

# Challenges of modeling interceptors on a planing hull

Final Project for 2.29

# Outline

- Background
  - Theory of planing
  - Interceptors
- Previous work – Experimental testing
- Original Objective
- InterFoam - VOF
- Challenges to modeling
- Conclusions

# Background – Theory of planing

- Displacement – Buoyant forces dominate

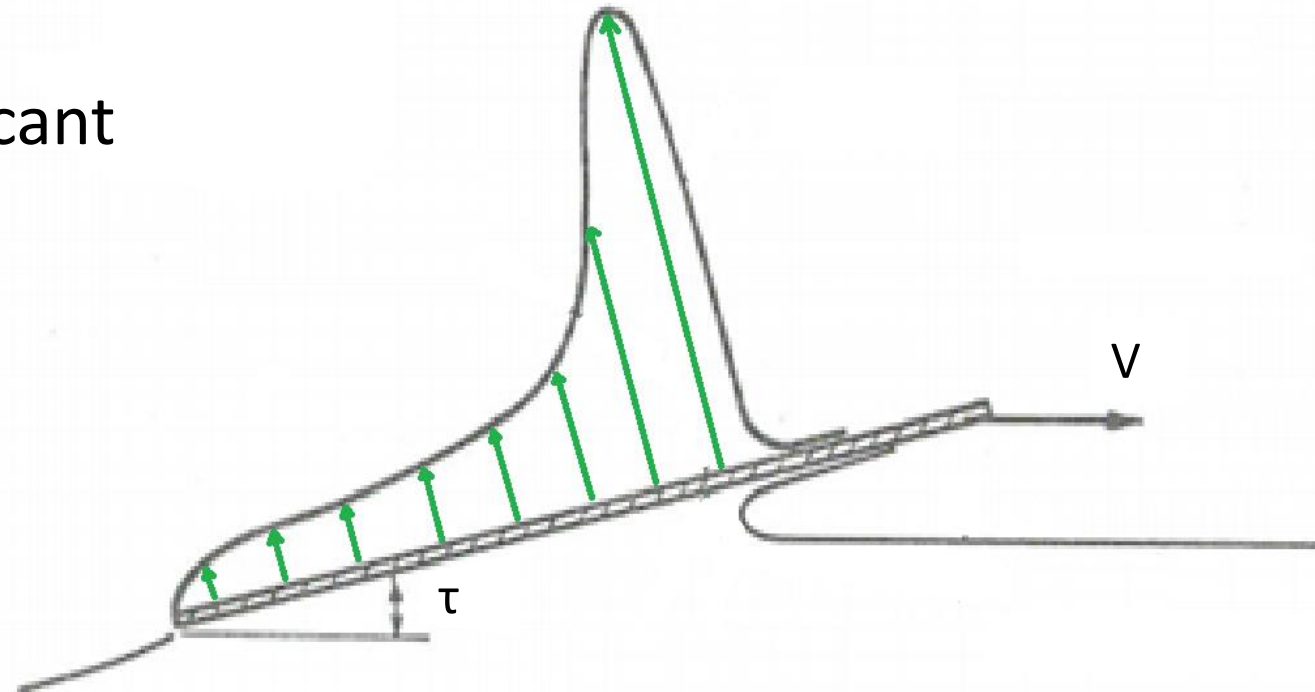
$$\text{Buoyant Force} = \rho g \nabla$$

