

## 6.946 Assignment 4<sup>1</sup>

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### Exercise 2.2: Steiner's Theorem

The moment of inertia with respect to the first line is given by  $I = \sum_{\alpha} m_{\alpha} (\xi_{\alpha}^{\perp})^2$ , where  $m_{\alpha}$  is the mass of the individual particle, and  $\xi_{\alpha}$  is the vector from the reference point to the individual point. Since the axis of rotation goes through the center of mass, the first line goes through the reference point.

Let  $\vec{R}$  be a perpendicular vector from the first line to the second, and let  $\xi_{\alpha}^{\perp'} = \xi_{\alpha}^{\perp} + \vec{R}$  be the reference vector from the second line to the individual particle. The new moment of inertia  $I'$  is given by:

$$\begin{aligned} I' &= \sum_{\alpha} m_{\alpha} (\xi_{\alpha}^{\perp'})^2 = \sum_{\alpha} m_{\alpha} (\xi_{\alpha}^{\perp} + \vec{R})^2 = \sum_{\alpha} m_{\alpha} \left( (\xi_{\alpha}^{\perp})^2 + 2\xi_{\alpha}^{\perp} \vec{R} + R^2 \right) = \\ &= \sum_{\alpha} m_{\alpha} (\xi_{\alpha}^{\perp})^2 + \sum_{\alpha} m_{\alpha} 2\xi_{\alpha}^{\perp} \vec{R} + R^2 \sum_{\alpha} m_{\alpha} = I + \sum_{\alpha} m_{\alpha} 2\xi_{\alpha}^{\perp} \vec{R} + MR^2 \end{aligned}$$

By the definition of the center of mass,  $\sum_{\alpha} m_{\alpha} \xi_{\alpha}^{\perp} = 0$ , and the middle term drops out. So

$$I' = I + MR^2$$

### Exercise 2.3: Some useful moments of inertia

In the continuous case, we can replace the equation for the moment of inertia with

$$I = \int_M (r_{\perp})^2 dm,$$

where  $r_{\perp}$  is the perpendicular distance from the axis of rotation to the position of  $dm$ , and we integrate over the entire mass.

(a) We introduce a density  $\delta = \frac{dm}{dV} = \frac{M}{\frac{4}{3}\pi R^3}$ . Consider a spherical coordinate system, and let the axis of rotation be the z-axis.

$$I = \int_M r_{\perp}^2 dm = \int_V r_{\perp}^2 \frac{dm}{dV} dV = \delta \int_{\rho=0}^{\rho=R} \int_{\theta=0}^{\theta=2\pi} \int_{\phi=0}^{\phi=\pi} r_{\perp}^2 (\rho^2 \sin \phi d\phi d\theta d\rho)$$

Since the axis of rotation is the z-axis, the perpendicular distance is just  $r_{\perp} = \rho \sin \phi$ , and we continue the calculation<sup>2</sup>:

$$I = \delta \int_{\rho=0}^{\rho=R} \int_{\theta=0}^{\theta=2\pi} \int_{\phi=0}^{\phi=\pi} (\rho \sin \phi)^2 \rho^2 \sin \phi d\phi d\theta d\rho = \delta 2\pi \int_{\rho=0}^{\rho=R} \int_{\phi=0}^{\phi=\pi} \rho^4 \sin^3 \phi d\phi d\rho$$

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<sup>1</sup>This only contains the first four of six problems. I'm turning the other two problems in on Tuesday.

<sup>2</sup>We use the easily verifiable fact that  $\int \sin^3(x) dx = \frac{2}{3} \sin^2(x) \cos(x) + \frac{1}{3} \cos(x)$ .

$$\begin{aligned}
&= \delta 2\pi \frac{R^5}{5} \int_{\phi=0}^{\phi=\pi} \sin^3 \phi \, d\phi = \delta 2\pi \frac{R^5}{5} \left[ \frac{1}{3} \sin^2 \phi \cos \phi + \frac{2}{3} \cos \phi \right]_{\phi=0}^{\phi=\pi} \\
&= \delta 2\pi \frac{R^5}{5} \frac{4}{3} = \frac{M}{\frac{4}{3}\pi R^3} 2\pi \frac{R^5}{5} \frac{4}{3} = \frac{24\pi M R^5}{60\pi R^3} = \frac{2}{5} M R^2
\end{aligned}$$

