

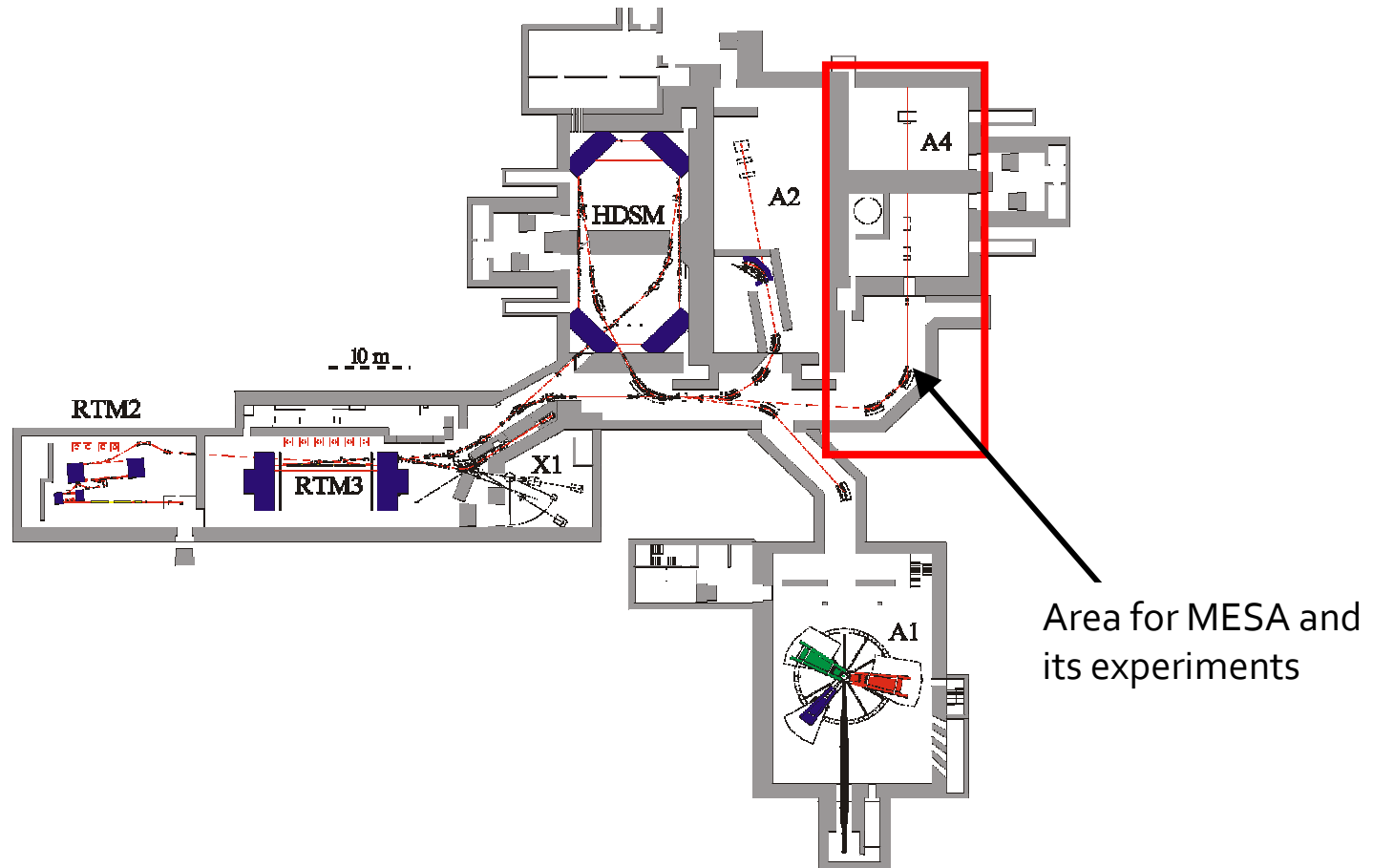
Design Status of the MESA Injector

Robert Heine

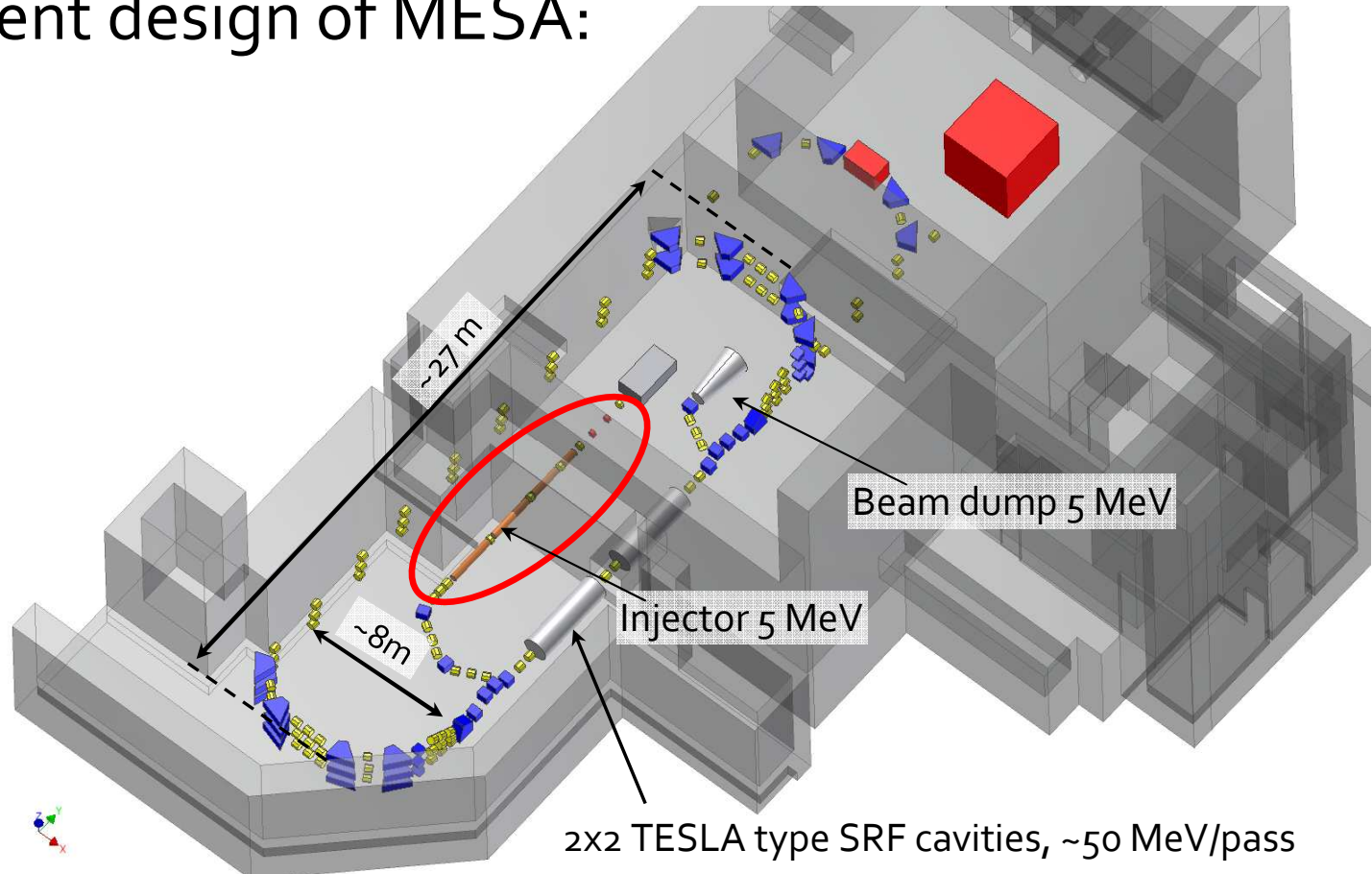
on behalf of MESA-CARE

- Motivation: MESA
- MAMI-ILAC
- Injectors for MESA
- Summary

Floor Plan of MAMI and Experimental Halls



Current design of MESA:



Lattice design by R. Eichorn

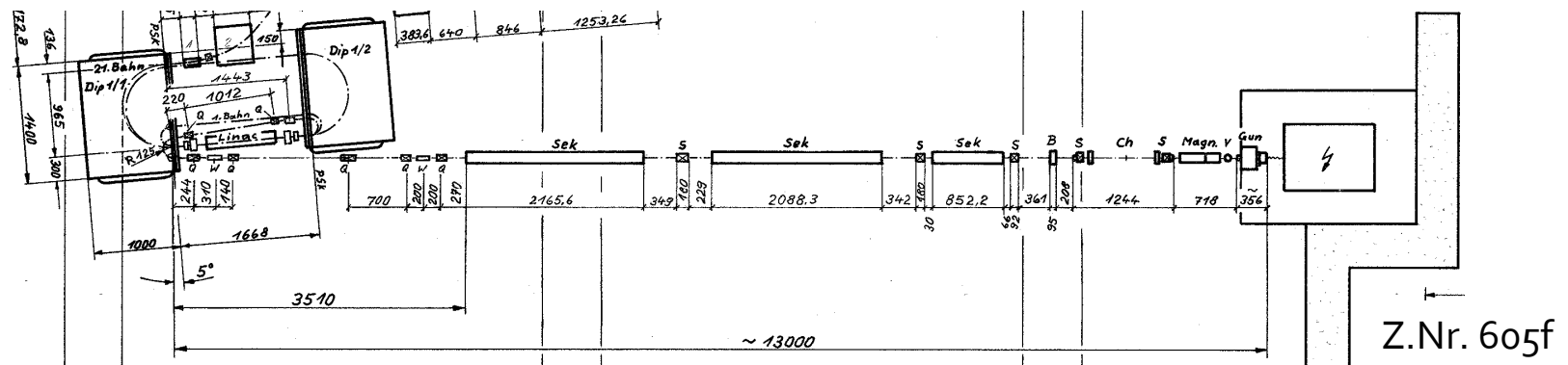
- Take MAMI-ILAC as a blue print for MESA injector
- scale it to 1.3 GHz
- aim at comparable ΔE and $\Delta \psi$
- at $E_{\text{end}} = 5 \text{ MeV}$, $I_{\text{max}} = 10 \text{ mA}$

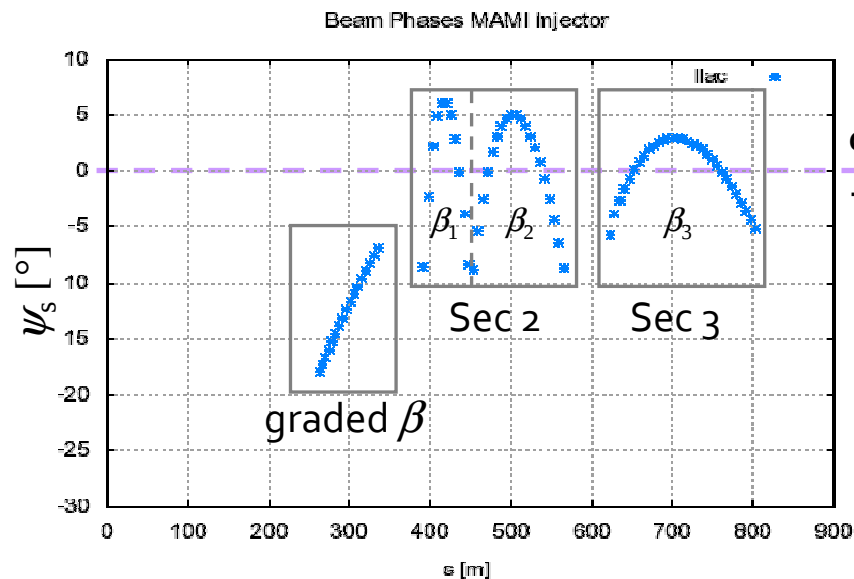
- 100 keV DC source ($\Delta E=2.5\text{eV}$, $I_b=100\mu\text{A}$, $\varepsilon=1\pi\text{ mm mrad}$)
- Chopper system
- Fundamental buncher
- (2nd harmonic buncher to capture more beam from photo gun)
- Section 1: $\beta=0.548\text{--}0.876$, 17 AC (100–550 keV)
- Section 2: $\beta_1=0.9176$, 11 AC; $\beta_2=0.966$, 20 AC
- Section 3: $\beta_3=0.987$, 31 AC
- $E_{\text{end}}=3.5\text{ MeV}$, $\Delta E=4\text{ keV}$ ($\Delta E/E=0.06\%$), $\Delta\psi=3^\circ$

