Diesel injection, ignition, and fuel air mixing

- 1. Fuel spray phenomena
- 2. Spontaneous ignition
- 3. Effects of fuel jet and charge motion on mixingcontrolled combustion
- 4. Fuel injection hardware
- 5. Challenges for diesel combustion

DIESEL FUEL INJECTION

The fuel spray serves multiple purposes:

- Atomization
- Fuel distribution
- Fuel/air mixing

Typical Diesel fuel injector

- Injection pressure: 1000 to 2200 bar
- 5 to 20 holes at ~ 0.12 0.2 mm diameter
- Drop size 0.1 to 10 μm
- For best torque, injection starts at about 20° BTDC

Injection strategies for NOx control

- Late injection (inj. starts at around TDC)
- · Other control strategies:
 - > Pilot and multiple injections, rate shaping, water emulsion

Diesel Fuel Injection System

(A Major cost of the diesel engine)

- Performs fuel metering
- Provides high injection pressure
- · Distributes fuel effectively
 - Spray patterns, atomization etc.
- · Provides fluid kinetic energy for charge mixing

Typical systems:

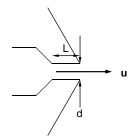
- Pump and distribution system (100 to 1500 bar)
- Common rail system (1000 to 1800 bar)
- Hydraulic pressure amplification
- Unit injectors (1000 to 2200 bar)
- Piezoelectric injectors (1800 bar)
- Electronically controlled

EXAMPLE OF DIESEL INJECTION

(Hino K13C, 6 cylinder, 12.9 L turbo-charged diesel engine, rated at 294KW@2000 rpm)

- Injection pressure = 1400 bar; duration = 40°CA
- BSFC 200 g/KW-hr
- Fuel delivered per cylinder per injection at rated condition
 - $-0.163 \text{ gm} \sim 0.21 \text{ cc} (210 \text{ mm}^3)$
- Averaged fuel flow rate during injection
 - $-64 \text{ mm}^3/\text{ms}$
- 8 nozzle holes, at 0.2 mm diameter
 - Average exit velocity at nozzle ~253 m/s

Typical physical quantities in nozzle flow



- Diesel fuel @ 100°C
 s.g. ~ 0.78, μ~5x10⁻⁴ N-s/m²
- Nozzle diameter ~0.2 mm
- L/d ~ 5 to 10
- Reynolds No. ~ 10⁵ (turbulent)
- Pressure drop in nozzle
 ~30 bar << driving pressure
 (~1000 bar)
- Injection velocity

$$u \approx \sqrt{\frac{2\Delta P}{\rho_{fuel}}} \approx 500 \text{ m/s } @ \Delta P \text{ of } 1000 \text{ bar}$$

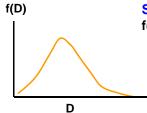
Fuel Atomization Process

 Liquid break up governed by balance between aerodynamic force and surface tension

Webber Number
$$(W_b) = \frac{\rho_{gas}u^2d}{\sigma}$$

- Critical Webber number: W_{b,critical} ~ 30; diesel fuel surface tension ~ 2.5x10⁻² N/m
- Typical W_b at nozzle outlet > W_{b,critical}; fuel shattered into droplets within ~ one nozzle diameter
- Droplet size distribution in spray depends on further droplet breakup, coalescence and evaporation





Size distribution:

f(D)dD = probability of finding particle with diameter in the range of (D, D + dD)

$$1=\int\limits_0^\infty f(D)dD$$

Average diameter

$$\overline{D} = \int\limits_0^\infty f(D)\,D\,dD$$

Volume distribution

$$\frac{1}{V}\frac{dV}{dD} = \frac{f(D)D^3}{\int\limits_0^\infty f(D)D^3dD}$$

Sauter Mean Diameter (SMD)

$$D_{32} = \frac{\int\limits_{0}^{\infty} f(D) D^{3} dD}{\int\limits_{0}^{\infty} f(D) D^{2} dD}$$

