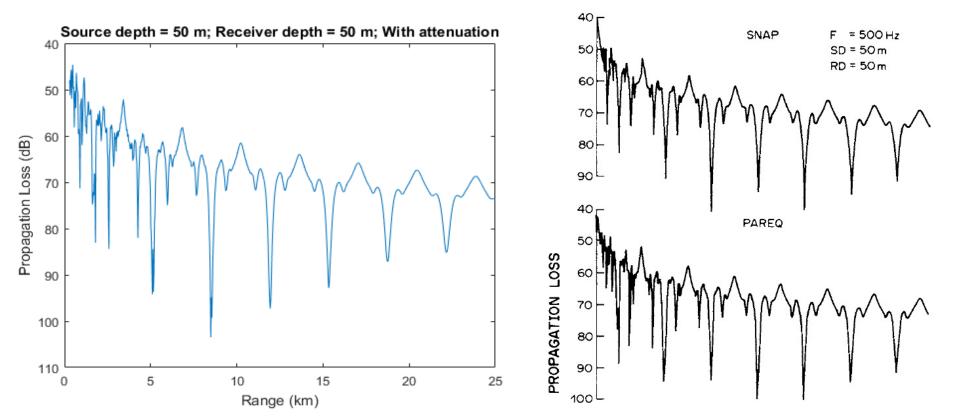
Seafloor Boundary: Pressure Release ( $\Psi$ =0)

• Isovelocity shallow water Case (ISWC) (Jensen and Kuperman, 1979)



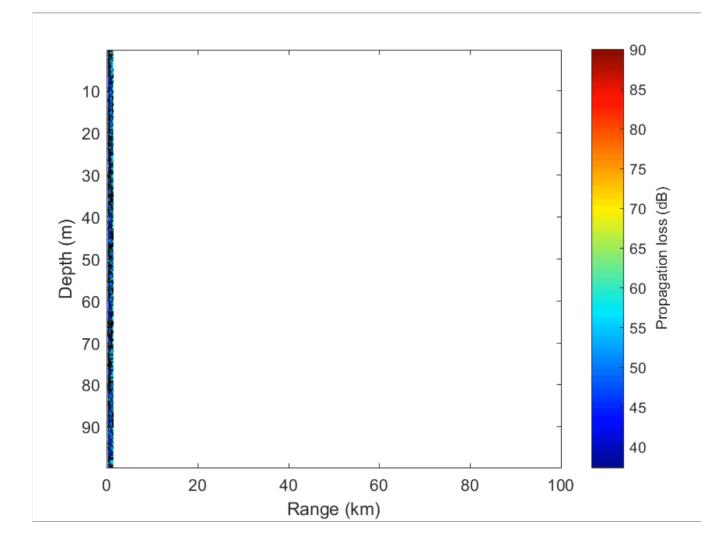
F. Jensen and W. A. Kuperman, "Environmental Acoustical Modeling at Saclant Cen", Saclant Cen Rep. SR – 34 (1979)

• Isovelocity shallow water Case (ISWC)



(Jensen and Kuperman, 1979)

F. Jensen and W. A. Kuperman, "Environmental Acoustical Modeling at Saclant Cen", Saclant Cen Rep. SR – 34 (1979)



#### Variable-Density PE

• Recall:

$$\frac{\partial \psi}{\partial r} = \frac{\rho i}{2k_0} \left( \frac{\partial}{\partial z} \left( \frac{1}{\rho} \frac{\partial \psi}{\partial z} \right) + \frac{1}{r^2} \frac{\partial}{\partial \theta} \left( \frac{1}{\rho} \frac{\partial \psi}{\partial \theta} \right) \right) + \frac{ik_0}{2} \left( n^2 - 1 \right) \psi$$

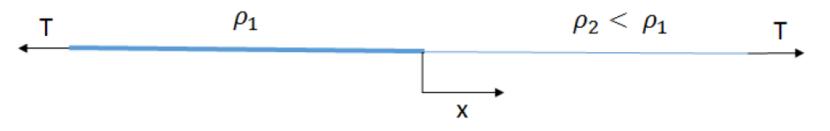
• Can be rewritten as:

$$\frac{\partial \psi}{\partial r} = \frac{i}{2k_0} \left( \frac{\partial^2 \psi}{\partial z^2} + \frac{1}{r^2} \frac{\partial^2 \psi}{\partial \theta^2} \right) + \frac{ik_0}{2} \left( n_{eff}^2 - 1 \right) \psi$$

Where:

$$n_{eff}^2 = n^2 + \frac{1}{2k_0^2} \rho^{1/2} \nabla \cdot \left( \rho^{-3/2} \nabla \rho \right)$$

# Variable-Density PE - Analogy to wave motion in taut string with stepped density



• Approach 1: Solve 2 wave equations with constant density and impose interface conditions, i.e.:

$$\frac{\rho_1}{T} \frac{\partial^2 y}{\partial x^2} = \frac{\partial^2 y}{\partial x^2} \text{for } x < 0$$
$$\frac{\rho_2}{T} \frac{\partial^2 y}{\partial x^2} = \frac{\partial^2 y}{\partial x^2} \text{for } x > 0$$

With

 Approach 2: Solve the wave equation on −∞ < x < +∞ with variable density, i.e.:

$$\frac{\rho(x)}{T}\frac{\partial^2 y}{\partial x^2} = \frac{\partial^2 y}{\partial x^2}$$