(MAMI Annual Report 1988/89, p.4)



MAMI Linac 2.45 GHz



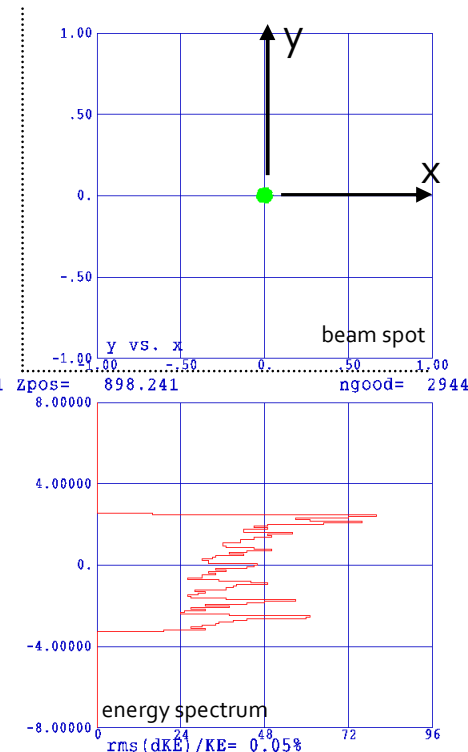
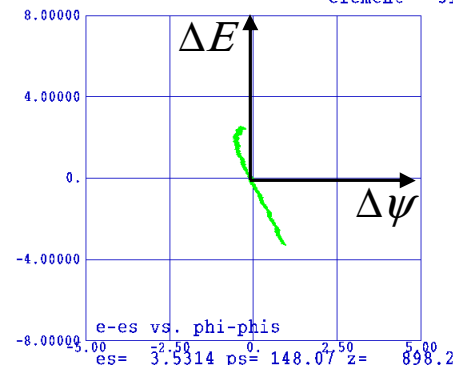
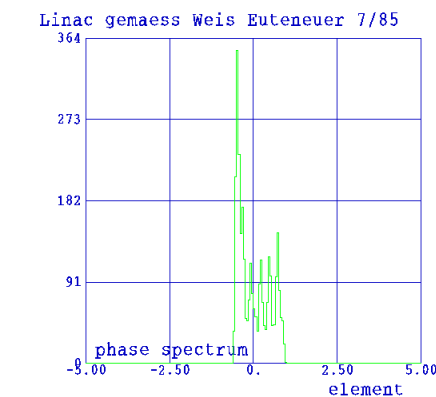


Beam phases taken from T. Weis MAMI 12/84

Simulated rms emittance
growth during acceleration:

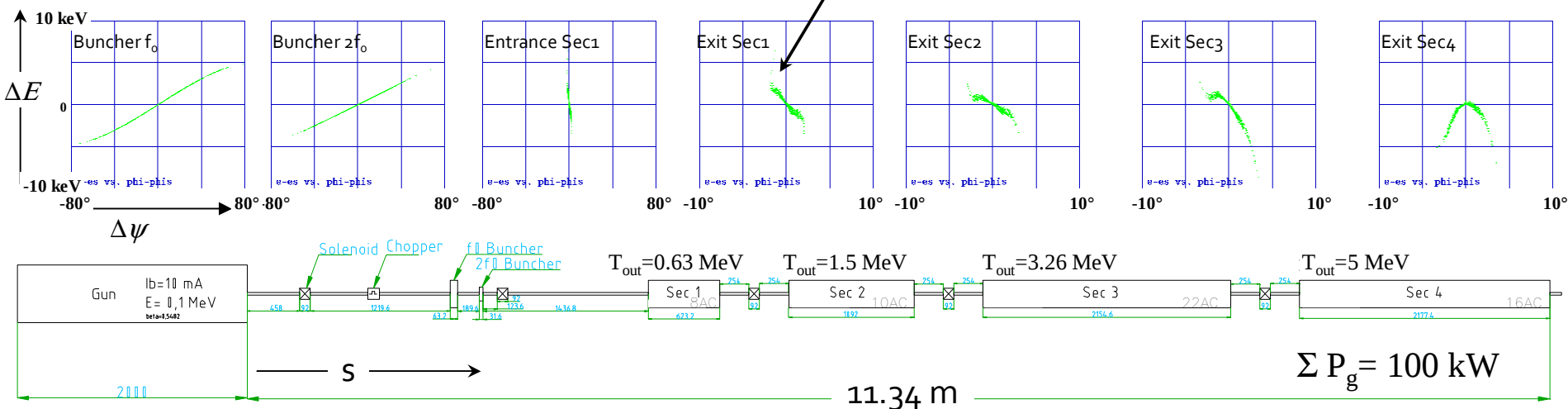
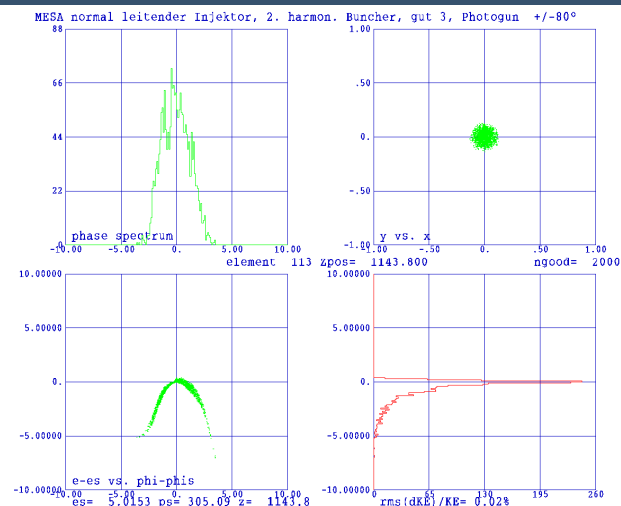
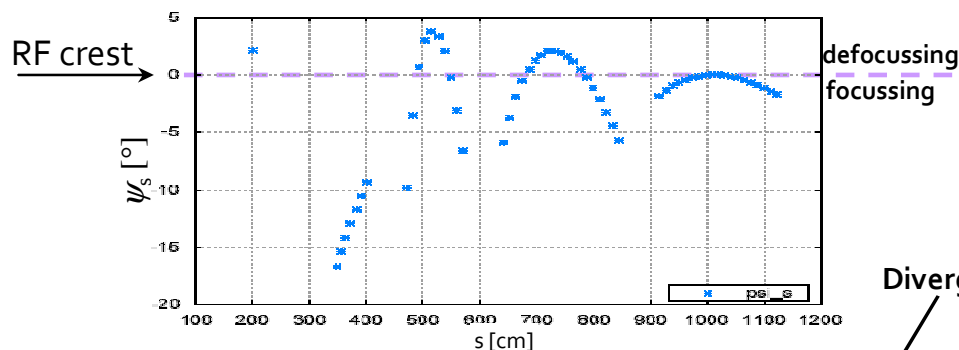
$$\Delta \epsilon_{x,n} = 4,7\%$$

$$\epsilon_{x,rms} = \frac{1}{N} \sqrt{\sum_{i=1}^N x_i^2 \sum_{i=1}^N x_i'^2 - \left(\sum_{i=1}^N x_i^2 x_i'^2 \right)^2} = \frac{\epsilon_{x,n,rms}}{1000\beta\gamma}$$

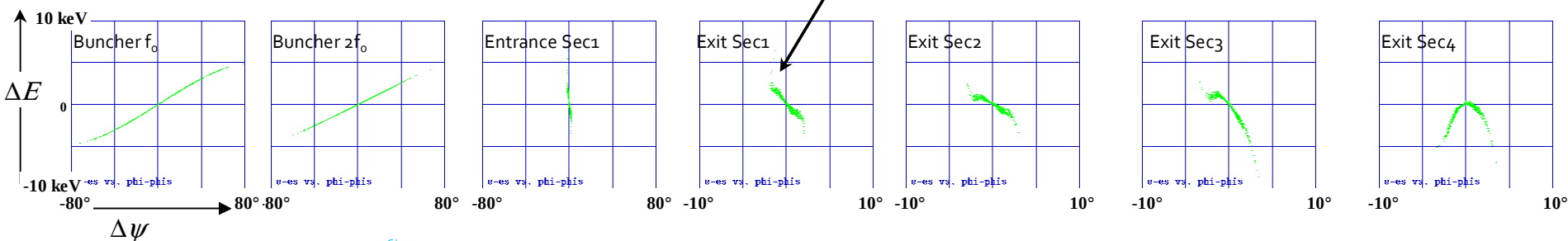
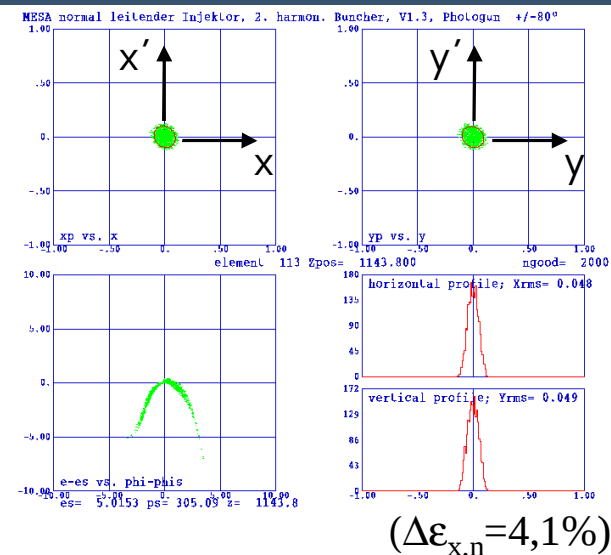
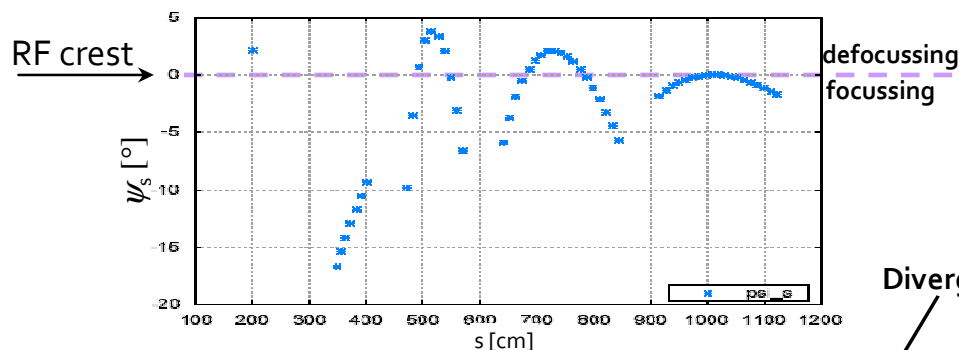


Injectors for MESA

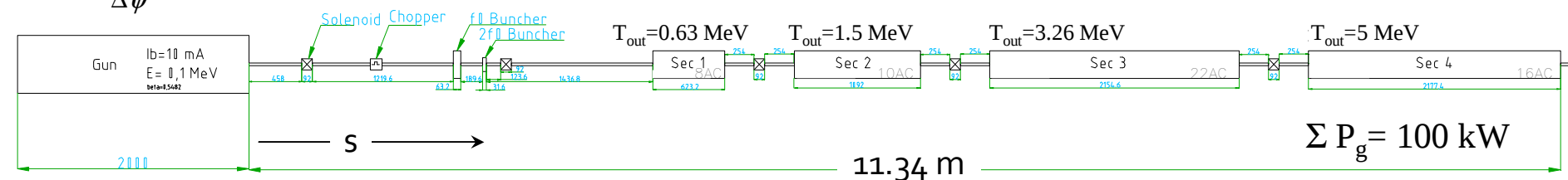
- Section 1: $\beta = 0.548 - 0.896$ (graded β)
- Section 2: $\beta = 0.946 = (\beta_{\text{out}} - \beta_{\text{in}})/2$
- Section 3: $\beta = 0.983$
- Section 4: $\beta = 0.993$