Droplet Size Distribution

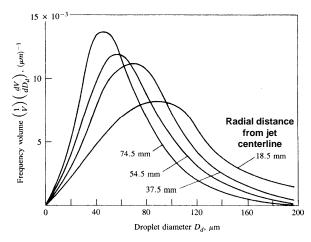
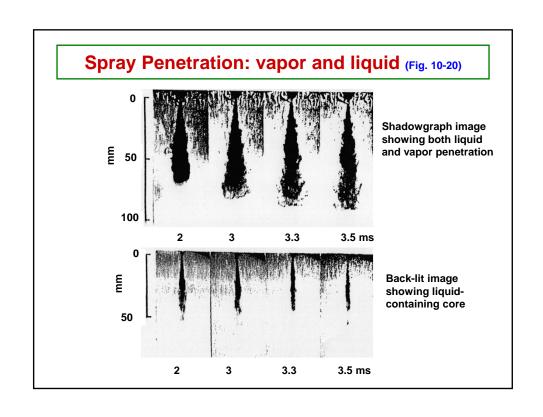


Fig. 10.28 Droplet size distribution measured well downstream; numbers on the curves are radial distances from jet axis. Nozzle opening pressure at 10 MPa; injection into air at 11 bar.

Droplet Behavior in Spray

- Small drops (~ micron size) follow gas stream; large ones do not
 - Relaxation time $\tau \propto d^2$
- - Evaporation time small once charge is ignited
- Spray angle depends on nozzle geometry and gas density : $\tan(\theta/2) \propto \sqrt{(\rho_{gas}/\rho_{liquid})}$
- Spray penetration depends on injection momentum, mixing with charge air, and droplet evaporation



Auto-ignition Process

PHYSICAL PROCESSES (Physical Delay)

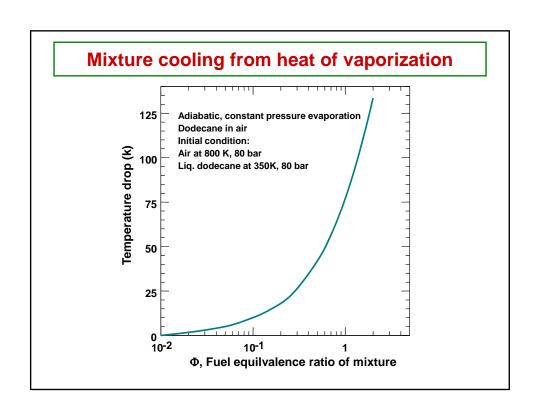
- > Drop atomization
- > Evaporation
- > Fuel vapor/air mixing

CHEMICAL PROCESSES (Chemical Delay)

- > Chain initiation
- ➤ Chain propagation
- > Branching reactions

CETANE IMPROVERS

- ➤ Alkyl Nitrates
 - 0.5% by volume increases CN by ~10



Ignition Mechanism: similar to SI engine knock

CHAIN BRANCHING EXPLOSION

Chemical reactions lead to increasing number of radicals, which leads to rapidly increasing reaction rates

Formation of Branching Agents

Chain Initiation

 $R\dot{O}_2 + RH \Rightarrow ROOH + \dot{R}$

 $RH + O_2 \Rightarrow \dot{R} + H\dot{O}_2$

 $R\dot{O}_2 \Rightarrow R'CHO + R''\dot{O}$

Chain Propagation

Degenerate Branching

 $\dot{R} + O_2 \Rightarrow R\dot{O}_2$, etc.

 $ROOH \Rightarrow R\dot{O} + \dot{O}H$

 $R'CHO + O_2 \Rightarrow R'\dot{C}O + H\dot{O}_2$

Cetane Rating

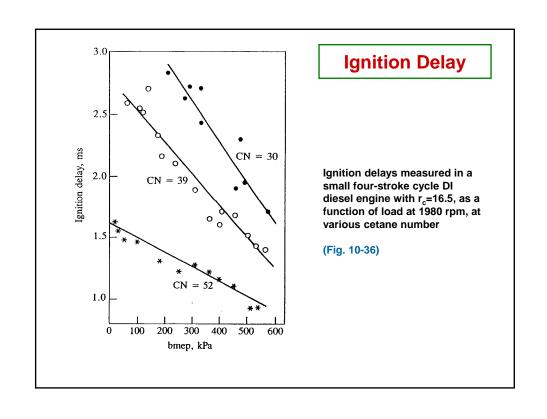
(Procedure is similar to Octane Rating for SI Engine; for details, see10.6.2 of text)