- Planing – Dynamic lift also significant

$$\text{Lift force} \propto \frac{1}{2} \rho V^2 A_P$$

- Volumetric Froude Number

$$A_P \propto \nabla^{2/3}, \quad F_{\nabla} = \frac{V}{\sqrt{g^3 \nabla}}$$

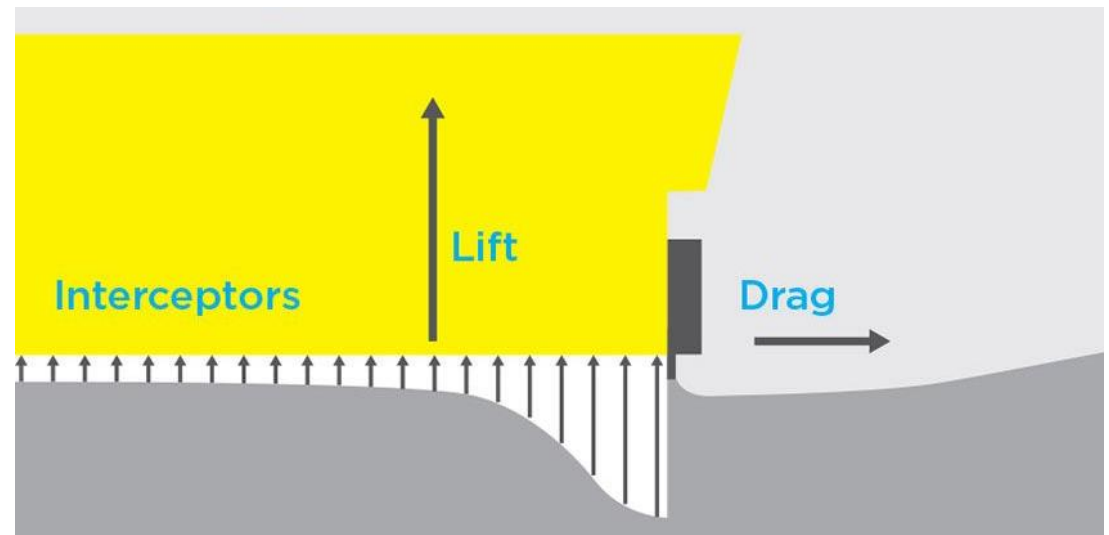


Adapted from Savitsky (1964)

# Background – Interceptors

- Transitional speeds
  - Large bow up trim
  - Significant pressure drag
- Large pressure drag during transition to planing
- Interceptors
  - Create stagnation point
  - Lifts transom
  - Decrease resistance

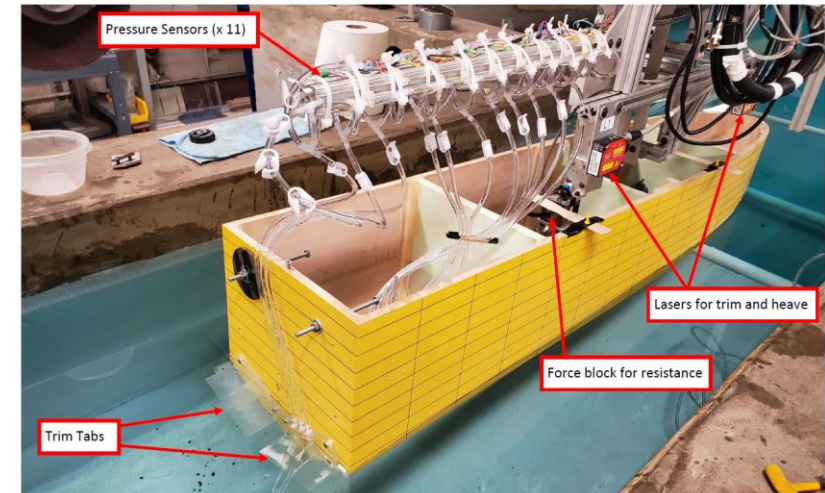
$$F_{\nabla} \sim 2 \text{ to } 3$$



Source: Zipwake.com

# Previous Work – Experimental Tests

- Model:
  - LOA= 1.524m
  - Beam= 0.305m
- Interceptors and trim tabs
- $F_{\nabla}$  1.11 – 3.14
- Multiple deployments
- Longitudinal pressure forward of interceptor



Source: Gaylo Roske (2019)

# Objective

- Model one speed and interceptor deployment. Validate with experimental data and compare results using different turbulence models.

- Choose largest deployment and mid-range speed

$$F_{\nabla} = 2.40 \quad (U \approx 4 \frac{m}{s}) \quad L_{deployment} = 1.143mm \quad \tau = 0.8^{\circ}$$

- From underside images calculated mean wetted length



$$Re_L = 4.7 \times 10^6$$

# InterFoam – Volume of Fluid method

- VOF – track free surface using a continuity equation
- InterFoam implementation:
  - Very close to machine precision mass conservative
  - Iteration brings closer
- Machine precision VOF methods exist.

$$\alpha(\vec{x}) = \begin{cases} 1, & \vec{x} \in \text{fluid 1} \\ 0, & \vec{x} \in \text{fluid 2} \end{cases}$$

$$\int_{\Omega} \alpha(\vec{x}) dV / \int_{\Omega} dV \in [0, 1]$$

$$\begin{aligned} \rho(\vec{x}) &= \alpha(\vec{x})\rho_1 + (1 - \alpha(\vec{x}))\rho_2 \\ \mu(\vec{x}) &= \alpha(\vec{x})\mu_1 + (1 - \alpha(\vec{x}))\mu_2 \end{aligned}$$