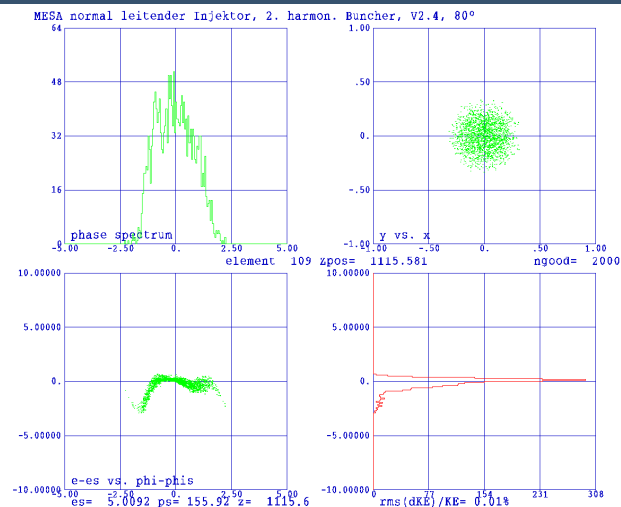
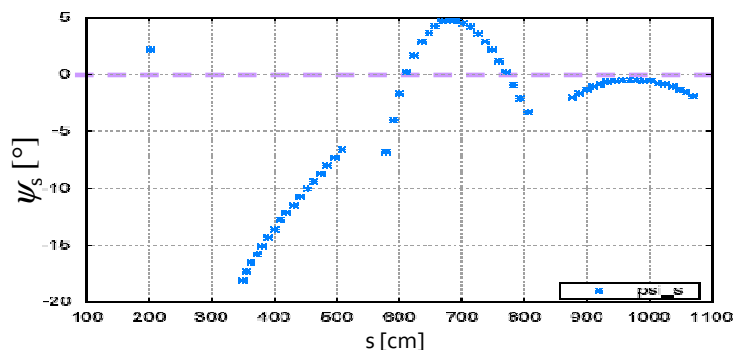
- Section 1: $\beta = 0.548 - 0.896$ (graded β)
- Section 2: $\beta = 0.946 = (\beta_{\text{out}} - \beta_{\text{in}})/2$
- Section 3: $\beta = 0.983$
- Section 4: $\beta = 0.993$



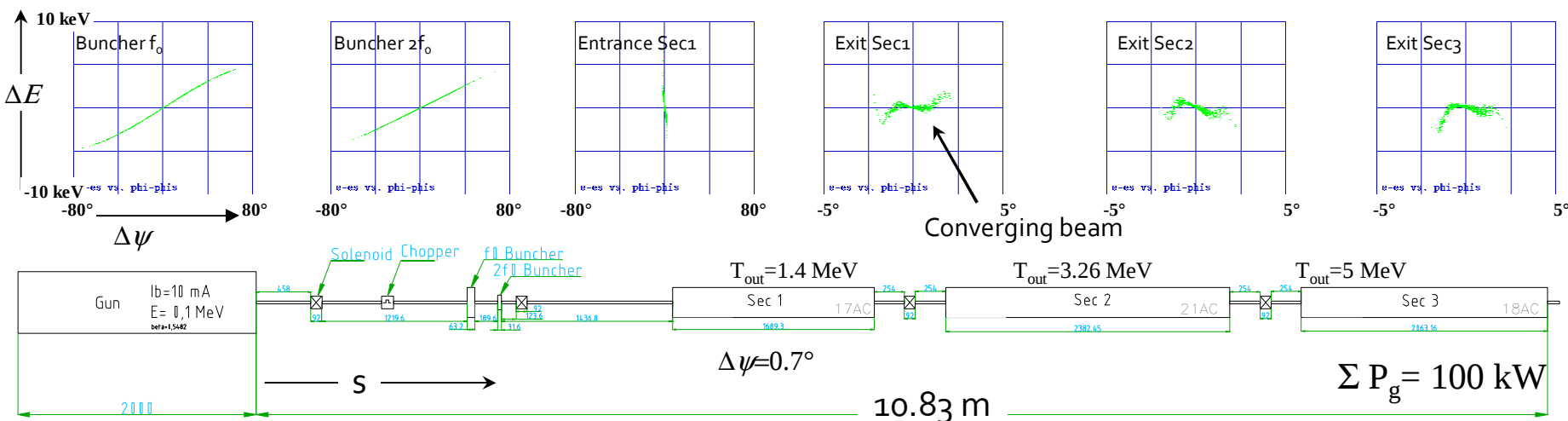
$T = 5.02 \text{ MeV}$ $\Delta\psi_{100\%} < \pm 3.6^\circ$ $\Delta T/T_{\text{rms}} = 0.02\%$



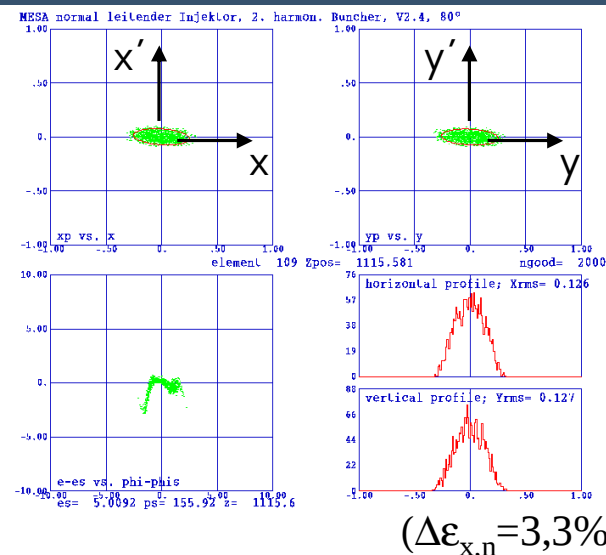
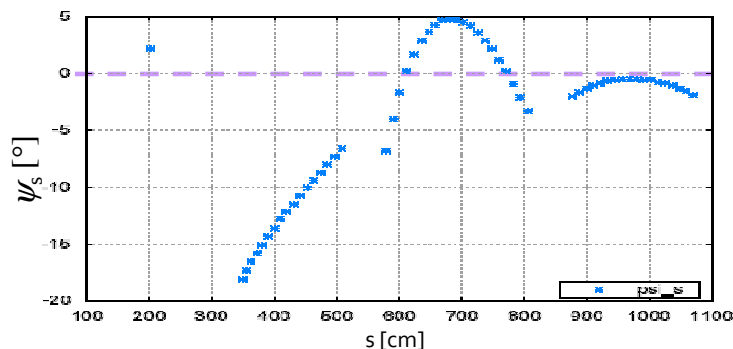
- Section 1: $\beta = 0.548 - 0.964$ (graded β)
- Section 2: $\beta = 0.982$
- Section 3: $\beta = 0.995$



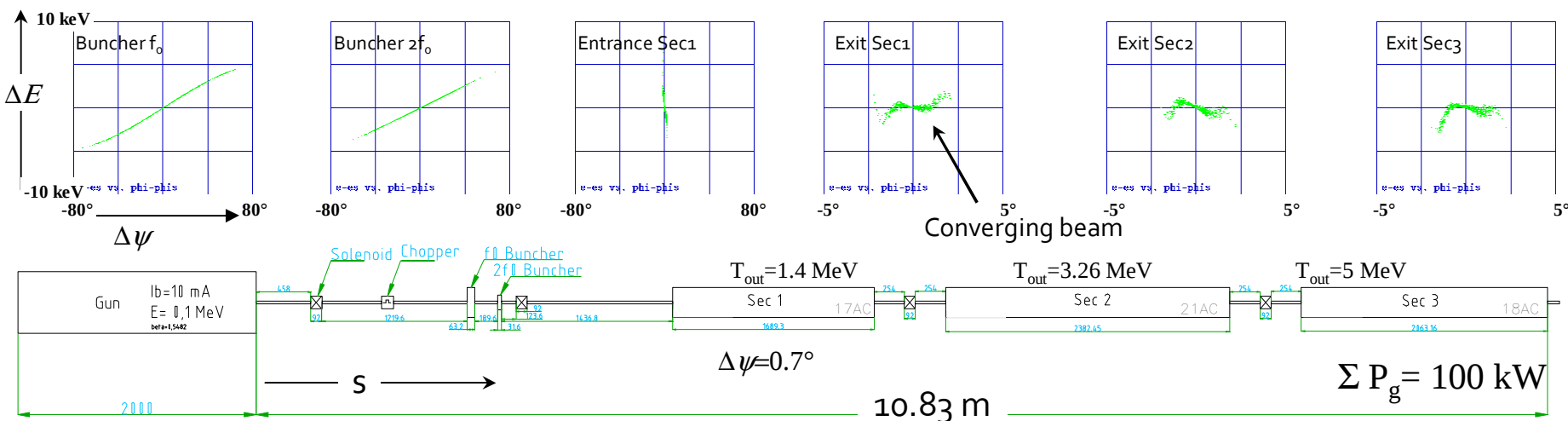
$T = 5.01 \text{ MeV}$ $\Delta\psi_{100\%} < \pm 2.3^\circ$ $\Delta T/T_{\text{rms}} = 0.01\%$



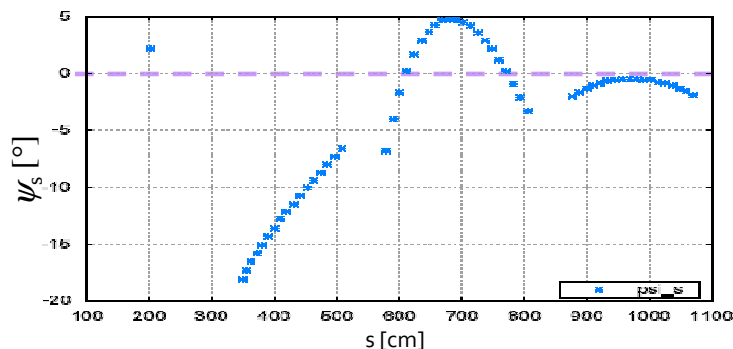
- Section 1: $\beta = 0.548 - 0.964$ (graded β)
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$T=5.01 \text{ MeV}$ $\Delta\psi_{100\%} < \pm 2.3^\circ$ $\Delta T/T_{\text{rms}}=0.01\%$

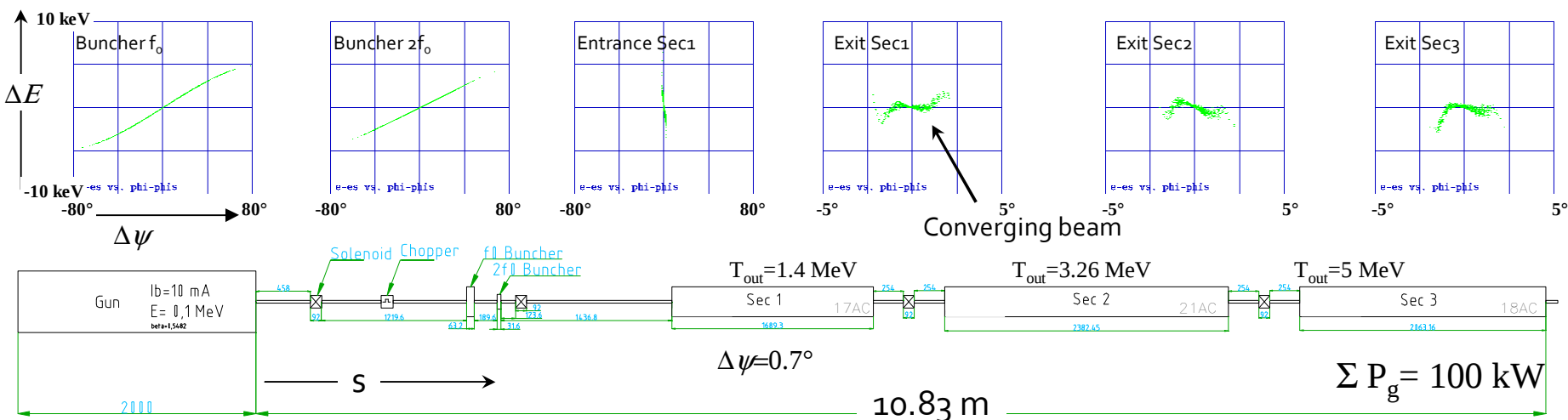


- Section 1: $\beta = 0.548 - 0.964$ (graded β)
- Section 2: $\beta = 0.982$
- Section 3: $\beta = 0.995$