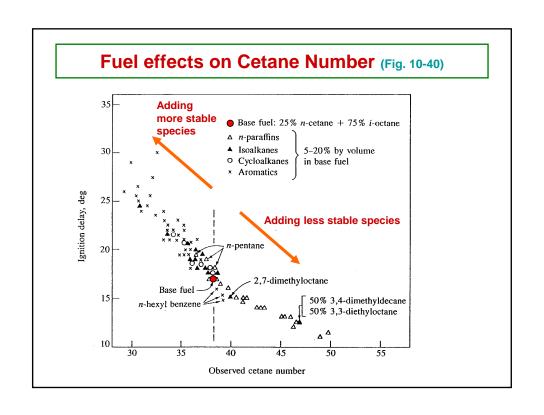
Primary Reference Fuels:

- Normal cetane ($C_{16}H_{34}$): CN = 100
- ightharpoonup Hepta-Methyl-Nonane (HMN; $C_{16}H_{34}$): CN = 15 (2-2-4-4-6-8-8 Heptamethylnonane)

Rating:

- > Operate CFR engine at 900 rpm with fuel
- ➤ Injection at 13° BTC
- Adjust compression ratio until ignition at TDC
- Replace fuel by reference fuel blend and change blend proportion to get same ignition point
- > CN = % n-cetane + 0.15 x % HMN





Ignition Delay Calculations

 Difficulty: do not know local conditions (species concentration and temperature) to apply kinetics information

Two practical approaches:

• Use an "instantaneous" delay expression

$$\tau(T,P) = P^{-n}exp(-E_A/T)$$

and solve ignition delay (τ_{id}) from

$$1 = \textstyle \int_{t}^{t} \! \! si^{+\tau} id \frac{1}{\tau(T(t),P(t))} dt$$

• Use empirical correlation of τ_{id} based on T, P at an appropriate charge condition; e.g. Eq. (10.37 of text)

$$\tau_{id}(CA) = (0.36 + 0.22\overline{S}_p(m/s)) \exp \left[E_A \left(\frac{1}{\widetilde{R}T(K)} - \frac{1}{17190} \right) + \left(\frac{21.2}{P(bar) - 12.4} \right)^{0.63} \right]$$

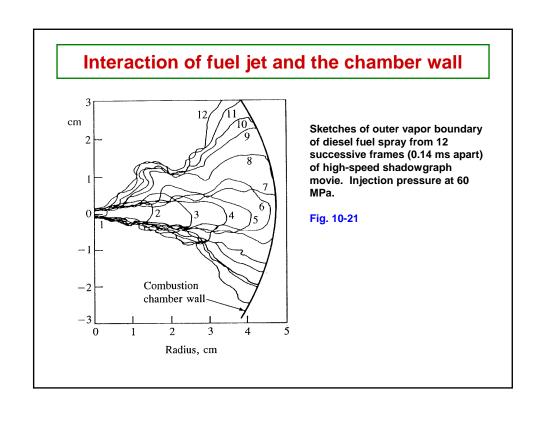
 E_A (Joules per mole) = 618,840 / (CN+25)

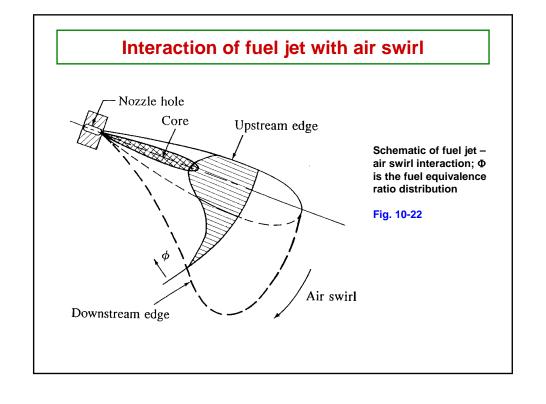
Diesel Engine Combustion Air Fuel Mixing Process

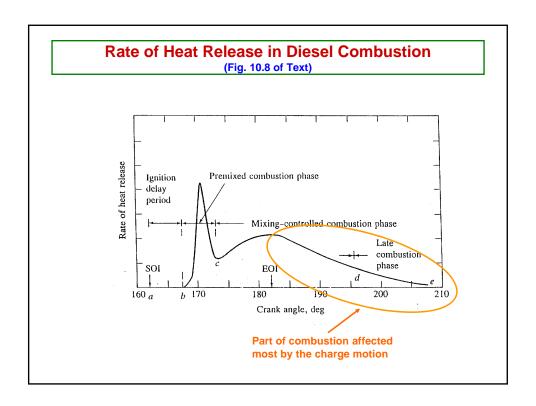
- Importance of air utilization
 - Smoke-limit A/F ~ 20
- Fuel jet momentum / wall interaction has a larger influence on the early part of the combustion process
- Charge motion impacts the later part of the combustion process (after end-of-injection)