(b) We introduce a mass-per-surface-area constant  $\delta = \frac{dm}{dS} = \frac{M}{4\pi R^2}$ . Consider a spherical coordinate system, and let the axis of rotation be the z-axis.

$$I = \int_M r_{\perp}^2 dm = \int_S r_{\perp}^2 \frac{dm}{dS} dS = \delta \int_{\theta=0}^{\theta=2\pi} \int_{\phi=0}^{\phi=\pi} r_{\perp}^2 (R^2 \sin \phi \, d\phi \, d\theta)$$

Since the axis of rotation is the z-axis, the perpendicular distance is just  $r_{\perp} = R \sin \phi$ , and we continue the calculation:

$$\begin{aligned}
I &= \delta R^2 \int_{\theta=0}^{\theta=2\pi} \int_{\phi=0}^{\phi=\pi} (R \sin \phi)^2 \sin \phi \, d\phi \, d\theta = \delta R^4 2\pi \int_{\phi=0}^{\phi=\pi} \sin^3 \phi \, d\phi \\
&= \delta R^4 2\pi \left[ \frac{1}{3} \sin^2 \phi \cos \phi + \frac{2}{3} \cos \phi \right]_{\phi=0}^{\phi=\pi} = \delta R^4 2\pi \frac{4}{3} = \frac{M}{4\pi R^2} R^4 2\pi \frac{4}{3} = \frac{8\pi M R^4}{12\pi R^2} = \frac{2}{3} M R^2
\end{aligned}$$

#### Exercise 2.4: Jupiter

(a) We can write the rotational inertia of both a sphere with equal density and a planet as  $\int_V \frac{dm}{dV} r^2 dV$ . In the case of the planet,  $\frac{dm}{dV}$  is a constant density, but in the case of the planet, this term is large when  $r$  is small and small when  $r$  is large. Thus, those mass infinitesimals contribute less to the total value of the integral, since they are integrated at a lower value of  $r$  than in the case of the sphere. Thus, the moment of inertia is smaller for a planet than for a sphere of uniform density of the same mass and radius.

(b) We use a spherical coordinate system, and align the z-axis with the axis of rotation. The variable density is given by  $\frac{dm}{dV} = \frac{M \sin(\pi r/R)}{R^3 \frac{4r}{R}}$ .

$$\begin{aligned}
I &= \int_M r_{\perp}^2 dm = \int_V r_{\perp}^2 \frac{dm}{dV} dV = \int_{r=0}^{r=R} \int_{\theta=0}^{\theta=2\pi} \int_{\phi=0}^{\phi=\pi} (r_{\perp}^2) \left( \frac{M \sin(\pi r/R)}{R^3 \frac{4r}{R}} \right) (r^2 \sin \phi \, d\phi \, d\theta \, dr) \\
&= \frac{M}{4R^2} \int_{r=0}^{r=R} \int_{\theta=0}^{\theta=2\pi} \int_{\phi=0}^{\phi=\pi} (r_{\perp}^2) r \sin(\pi r/R) \sin \phi \, d\phi \, d\theta \, dr \\
&= 2\pi \frac{M}{4R^2} \int_{r=0}^{r=R} \int_{\phi=0}^{\phi=\pi} (r_{\perp}^2) r \sin(\pi r/R) \sin \phi \, d\phi \, dr
\end{aligned}$$