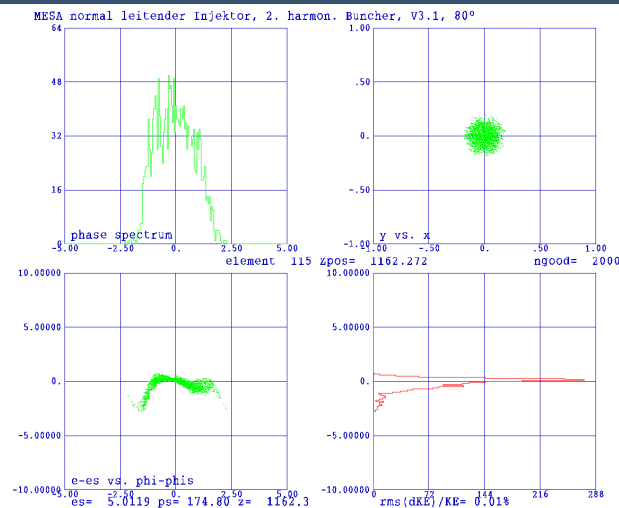
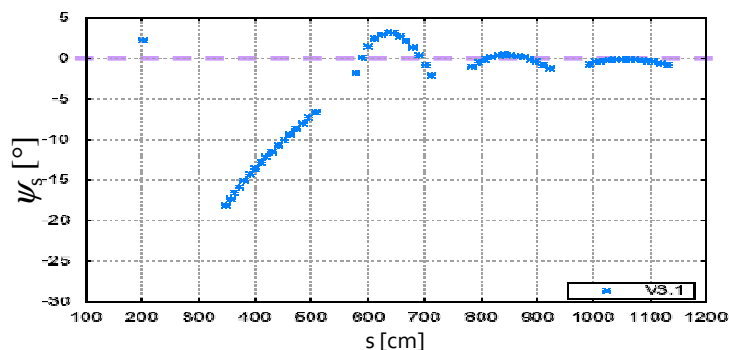


- Acceptable solution
- $\Delta\psi$ can be minimised by running Sec 2&3 at a different phase, but on cost of $\Delta T/T$
- Injector is rather long
- RF demands are high

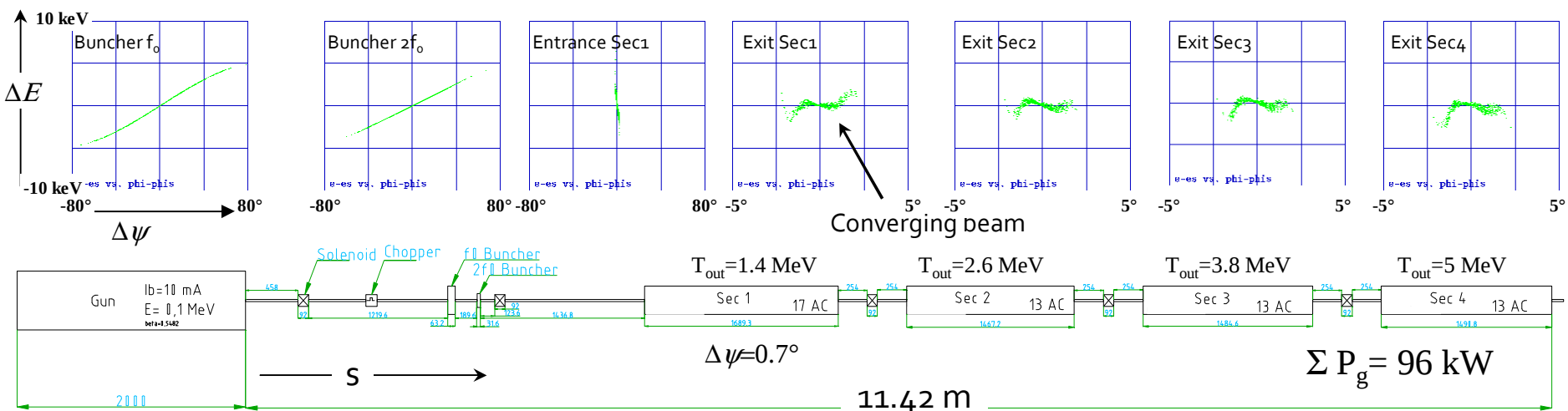
$T = 5.01 \text{ MeV}$ $\Delta\psi_{100\%} < \pm 2.3^\circ$ $\Delta T/T_{\text{rms}} = 0.01\%$



- Section 1: $\beta = 0.548 - 0.964$ (graded β)
- Section 2: $\beta = 0.979$
- Section 3: $\beta = 0.99$
- Section 4: $\beta = 0.995$

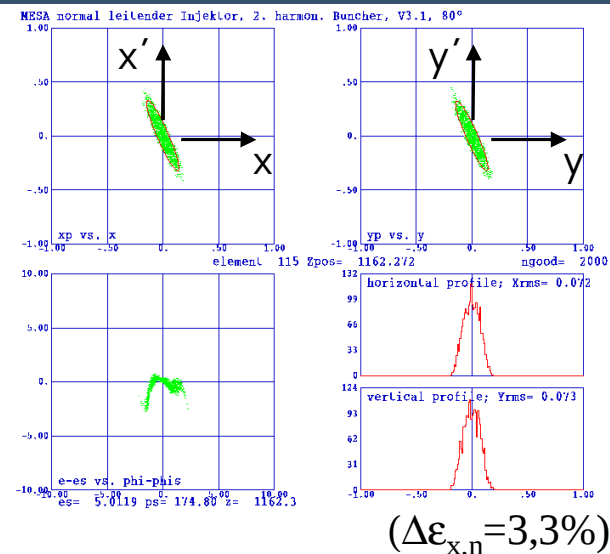
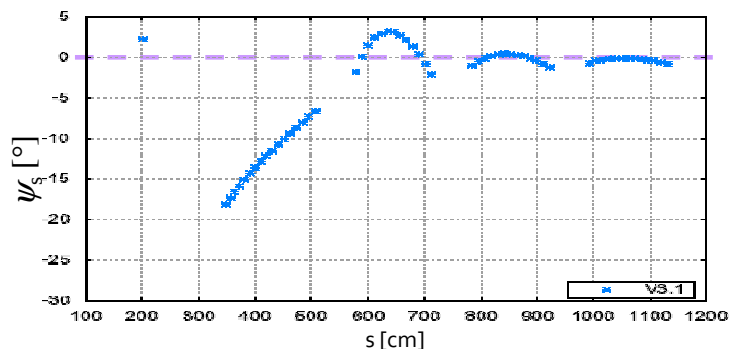


$T = 5.01 \text{ MeV}$ $\Delta\psi_{100\%} < \pm 2.3^\circ$ $\Delta T/T_{\text{rms}} = 0.01\%$

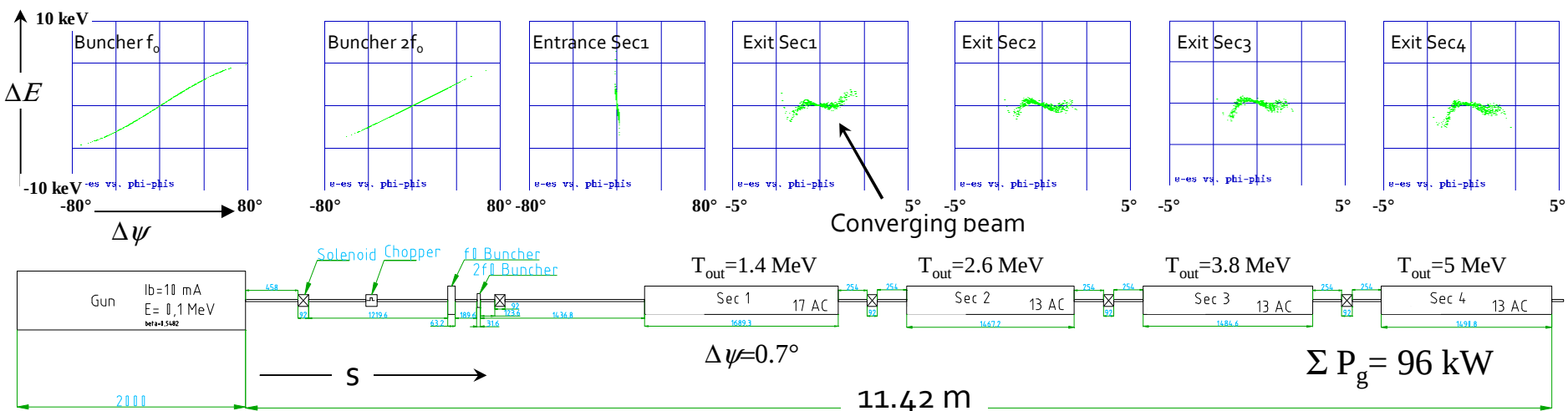


Normal Conducting Injector V3

- Section 1: $\beta = 0.548 - 0.964$ (graded β)
- Section 2: $\beta = 0.979$
- Section 3: $\beta = 0.99$
- Section 4: $\beta = 0.995$

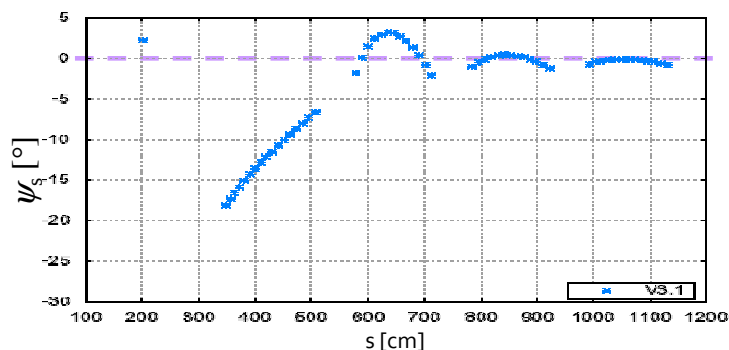


$T = 5.01 \text{ MeV}$ $\Delta\psi_{100\%} < \pm 2.3^\circ$ $\Delta T/T_{\text{rms}} = 0.01\%$

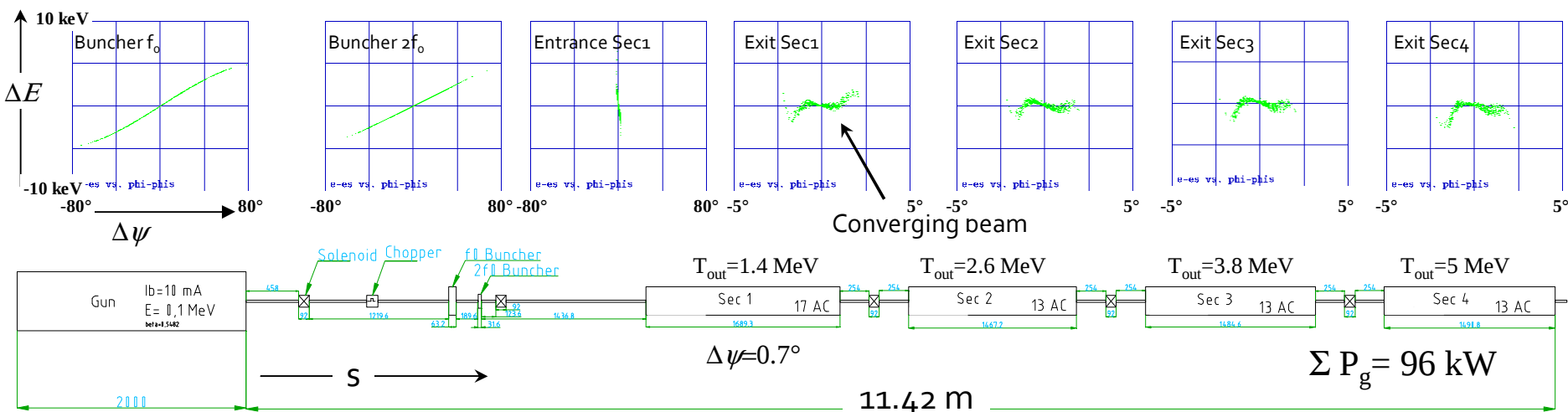


- Section 1: $\beta = 0.548 - 0.964$ (graded β)
- Section 2: $\beta = 0.979$
- Section 3: $\beta = 0.99$
- Section 4: $\beta = 0.995$