CHARGE MOTION CONTROL

- Intake created motion: swirl, etc.
 - Not effective for low speed large engine
- Piston created motion squish





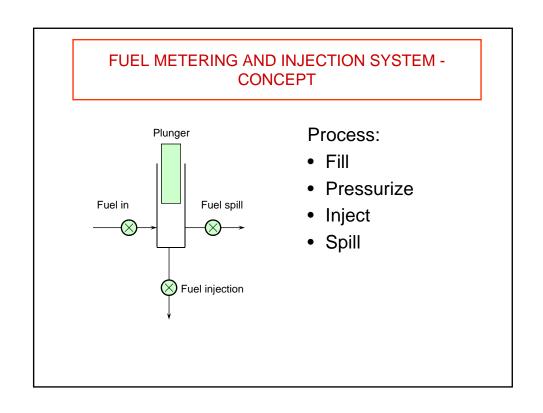


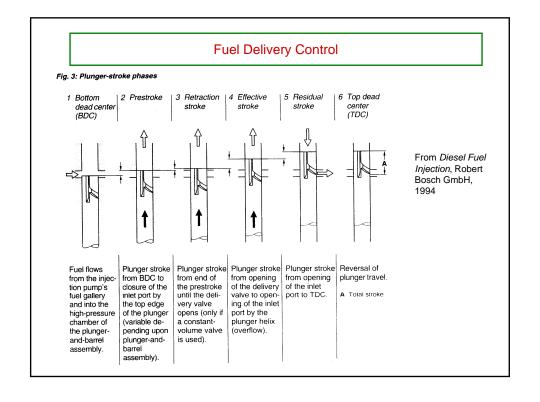
DIESEL FUEL INJECTION HARDWARE

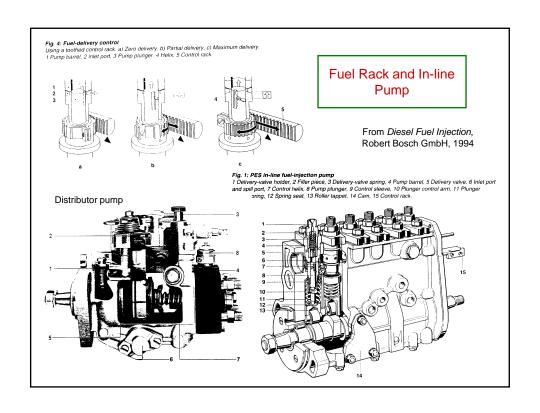
- High pressure system
 - precision parts for flow control
- Fast action
 - high power movements