Since the axis of rotation is the z-axis, the perpendicular distance is just  $r_{\perp} = r \sin \phi$ , and we continue the calculation:

$$\begin{aligned}
&= 2\pi \frac{M}{4R^2} \int_{r=0}^{r=R} \int_{\phi=0}^{\phi=\pi} (r^2 \sin^2 \phi) r \sin(\pi r/R) \sin \phi \, d\phi \, dr \\
&= 2\pi \frac{M}{4R^2} \int_{r=0}^{r=R} \int_{\phi=0}^{\phi=\pi} \sin^2 \phi \, r^3 \sin(\pi r/R) \sin \phi \, d\phi \, dr
\end{aligned}$$

$$= 2\pi \frac{M}{4R^2} \int_{r=0}^{r=R} r^3 \sin(\pi r/R) dr \int_{\phi=0}^{\phi=\pi} \sin^3 \phi d\phi$$

We know from **2.3 (a)** that the integral on the right is  $\frac{4}{3}$ . We look up the integral on the left on the internet<sup>3</sup>.

$$\begin{aligned} &= 2\pi \frac{M}{4R^2} \left[ \frac{3\left(\frac{\pi}{R}\right)^2 r^2 - 2\sin(\pi r/R)}{\left(\frac{\pi}{R}\right)^4} - \frac{r\left(\frac{\pi}{R}\right)^2 r^2 - 6\cos(\pi r/R)}{\left(\frac{\pi}{R}\right)^3} \right]_{r=0}^{r=R} \left[ \frac{4}{3} \right] \\ &= 2\pi \frac{M}{3R^2} \left[ \left(0 - \frac{R\left(\frac{\pi}{R}\right)^2 R^2 - 6\cos(\pi)}{\left(\frac{\pi}{R}\right)^3}\right) - (0 - 0) \right] = \frac{2M\pi}{3R^2} \left[ R^4 \frac{\pi^2 - 6}{\pi^3} \right] \\ &= \frac{2MR^2}{3} \frac{\pi^2 - 6}{\pi^2} = \frac{2}{3} \left(1 - \frac{6}{\pi^2}\right) MR^2 \end{aligned}$$

Which is less than the moment of inertia of a sphere with equal, albeit evenly distributed, mass -  $\frac{2}{3}MR^2$ .

### Exercise 2.5: A constraint on the moments of inertia

Let there be some arrangement of particles  $\{\alpha\}$  with mass  $\{m_\alpha\}$  and position  $r_\alpha = r_{\alpha,1}\hat{e}_1 + r_{\alpha,2}\hat{e}_2 + r_{\alpha,3}\hat{e}_3$  with respect to some set of orthonormal axes  $\{\hat{e}_i\}$ . Consider the sum of any two moments of inertia, say  $I_{11}$  and  $I_{22}$ , and compare it with  $I_{33}$ .

$$I_{11} + I_{22} = \sum_{\alpha} m_{\alpha} ((\hat{e}_1 \times r_{\alpha})^2 + (\hat{e}_2 \times r_{\alpha})^2) = \sum_{\alpha} m_{\alpha} ((r_{\alpha,2}^2 + r_{\alpha,3}^2) + (r_{\alpha,1}^2 + r_{\alpha,3}^2))$$

$$I_{33} = \sum_{\alpha} m_{\alpha} (\hat{e}_3 \times r_{\alpha})^2 = \sum_{\alpha} m_{\alpha} (r_{\alpha,1}^2 + r_{\alpha,2}^2)$$

So  $I_{11} + I_{22} \geq I_{33}$ . (In particular, there is only equality if  $\sum_{\alpha} r_{\alpha,3}^2 = 0$ .) By symmetry, this is true for any choice of orthonormal axes. The sum of any two moments of inertia are greater than or equal to the third.

### Exercise 2.6: Principal moments of inertia

(a) We choose a set of axes, and show that they are the principal axes. Let  $(0,0,0)$  be the origin and center of mass, and let  $r_1 = (\frac{1}{\sqrt{3}}, 0, -\frac{1}{4}\sqrt{\frac{2}{3}})$ ,  $r_2, r_3 = (-\frac{1}{2\sqrt{3}}, \pm\frac{1}{2}, -\frac{1}{4}\sqrt{\frac{2}{3}})$ , and  $p_4 = (0, 0, \frac{3}{4}\sqrt{\frac{2}{3}})$  be the four points. Thus, the distance between any two points is 1. The orthogonal axis we choose is  $(\hat{x}, \hat{y}, \hat{z})$ . We intend to calculate the components of the moments of inertia for every combination  $(i, j)$ :

$$I_{ij} = \sum_{\alpha} m_{\alpha} (e_i \times r_{\alpha}) \cdot (e_j \times r_{\alpha})$$