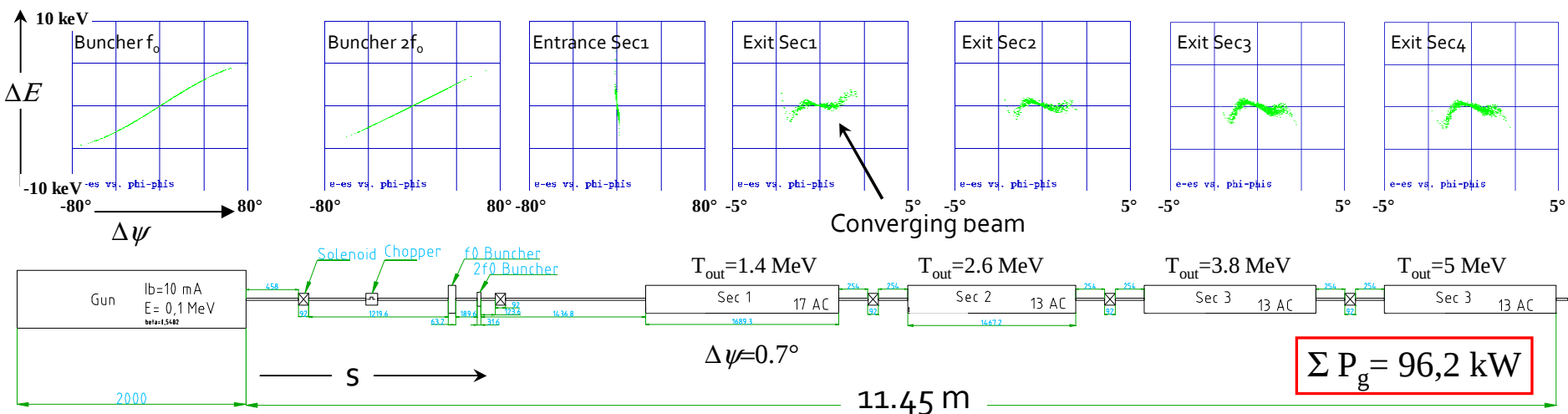
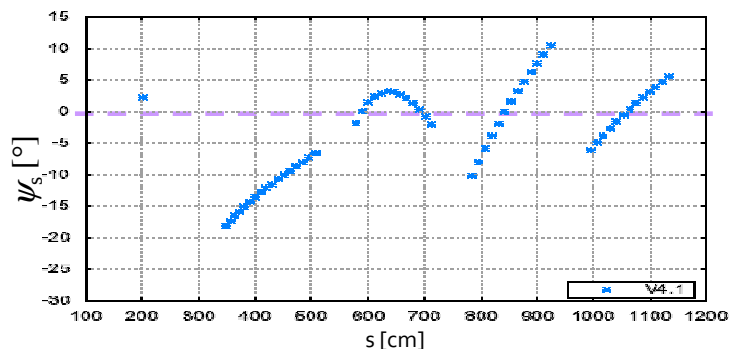
- Solution comparable to V2
- Less RF demands (<30kW/section)
- Injector is longer



$T = 5.01 \text{ MeV}$ $\Delta\psi_{100\%} < \pm 2.3^\circ$ $\Delta T/T_{\text{rms}} = 0.01\%$

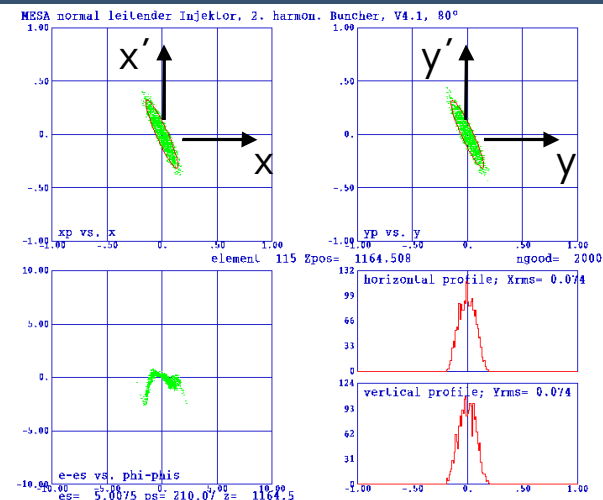
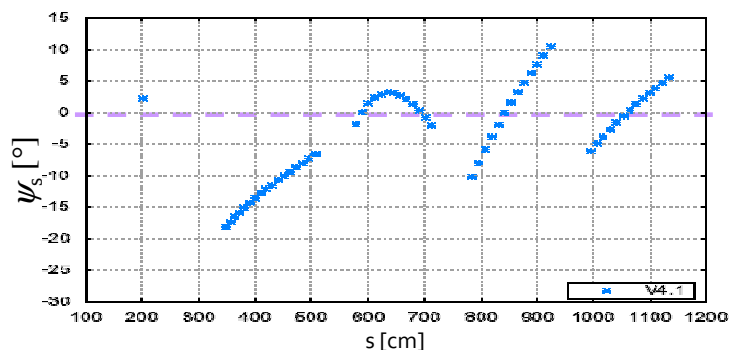


- Section 1: $\beta = 0.548 - 0.964$ (graded β)
- Section 2: $\beta = 0.979$
- Section 3: $\beta = 1$
- Section 4: $\beta = 1$



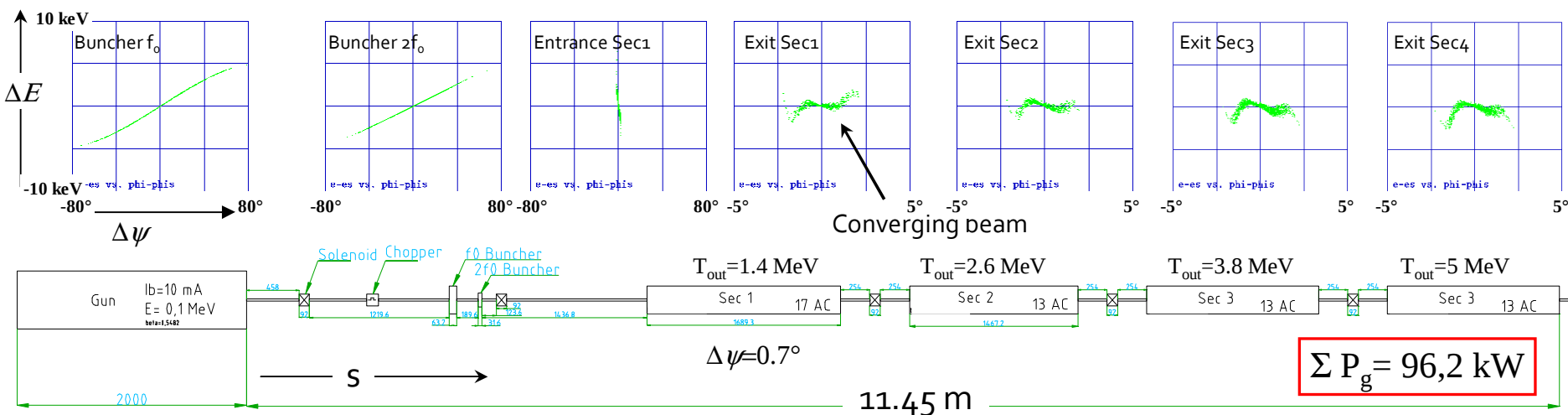
Normal Conducting Injector V4

- Section 1: $\beta = 0.548 - 0.964$ (graded β)
- Section 2: $\beta = 0.979$
- Section 3: $\beta = 1$
- Section 4: $\beta = 1$



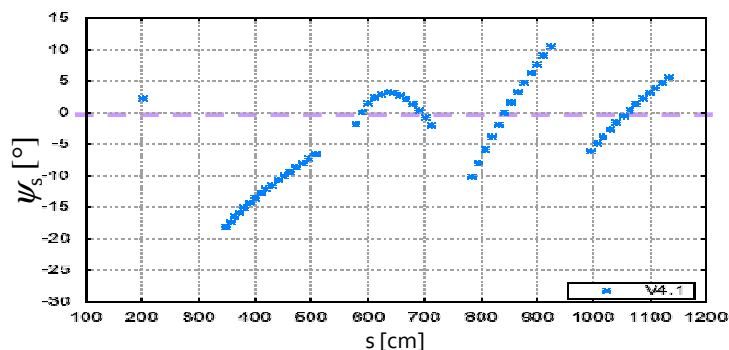
$$(\Delta\epsilon_{x,n}=3,3\%)$$

$$T=5.01 \text{ MeV} \quad \Delta\psi_{100\%} < \pm 2.3^\circ \quad \Delta T/T_{\text{rms}}=0.01\%$$

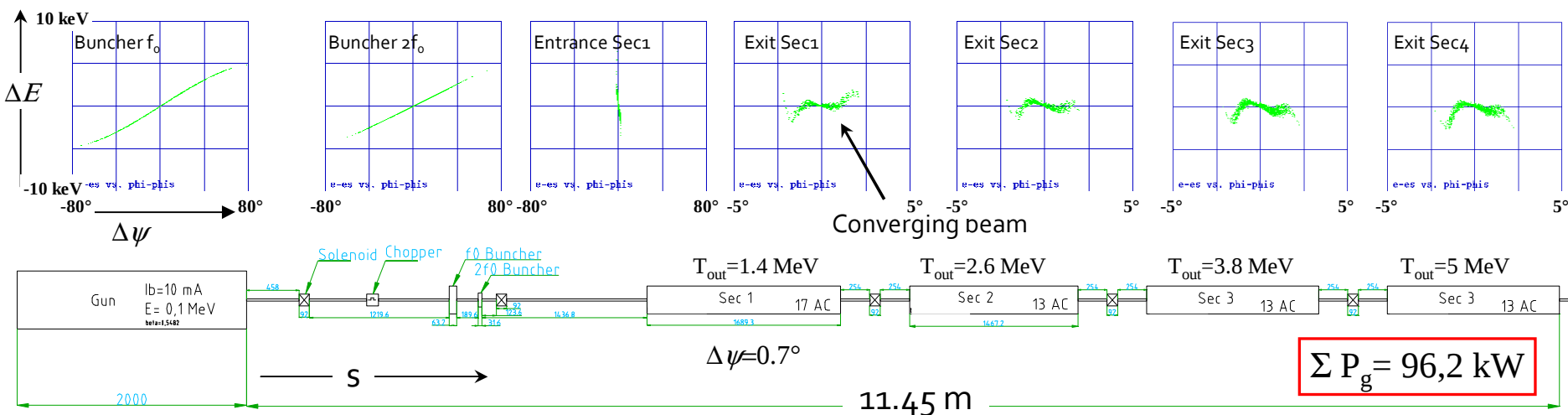


- Section 1: $\beta = 0.548 - 0.964$ (graded β)
- Section 2: $\beta = 0.979$
- Section 3: $\beta = 1$
- Section 4: $\beta = 1$

- Solution nearly identical to V3
- Less RF demands (<30kW/section)
- Section 3 & 4 are identical
- Injector is longer



$T = 5.01 \text{ MeV}$ $\Delta\psi_{100\%} < \pm 2.3^\circ$ $\Delta T/T_{\text{rms}} = 0.01\%$