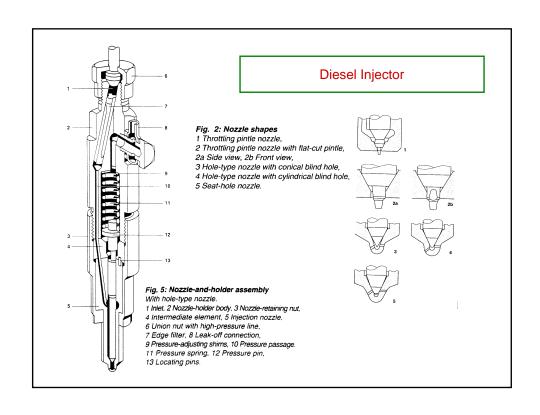


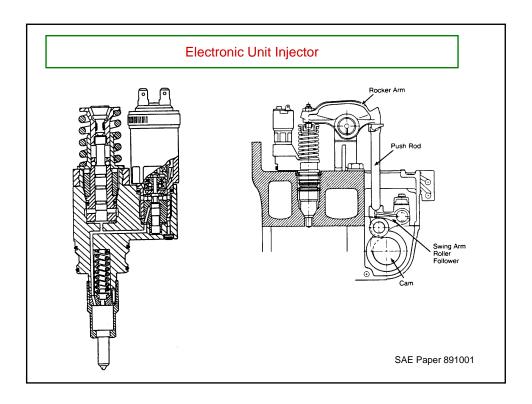
Expensive system





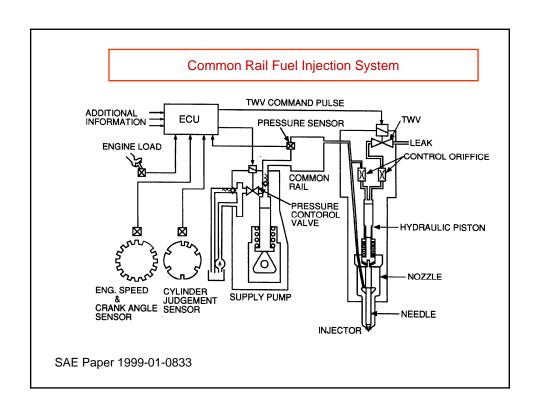


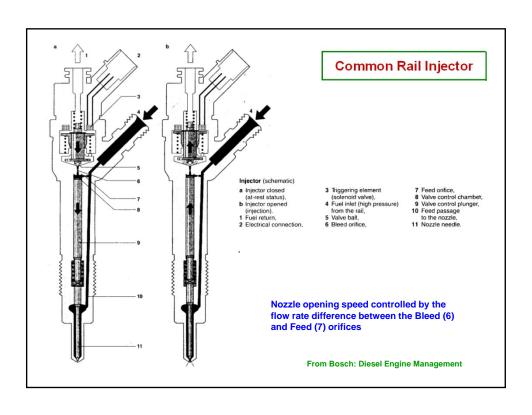


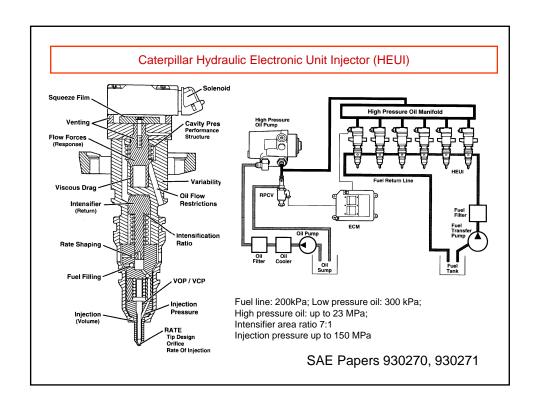


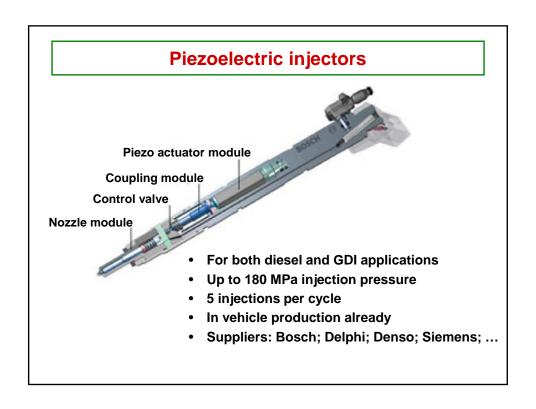
Injection pressure

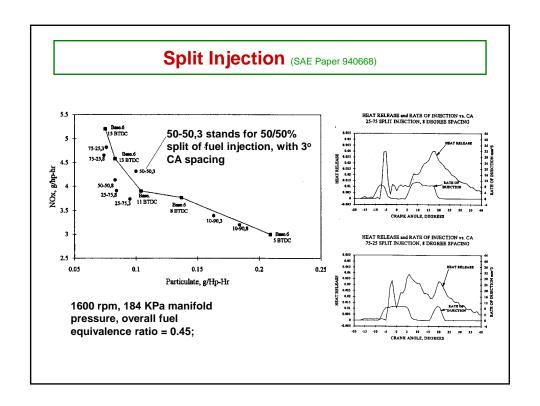
- Positive displacement injection system
 - Injection pressure adjusted to accommodate plunger motion
 - Injection pressure $\propto \text{rpm}^2$
- · Injection characteristics speed dependent
 - Injection pressure too high at high rpm
 - Injection pressure too low at low rpm











CHALLENGES IN DIESEL COMBUSTION

Heavy Duty Diesel Engines

- NOx emission
- · Particulate emission
- Power density
- Noise

High Speed Passenger Car Diesel Engines

- All of the above, plus
 - Fast burn rate

Cavitation in Injection Nozzle

- Cavitation happens when local pressure is lower than the fluid vapor pressure
- Effects
 - Affects the spray angle
 - Damage to the nozzle passage
- · Factors affecting cavitation
 - Combustion chamber pressure
 - Local streamline curvature within the nozzle