Before we do this, however, we determine the cross product of the axes with the different  $\{r_i\}$ :

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<sup>3</sup><http://integrals.wolfram.com/index.jsp>

$$\hat{x} \times r_1 = \frac{1}{4}\sqrt{\frac{2}{3}}\hat{y}, \quad \hat{y} \times r_1 = -\frac{1}{4}\sqrt{\frac{2}{3}}\hat{x} - \frac{1}{\sqrt{3}}\hat{z}, \quad \hat{z} \times r_1 = \frac{1}{\sqrt{3}}\hat{y}$$

$$\hat{x} \times r_2 = \frac{1}{4}\sqrt{\frac{2}{3}}\hat{y} + \frac{1}{2}\hat{z}, \quad \hat{y} \times r_2 = -\frac{1}{4}\sqrt{\frac{2}{3}}\hat{x} + \frac{1}{2\sqrt{3}}\hat{z}, \quad \hat{z} \times r_2 = -\frac{1}{2}\hat{x} - \frac{1}{2\sqrt{3}}\hat{y}$$

$$\hat{x} \times r_3 = \frac{1}{4}\sqrt{\frac{2}{3}}\hat{y} - \frac{1}{2}\hat{z}, \quad \hat{y} \times r_3 = -\frac{1}{4}\sqrt{\frac{2}{3}}\hat{x} + \frac{1}{2\sqrt{3}}\hat{z}, \quad \hat{z} \times r_3 = \frac{1}{2}\hat{x} - \frac{1}{2\sqrt{3}}\hat{y}$$

$$\hat{x} \times r_4 = -\frac{3}{4}\sqrt{\frac{2}{3}}\hat{y}, \quad \hat{y} \times r_4 = \frac{3}{4}\sqrt{\frac{2}{3}}\hat{x}, \quad \hat{z} \times r_4 = 0$$

We calculate the off-diagonal components  $I_{xy}$ ,  $I_{yz}$  and  $I_{xz}$ , and let the mass term be a constant.

$$I_{xy} = m \sum_{\alpha} (\hat{x} \times r_{\alpha}) \cdot (\hat{y} \times r_{\alpha}) = m(0 + \frac{1}{4\sqrt{3}} - \frac{1}{4\sqrt{3}} + 0) = 0$$

$$I_{yz} = m \sum_{\alpha} (\hat{y} \times r_{\alpha}) \cdot (\hat{z} \times r_{\alpha}) = m(0 + \frac{1}{8}\sqrt{\frac{2}{3}} - \frac{1}{8}\sqrt{\frac{2}{3}} + 0) = 0$$

$$I_{xz} = m \sum_{\alpha} (\hat{x} \times r_{\alpha}) \cdot (\hat{z} \times r_{\alpha}) = m(\frac{\sqrt{2}}{12} - \frac{\sqrt{2}}{24} - \frac{\sqrt{2}}{24} + 0) = 0$$

By symmetry,  $I_{yx} = I_{zy} = I_{zx} = 0$ , and the off-diagonal elements are zero. Thus, our chosen axes are the principal axes. We now find the principal moments of inertia.

$$I_{xx} = m \sum_{\alpha} (\hat{x} \times r_{\alpha}) \cdot (\hat{x} \times r_{\alpha}) = m\frac{1}{16}\frac{2}{3} + 2m\left(\frac{1}{16}\frac{2}{3} + \frac{1}{4}\right) + m\frac{9}{16}\frac{2}{3} = m$$

$$I_{yy} = m \sum_{\alpha} (\hat{y} \times r_{\alpha}) \cdot (\hat{y} \times r_{\alpha}) = m\left(\frac{1}{16}\frac{2}{3} + \frac{1}{3}\right) + 2m\left(\frac{1}{16}\frac{2}{3} + \frac{1}{12}\right) + m\frac{9}{16}\frac{2}{3} = m$$

$$I_{zz} = m \sum_{\alpha} (\hat{z} \times r_{\alpha}) \cdot (\hat{z} \times r_{\alpha}) = m\frac{1}{3} + 2m\left(\frac{1}{4} + \frac{1}{12}\right) + 0 = m$$