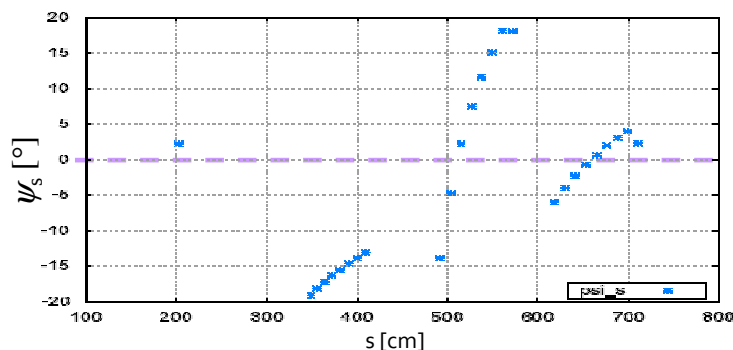
Source: HZB Homepage

π -mode, $E_{CW} < 20$ MV/m, $\beta = 1$

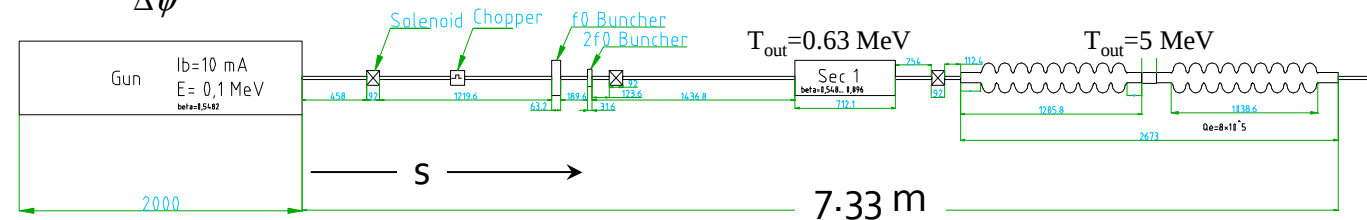
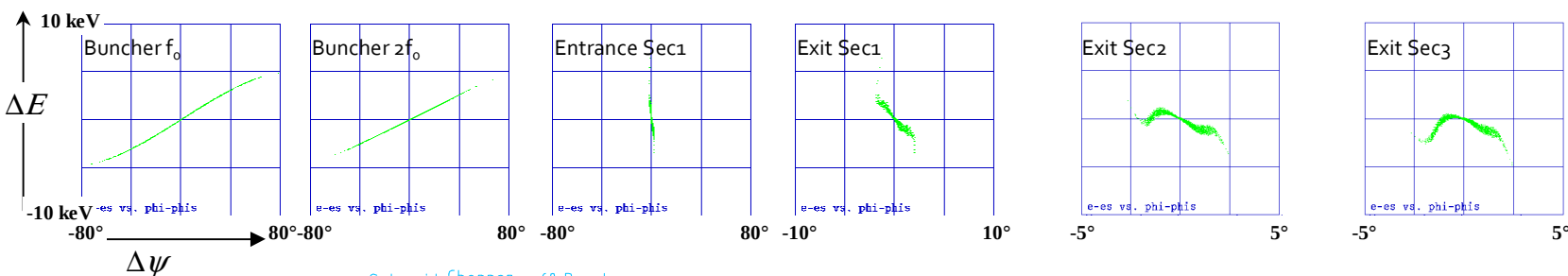
$R/Q = 518 \Omega$
 $Q_0 > 5 \cdot 10^9$
 $TT \approx 0.73$

- Section 1: $\beta = 0.548 - 0.896$ (graded β)
- Section 2: $\beta = 1$
- Section 3: $\beta = 1$

Hybrid injector stands for the combination of a normal conducting graded β section with superconducting TESLA sections

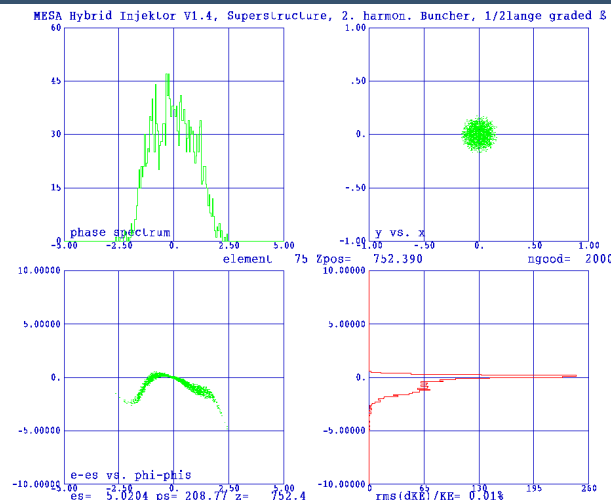
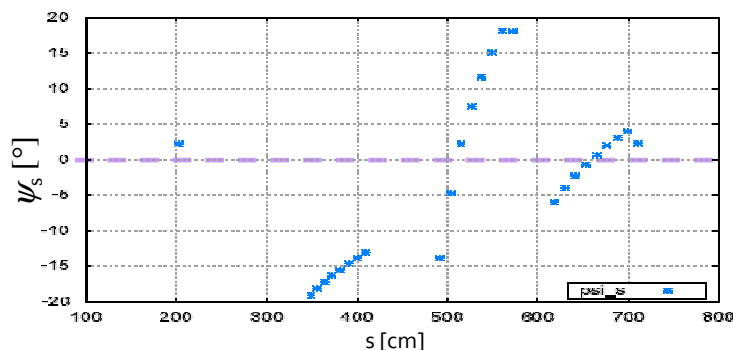


$T = 5.02 \text{ MeV}$ $\Delta\psi_{\text{rms}} < \pm 2.6^\circ$ $\Delta T/T_{\text{rms}} = 0.01\%$

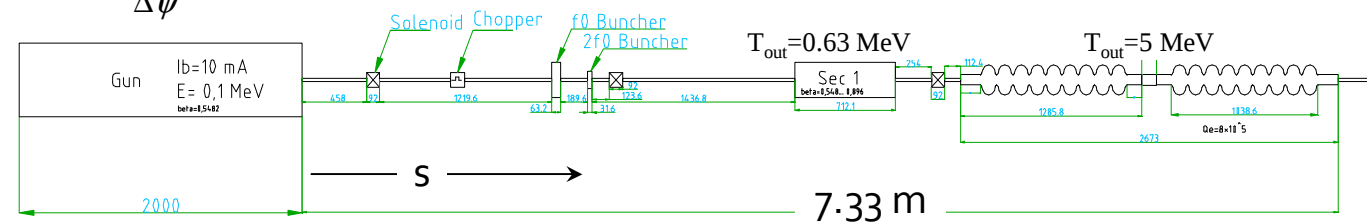
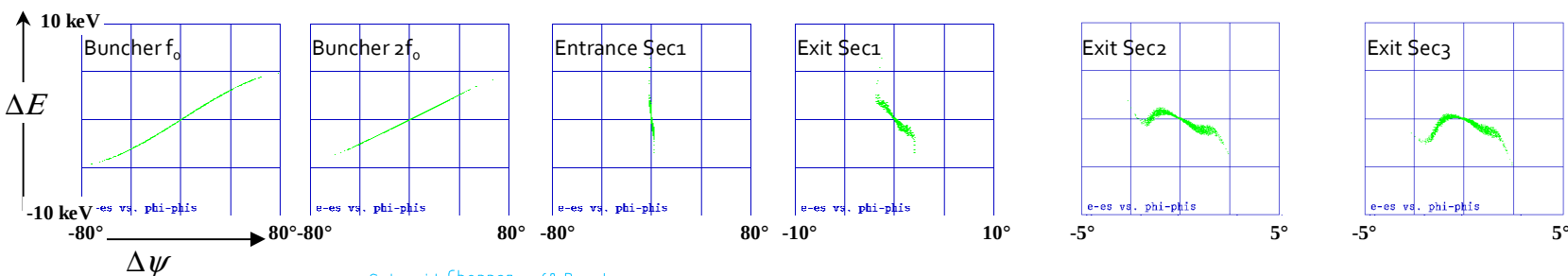


$E = 2.85 \text{ MV/m}$ $P_c = 3.4 \text{ W}$
 $\Sigma P_g = 71 \text{ kW}$

- Section 1: $\beta = 0.548 - 0.896$ (graded β)
- Section 2: $\beta = 1$
- Section 3: $\beta = 1$

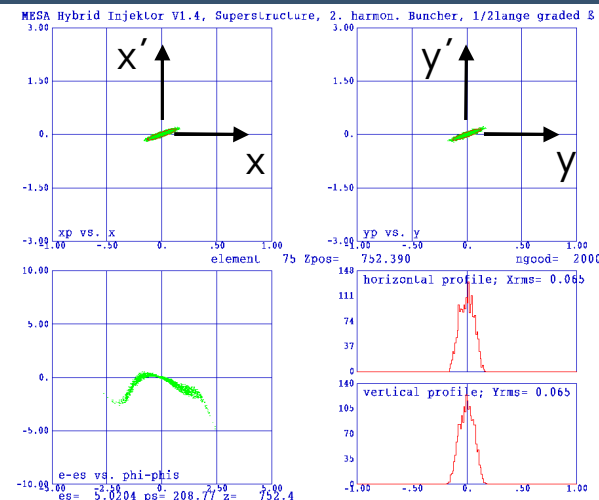
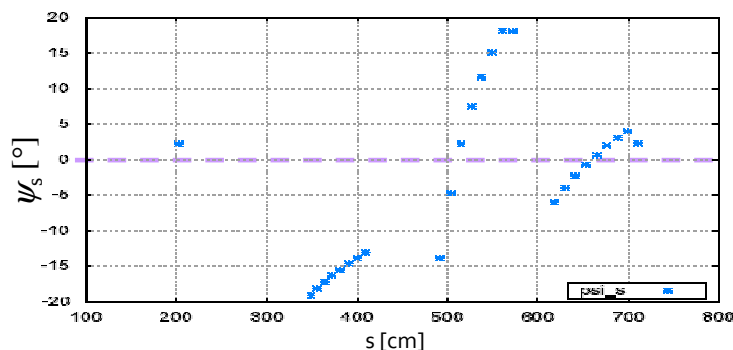


$T=5.02 \text{ MeV}$ $\Delta\psi_{\text{rms}} < \pm 2.6^\circ$ $\Delta T/T_{\text{rms}} = 0.01\%$



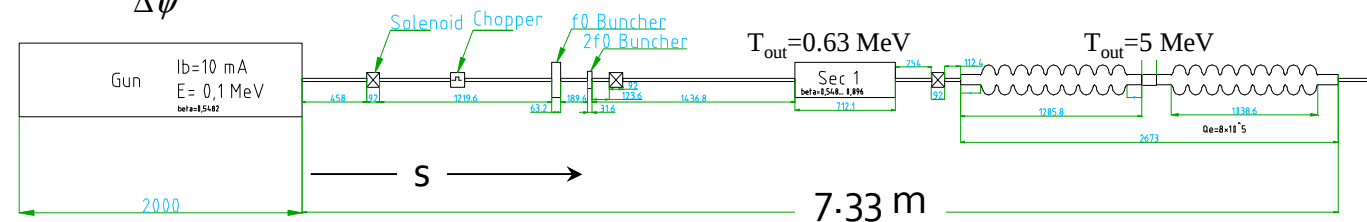
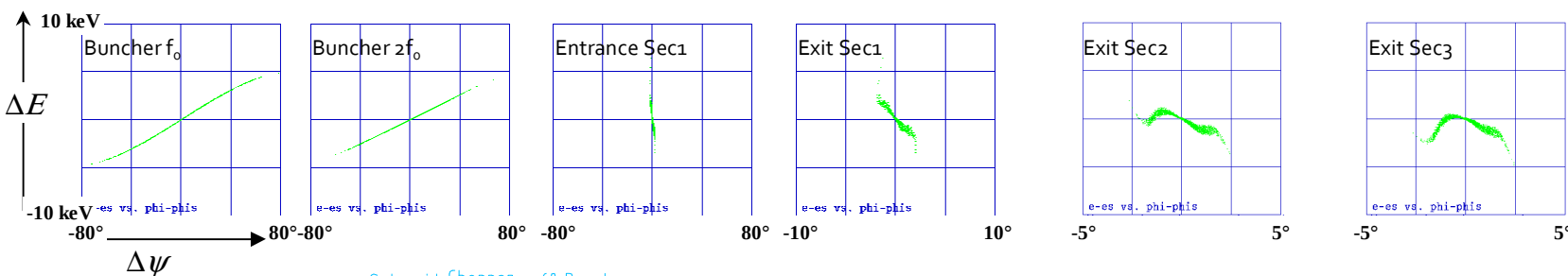
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- Section 1: $\beta = 0.548 - 0.896$ (graded β)
- Section 2: $\beta = 1$
- Section 3: $\beta = 1$