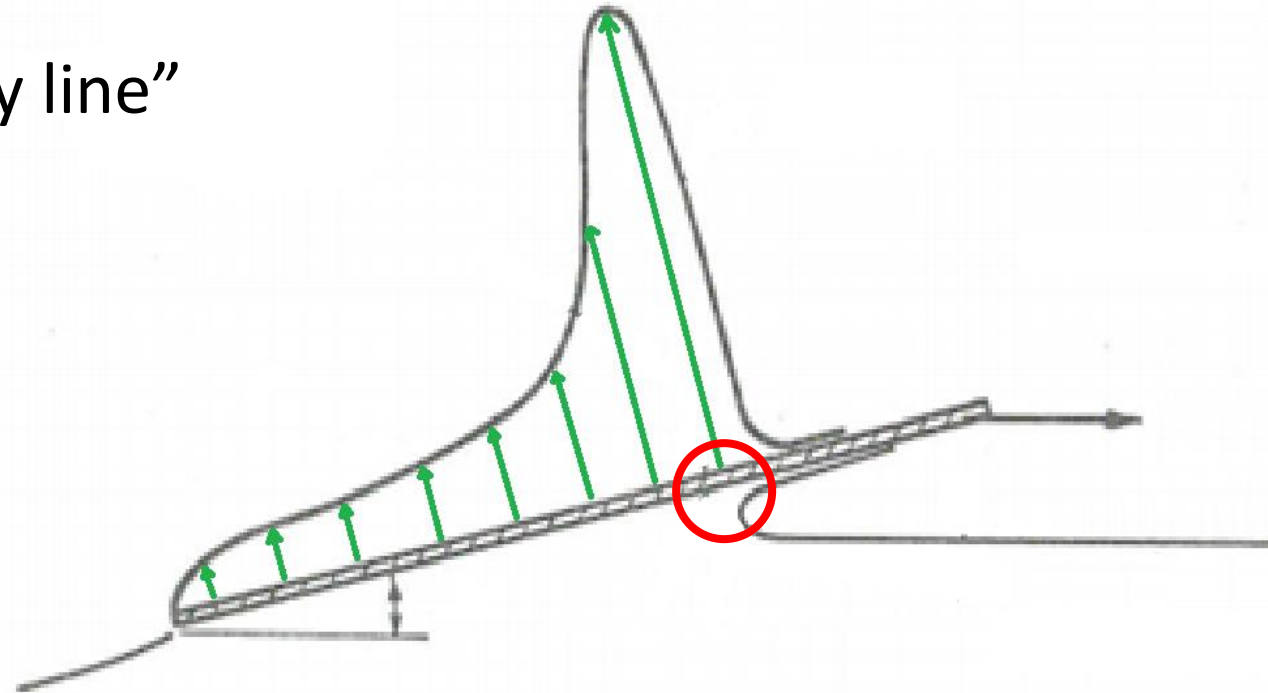
\*Ignored surface tension

$$\frac{\partial \alpha}{\partial t} + \frac{\partial(\alpha u_j)}{\partial x_j} = 0$$



# Challenges – Adverse pressure gradient

- Stagnation point near bow – “Spray line”
- $k - \epsilon$ , accumulates epsilon
- $k - \omega$ , better
- Spray line needs grid refinement
  - location difficult to predict
- Switched to 2D simulation
  - Modeled forward top boundary condition as a symmetry plane.



Adapted from Savitsky (1964)



# Challenges – Grid Resolution

- $\frac{L_{deployment}}{L_{hull}} \approx 1000$       Minimum Domain Length =  $3 L_{hull}$
- For planing hulls, much larger domain lengths often needed.
- To model interceptor, layers near nearby would need aspect ratios near 1, unlike typical boundary layer cells.
- Difficult to maintain reasonable grid sizes, aspect ratios, and cell expansion rates.

# Challenges – Wall and Interceptor refinement

- Using ITTC-1957 friction coefficient,

$$y^+ (L_{deployment} = 1.143mm) \approx 180$$

- For wall functions, first cell center  $30 < y^+ < 100$ .
- Only three cells to capture interceptor deployment.
- To accurately model interceptor, would likely need to use near wall,  $y^+ \approx 1$ .

# Challenges – Courant Restriction

- Transom usually fully ventilated

$$p_{front} \approx 0.3 \frac{1}{2} \rho V^2 + \rho g z \qquad p_{back} \approx 0$$

- Velocity near tip of interceptor  $O(V)$

- For  $\Delta x \sim L_{deployment}/3$        $V = 4 \text{ m/s}$       and  $CFL = 1$

$$\Delta t \sim 10^{-6} \text{ s}$$

Assuming  $T_{converge} \sim 10 L_{Domain}/V$ , need  $O(10^7)$  timesteps

# Conclusions

- Due primarily to stagnation points close to the free surface, planing creates a very computationally expensive problem.
- $k - \epsilon$  is not stable in simulations with strong adverse pressure gradients, and can become unstable at stagnation points.
- Numerically modeling realistic model scale interceptor deployments adds significant computational cost.

# Questions?