Let  $R$  be the distance between the points, or, the scale of the arrangement. We chose  $R$  to be 1 earlier, but we can extend this calculation to a general tetrahedral arrangement by multiplying the principal moments of inertia by  $R^2$ . Thus, the principal axes are  $\hat{x}, \hat{y}, \hat{z}$ , and the corresponding principal moments of inertia are each  $mR^2$ , which is what we wanted to show.

**(b)** Let the cube with side length  $R$  centered at  $(0, 0, 0)$  be described by  $-\frac{R}{2} \leq x, y, z \leq \frac{R}{2}$ . We will show that  $(\hat{x}, \hat{y}, \hat{z})$  are the principal axes. Let the cube have a uniform density  $\delta = \frac{M}{R^3}$ .

First, we compute the off-diagonal inertial moments. Let  $r(x, y, z) = x\hat{x} + y\hat{y} + z\hat{z}$  be the vector from the origin to the point at  $(x, y, z)$ .

$$I_{xy} = \int_V \delta(\hat{x} \times r) \cdot (\hat{y} \times r) dV = \delta \int_V (-z\hat{y} + y\hat{z}) \cdot (z\hat{x} - x\hat{z}) dV = \delta \int_V -xy dV$$

But by symmetry, this is zero, and so are the rest of the off-diagonal components. Thus, the axes we have chosen are the principal axes, and we go to calculate the principal moments.

$$\begin{aligned} I_{xx} &= \int_V \delta(\hat{x} \times r) \cdot (\hat{x} \times r) dV = \delta \int_V (-z\hat{y} + y\hat{z}) \cdot (-z\hat{y} + y\hat{z}) dV = \delta \int_V z^2 + y^2 dV \\ &= \delta \int_V z^2 + y^2 dV = \delta R \int_{-R/2}^{R/2} \int_{-R/2}^{R/2} z^2 + y^2 dz dy = 2\delta R^2 \int_{-R/2}^{R/2} z^2 dz = 2\delta R^2 \frac{1}{12} R^3 = \frac{1}{6} MR^2 \end{aligned}$$

Similarly,  $I_{yy} = I_{zz} = \frac{1}{6} MR^2$ .

(c) The center of mass of this arrangement is  $(\frac{-1+1+1+0+0}{5}, \frac{0+0+1+0+0}{5}, \frac{0+0+0+0+1}{5}) = (\frac{1}{5}, \frac{1}{5}, \frac{1}{5})$ . Our plan of attack is to choose any set of orthogonal axes, and to calculate the tensor matrix  $I$ . The eigenvalues of the matrix are the principal moments of inertia, and the eigenvectors are the principal axes. Since it contributes only a multiplicative term, we let the mass  $m_\alpha = 1$  for all  $\alpha$ .

We choose  $(\hat{x}, \hat{y}, \hat{z})$  as our axes, and calculate the cross product of each of these with the relative displacement vectors for the points. First we calculate these new vectors:

$$r_1 = \left(\frac{4}{5}, -\frac{1}{5}, -\frac{1}{5}\right), r_2 = \left(-\frac{6}{5}, -\frac{1}{5}, -\frac{1}{5}\right), r_3 = \left(\frac{4}{5}, \frac{4}{5}, -\frac{1}{5}\right)$$

$$r_4 = \left(-\frac{1}{5}, -\frac{1}{5}, -\frac{1}{5}\right), r_5 = \left(-\frac{1}{5}, -\frac{1}{5}, \frac{4}{5}\right)$$

Then the crossproducts.