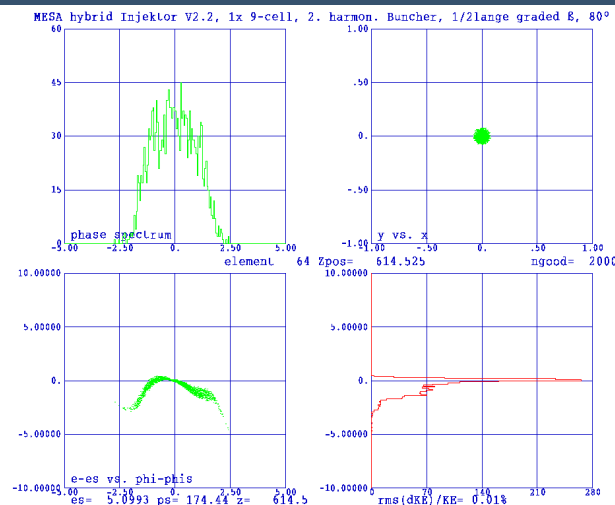
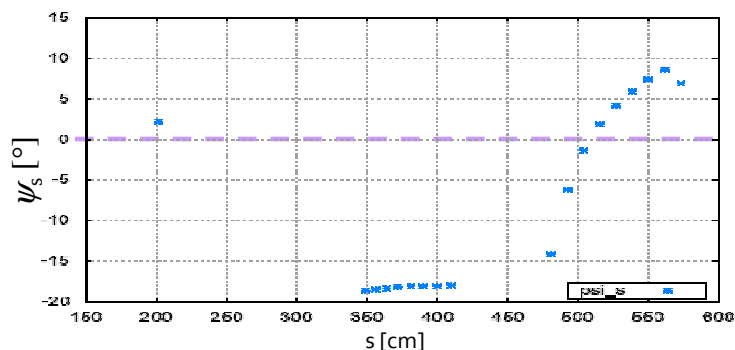
$$(\Delta\epsilon_{x,n} = 1.6\%)$$

$$T = 5.02 \text{ MeV} \quad \Delta\psi_{\text{rms}} < \pm 2.6^\circ \quad \Delta T/T_{\text{rms}} = 0.01\%$$

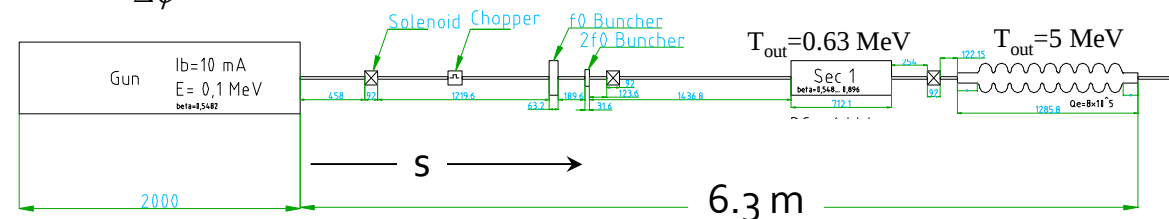
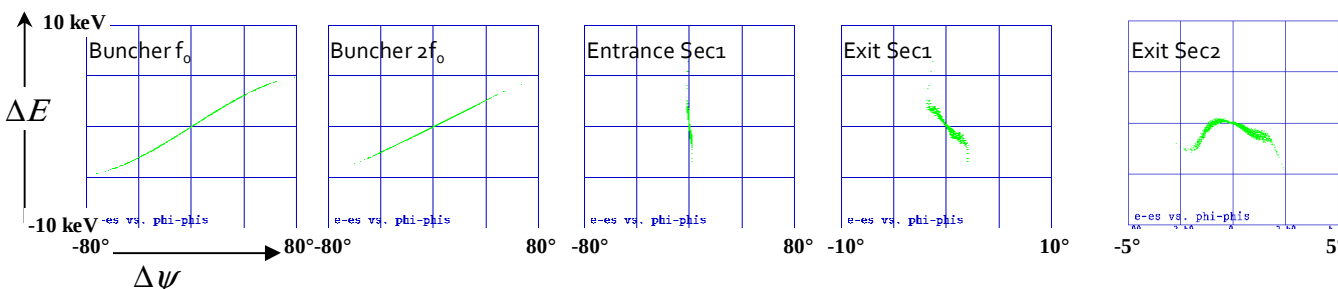


$$E = 2.85 \text{ MV/m} \quad P_c = 3.4 \text{ W} \\ \Sigma P_g = 71 \text{ kW}$$

- Section 1: $\beta = 0.548 - 0.896$ (graded β)
- Section 2: $\beta = 1$

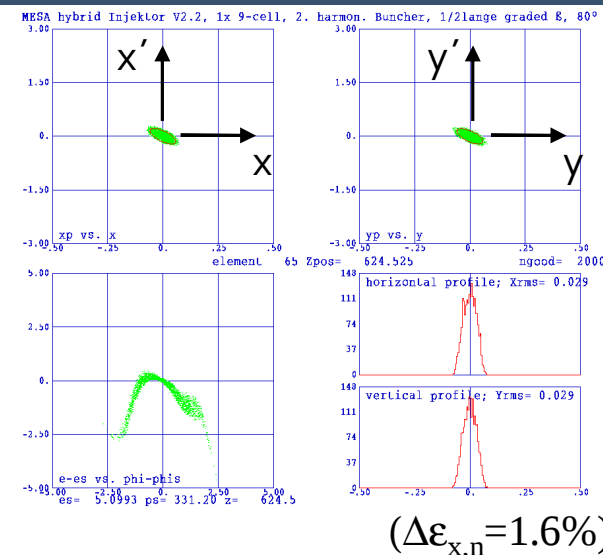
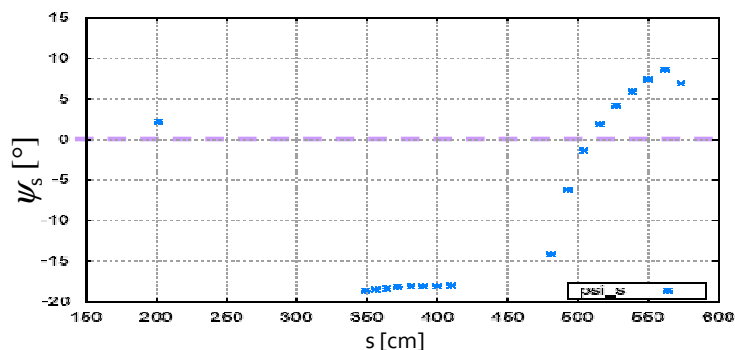


$T = 5.1 \text{ MeV}$ $\Delta\psi_{100\%} < \pm 2.6^\circ$ $\Delta T/T_{\text{rms}} = 0.01\%$

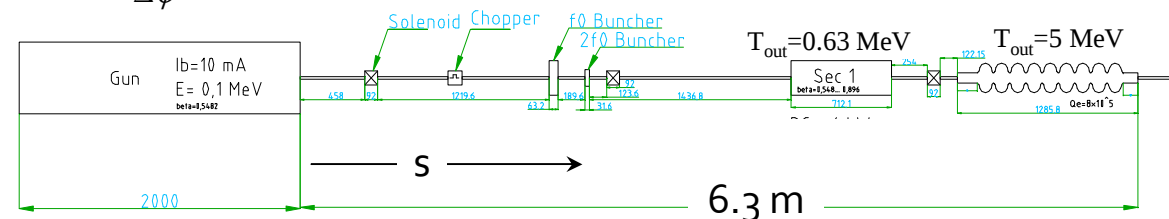
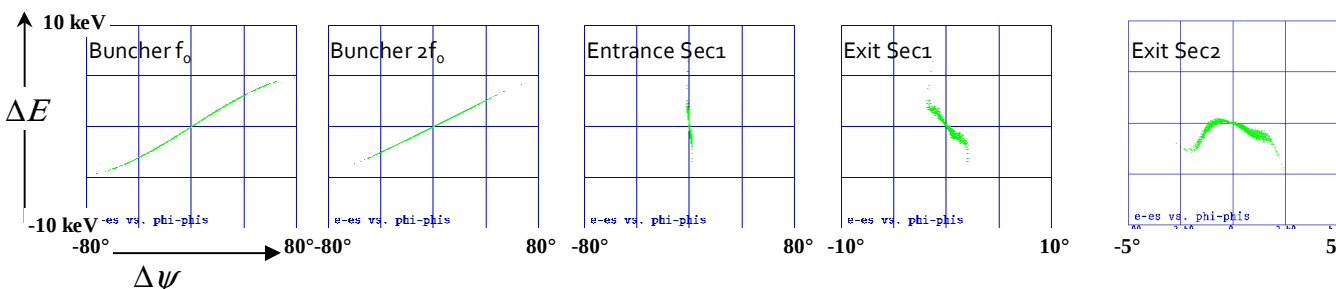


$E = 5.75 \text{ MV/m}$ $P_c = 6.9 \text{ W}$
 $\Sigma P_g = 71.8 \text{ kW}$

- Section 1: $\beta = 0.548 - 0.896$ (graded β)
- Section 2: $\beta = 1$

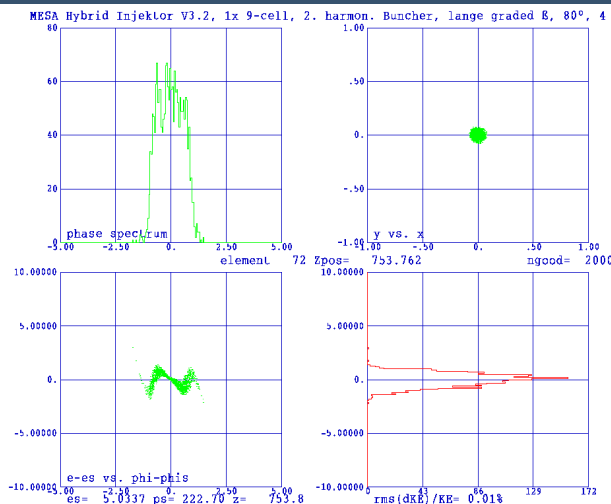
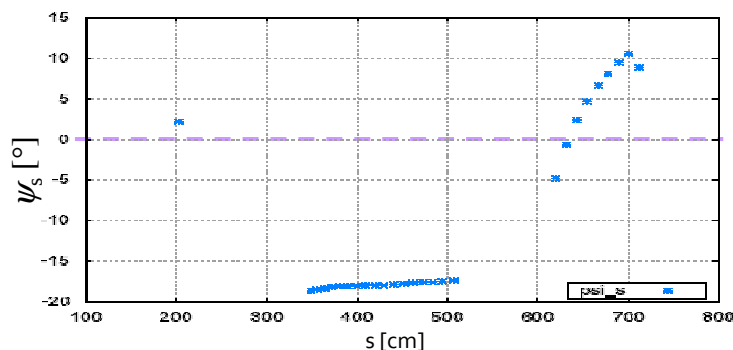


$T=5.1 \text{ MeV}$ $\Delta\psi_{100\%} < \pm 2.6^\circ$ $\Delta T/T_{\text{rms}} = 0.01\%$