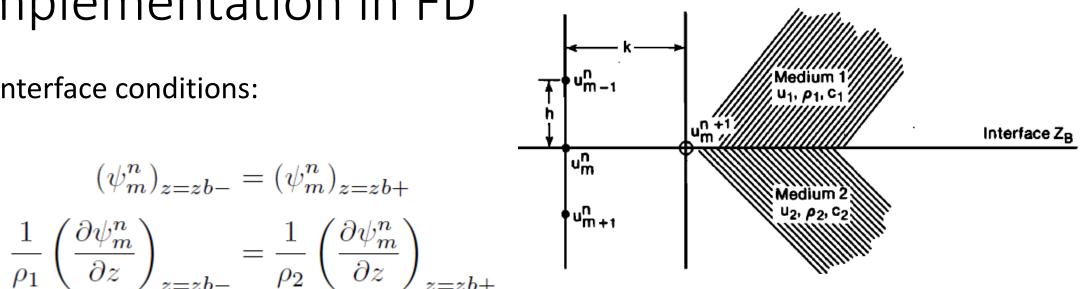
With

$$\rho(x) = \begin{cases} \rho_1 & \text{if } x < 0\\ \rho_2 & \text{if } x > 0 \end{cases}$$

# Variable-Density PE – Approach 1: implementation in FD

• Interface conditions:

 $(\psi_m^n)_{z=zb-} = (\psi_m^n)_{z=zb+}$ 

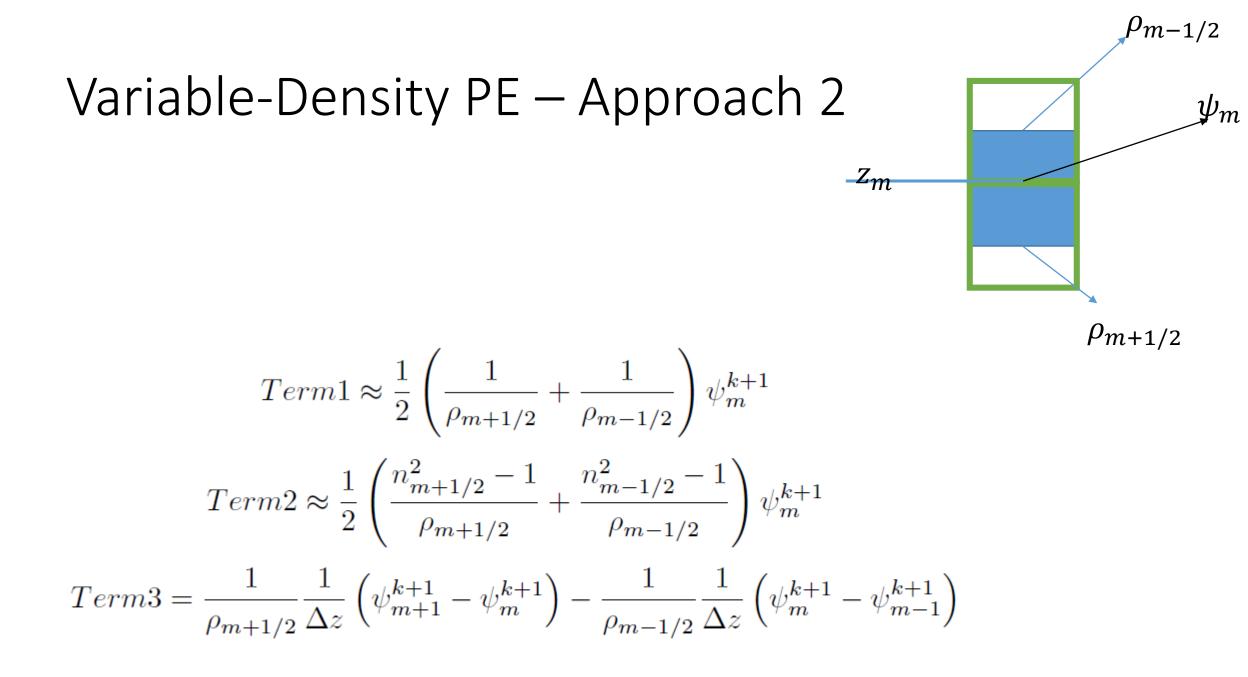


$$\frac{d\psi_m^n}{dr} = \left(\frac{1}{b_1} + \frac{\rho_1}{\rho_2}\frac{1}{b_2}\right)^{-1} \left[ \left(\frac{a_1}{b_1} + \frac{\rho_1}{\rho_2}\frac{a_2}{b_2}\right)\psi_m^n + \frac{2}{\Delta z^2}\left(\frac{\rho_1}{\rho_2}\left(\psi_{m+1}^n - \psi_m^n\right) - \left(\psi_m^n - \psi_{m-1}^n\right)\right) \right]$$

Variable-Density PE – Approach 2  

$$\begin{bmatrix} \frac{1}{\rho} - \frac{\delta}{4} \left( \frac{n^2 - 1}{\rho} + \frac{1}{k_0^2} \frac{\partial}{\partial z} \left( \frac{1}{\rho} \frac{\partial}{\partial z} \right) \right) \end{bmatrix} \psi_{k+1} = \begin{bmatrix} \frac{1}{\rho} + \frac{\delta}{4} \left( \frac{n^2 - 1}{\rho} + \frac{1}{k_0^2} \frac{\partial}{\partial z} \left( \frac{1}{\rho} \frac{\partial}{\partial z} \right) \right) \end{bmatrix} \psi_k \qquad \rho_{m+1/2}$$

$$LHS = \int_{zm-1/2}^{zm+1/2} \frac{1}{\rho} \psi^{k+1} dz - \frac{\delta}{4} \left( \int_{zm-1/2}^{zm+1/2} \frac{n^2 - 1}{\rho} \psi^{k+1} dz + \frac{1}{k_0^2} \int_{zm-1/2}^{zm+1/2} \frac{\partial}{\partial z} \left( \frac{1}{\rho} \frac{\partial \psi^{k+1}}{\partial z} dz \right) \right)$$



## Acknowledgments

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