$$\hat{x} \times r_1 = \frac{1}{5}\hat{y} - \frac{1}{5}\hat{z}, \hat{y} \times r_1 = -\frac{1}{5}\hat{x} - \frac{4}{5}\hat{z}, \hat{z} \times r_1 = \frac{1}{5}\hat{x} + \frac{4}{5}\hat{y}$$

$$\hat{x} \times r_2 = \frac{1}{5}\hat{y} - \frac{1}{5}\hat{z}, \hat{y} \times r_2 = -\frac{1}{5}\hat{x} + \frac{6}{5}\hat{z}, \hat{z} \times r_2 = \frac{1}{5}\hat{x} - \frac{6}{5}\hat{y}$$

$$\hat{x} \times r_3 = \frac{1}{5}\hat{y} + \frac{4}{5}\hat{z}, \hat{y} \times r_3 = -\frac{1}{5}\hat{x} - \frac{4}{5}\hat{z}, \hat{z} \times r_3 = -\frac{4}{5}\hat{x} + \frac{4}{5}\hat{y}$$

$$\hat{x} \times r_4 = \frac{1}{5}\hat{y} - \frac{1}{5}\hat{z}, \hat{y} \times r_4 = -\frac{1}{5}\hat{x} + \frac{1}{5}\hat{z}, \hat{z} \times r_4 = \frac{1}{5}\hat{x} - \frac{1}{5}\hat{y}$$

$$\hat{x} \times r_5 = -\frac{4}{5}\hat{y} - \frac{1}{5}\hat{z}, \hat{y} \times r_5 = \frac{4}{5}\hat{x} + \frac{1}{5}\hat{z}, \hat{z} \times r_5 = \frac{1}{5}\hat{x} - \frac{1}{5}\hat{y}$$

Now we calculate entries in the matrix  $I$ , using  $I_{ij} = \sum_\alpha (\hat{e}_i \times r_\alpha) \cdot (\hat{e}_j \times r_\alpha)$ .

$$I_{xx} = \frac{2}{25} + \frac{2}{25} + \frac{17}{25} + \frac{2}{25} + \frac{17}{25} = \frac{8}{5}$$

$$I_{yy} = \frac{17}{25} + \frac{37}{25} + \frac{17}{25} + \frac{2}{25} + \frac{17}{25} = \frac{18}{5}$$

$$I_{zz} = \frac{17}{25} + \frac{37}{25} + \frac{32}{25} + \frac{2}{25} + \frac{2}{25} = \frac{18}{5}$$

And the off-diagonal moments.

$$I_{xy} = \frac{4}{25} - \frac{6}{25} - \frac{16}{25} - \frac{1}{25} - \frac{1}{25} = \frac{4}{5}$$

$$I_{yz} = -\frac{1}{25} - \frac{1}{25} + \frac{4}{25} - \frac{1}{25} + \frac{4}{25} = \frac{1}{5}$$

$$I_{xz} = \frac{4}{25} - \frac{6}{25} + \frac{4}{25} - \frac{1}{25} + \frac{4}{25} = \frac{1}{5}$$

Since the  $I^T = I$ , we have

$$I = \frac{1}{5} \begin{pmatrix} 8 & 4 & 1 \\ 4 & 18 & 1 \\ 1 & 1 & 18 \end{pmatrix}$$

I used Scientific Python (SciPy) to solve for the eigenvalues and eigenvectors of this matrix.

```
>>> import scipy; import scipy.linalg
>>> scipy.linalg.eig(1/5. * scipy.array([[8,4,1],[4,18,1],[1,1,18]]))
(array([ 1.31273832+0.j,  4.03274534+0.j,  3.45451633+0.j]),
 array([[ -0.94401077,  0.30599901, -0.12332182],
        [ 0.3254508 ,  0.80245031, -0.50015525],
        [ 0.05408738,  0.51228712,  0.85710936]]))
```

Thus, the principal axes are, to three decimal places,  $-.944\hat{x} + .305\hat{y} + -.123\hat{z}$ ,  $.325\hat{x} + .802\hat{y} + -.500\hat{z}$ , and  $.054\hat{x} + .512\hat{y} + .857\hat{z}$ , with associated principal moments of inertia 1.313m, 4.033m and 3.455m.