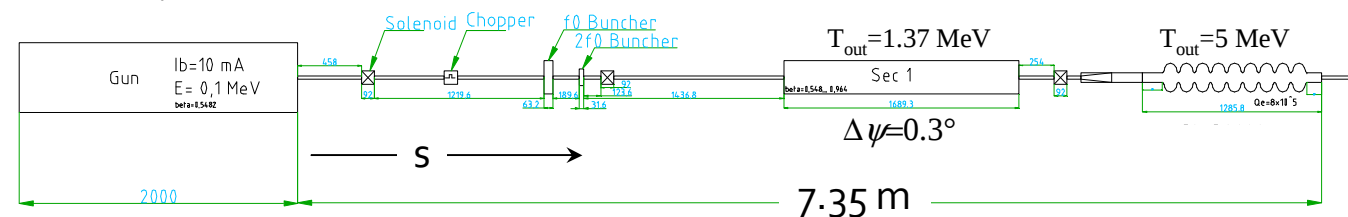
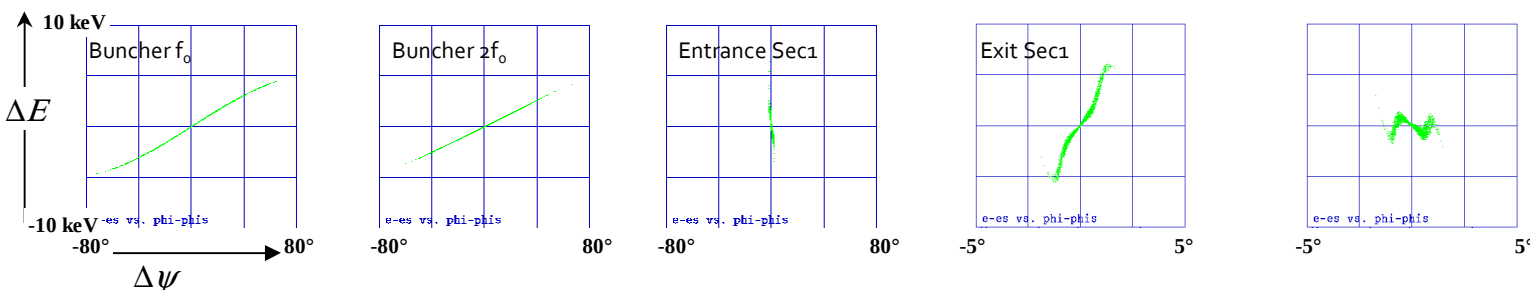


$E = 5.75 \text{ MV/m}$ $P_c = 6.9 \text{ W}$
 $\Sigma P_g = 71.8 \text{ kW}$

- Section 1: $\beta = 0.548 - 0.964$ (graded β)
- Section 2: $\beta = 1$

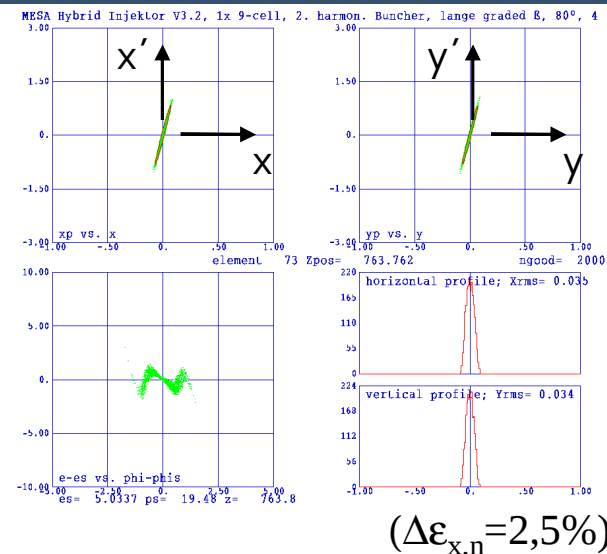
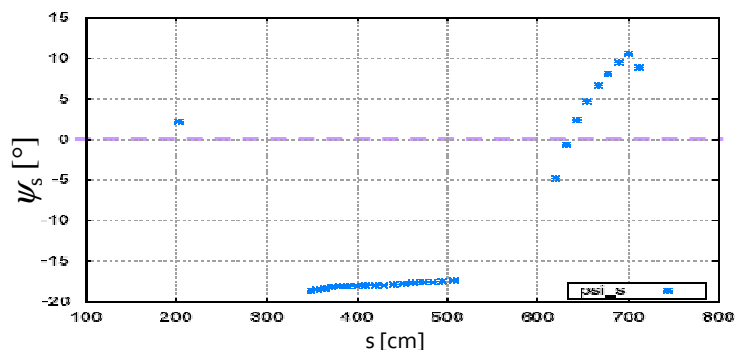


$T=5.03 \text{ MeV}$ $\Delta\psi_{100\%} < \pm 1.7^\circ$ $\Delta T/T_{\text{rms}} = 0.01\%$

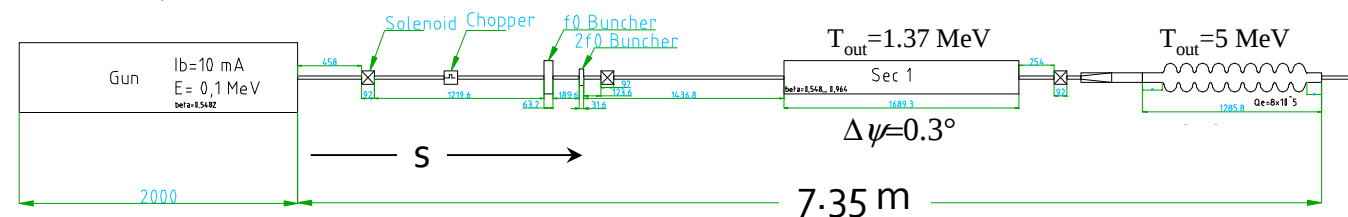
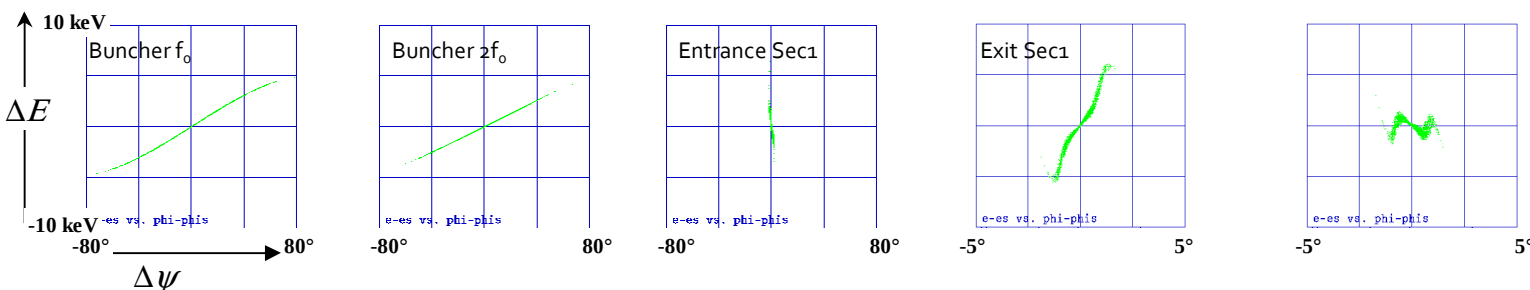


$E = 4.65 \text{ MV/m}$ $P_c = 4.5 \text{ W}$
 $\Sigma P_g = 74.2 \text{ kW}$

- Section 1: $\beta = 0.548 - 0.964$ (graded β)
- Section 2: $\beta = 1$



$T = 5.03 \text{ MeV}$ $\Delta\psi_{100\%} < \pm 1.7^\circ$ $\Delta T/T_{\text{rms}} = 0.01\%$

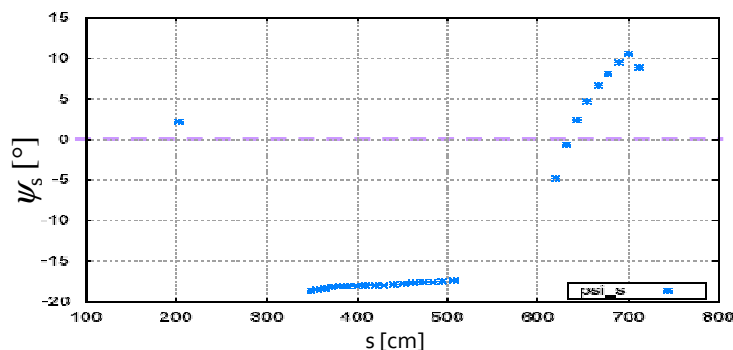


$E = 4.65 \text{ MV/m}$ $P_c = 4.5 \text{ W}$

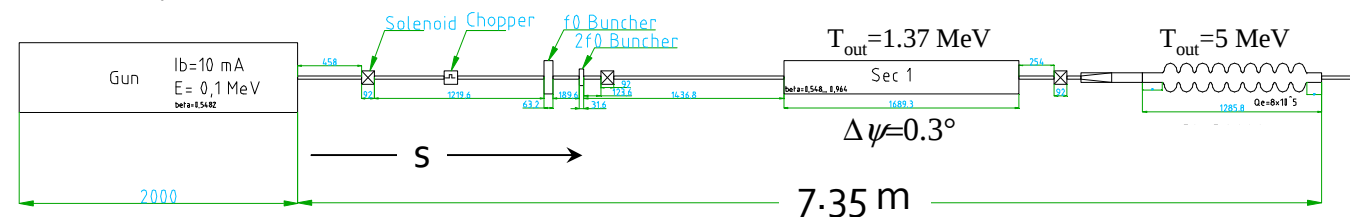
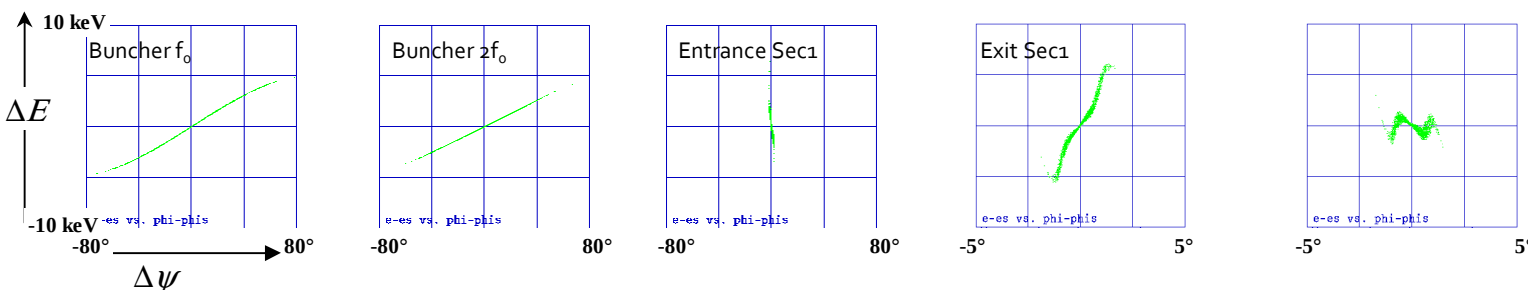
$\Sigma P_g = 74.2 \text{ kW}$

- Section 1: $\beta = 0.548 - 0.964$ (graded β)
- Section 2: $\beta = 1$

- + Solution meets all demands!
- + Injector is compact
- SRF needs more investment cost
- Larger LHe system necessary



$T = 5.03 \text{ MeV}$ $\Delta\psi_{100\%} < \pm 1.7^\circ$ $\Delta T/T_{\text{rms}} = 0.01\%$



$E = 4.65 \text{ MV/m}$ $P_c = 4.5 \text{ W}$

$\Sigma P_g = 74.2 \text{ kW}$

- Several configurations of the MESA injector have been presented
- Two concepts were followed: a completely normal conducting and a hybrid superconducting concept
- Both concepts are competitive
- The hybrid concept gives a smaller long. phase space, is more compact and technologically more interesting
- The normal conducting concept has a slightly larger long. phase space, is more space consuming but based on established technology

Thank you for your kind
attention!