

Extending Bell's Model: How Force Transducer Stiffness Alters Measured Unbinding Forces and Kinetics of Molecular Complexes

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ABSTRACT Forced unbinding of complementary macromolecules such as ligand-receptor complexes can reveal energetic and kinetic details governing physiological processes ranging from cellular adhesion to drug metabolism. Although molecular-level experiments have enabled sampling of individual ligand-receptor complex dissociation events, disparities in measured unbinding force F_R among these methods lead to marked variation in inferred binding energetics and kinetics at equilibrium. These discrepancies are documented for even the ubiquitous ligand-receptor pair, biotin-streptavidin. We investigated these disparities and examined atomic-level unbinding trajectories via steered molecular dynamics simulations, as well as via molecular force spectroscopy experiments on biotin-streptavidin. In addition to the well-known loading rate dependence of F_R predicted by Bell's model, we find that experimentally accessible parameters such as the effective stiffness of the force transducer k can significantly perturb the energy landscape and the apparent unbinding force of the complex for sufficiently stiff force transducers. Additionally, at least 20% variation in unbinding force can be attributed to minute differences in initial atomic positions among energetically and structurally comparable complexes. For force transducers typical of molecular force spectroscopy experiments and atomistic simulations, this energy barrier perturbation results in extrapolated energetic and kinetic parameters of the complex that depend strongly on k . We present a model that explicitly includes the effect of k on apparent unbinding force of the ligand-receptor complex, and demonstrate that this correction enables prediction of unbinding distances and dissociation rates that are decoupled from the stiffness of actual or simulated molecular linkers.

INTRODUCTION

Ligand-receptor kinetics and energetics have been measured typically through experimental methods that quantify population-averaged responses (1), but a range of new experiments and simulations enables the probing of individual complexes to explore important variations in binding responses within and among ligand or cell populations (2–4). Biotin-streptavidin is among the strongest known ligand-receptor interactions and, as such, it has been widely studied as a model system (5–14) and utilized in biological experiments (15–23). Despite the ubiquitous application of the biotin-streptavidin complex in biotechnology and biophysics as a molecular glue capable of strong, specific interactions and long binding lifetime, there is considerable disagreement among experiments regarding the actual strength of this complex (24,25). Many studies of the dynamic strength of biotin-streptavidin have been reported, using diverse experimental tools such as optical traps (26), laminar flow chambers (27), electric fields (28), magnetic fields (29), the biomembrane force probe (30), and the atomic force microscope (31–39) to rupture the complex. Although these experimental methods differ from each other in many ways, they all aim to measure the unbinding force F_R of the same molecular system. However, even among experiments at comparable loading rates—a known controlling factor of F_R —the magnitude and rate dependence of F_R can vary widely (24,25), as illustrated in Fig. 1.

The dynamic strength of this complex has also been studied through various computational and analytical methods, such as steered molecular dynamics (40) and Langevin dynamics (41).

Accurate measurements of F_R are necessary if experiments and simulations are to provide quantitative value to chemo-mechanical imaging of cell surfaces (42,43), biophysical studies of unbinding trajectories (4), and prediction of binding kinetics (42). Bell's model of specific adhesion under applied force (3,44,45) is commonly applied to such experiments to extract kinetic and energetic binding constants. For a monotonically increasing applied force, an adaptation of this model relates the unbinding force to experimental, kinetic, and energetic parameters as

$$F_R = \frac{k_B T}{x_b} \ln \frac{F' x_b}{k_B T k_{\text{off}}}, \quad (1)$$

where k_B is Boltzmann's constant, T is absolute temperature, x_b is the distance between the bound state, and the energetic maximum, $F' = kv$ is the loading rate (where k is the stiffness of the force transducer and v is the velocity), and k_{off} is the kinetic rate of binding dissociation at equilibrium. From forced dissociation of molecules far from equilibrium, the extrapolated value of $\ln(F')$ at $F_R = 0$ and the slope of F_R versus $\ln(F')$ are critical for estimating both the kinetic (k_{off}) and energetic (x_b) parameters of the complex at equilibrium. To obtain accurate estimates of k_{off} and x_b , it is necessary to understand both the bandwidth of such measurements and the extent to which experimental or computational parameters perturb F_R .

To the best of our knowledge, we have reviewed all reported studies of the forced unbinding of the biotin-streptavidin

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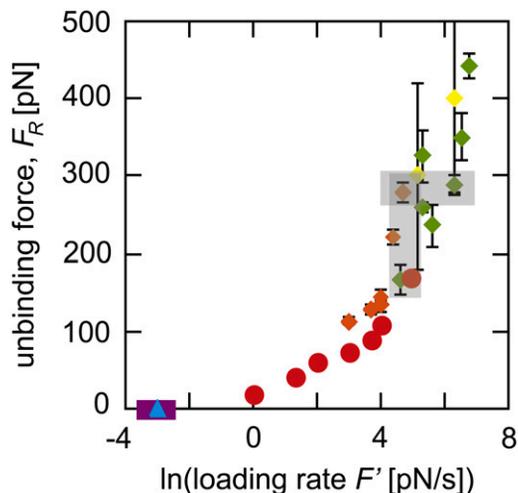


FIGURE 1 Experiments to determine the unbinding force spectrum of biotin-streptavidin have not reached a consensus. Reported data on the unbinding force of biotin-streptavidin is shown as measured by AFM MFS (diamonds in green (35–37), orange (32), and yellow (38)), electric fields (blue triangles (28)), magnetic fields (purple squares (29), points overlap), and BFP (red circles (30)). Error bars indicating the standard deviation among experimental measurements are shown for all data points, but in some cases are smaller than the symbols. The shaded rectangles highlight measurements at similar loading rates where measured unbinding forces differ by a factor of two and measurements of similar unbinding forces where the loading rate differed by two orders of magnitude.

complex. Experiments in which the loading rate or the unbinding force could not be determined were excluded, and our focus was limited to studies utilizing methods that attempted to apply a monotonically increasing force to the ligand-receptor complex, including applied electric (28) and magnetic (29) fields, the biomembrane force probe (BFP) (30), the atomic force microscope (AFM) (31–39), and optical traps (26), as reviewed by Van Vliet et al. (46). We also excluded studies of slightly different molecules such as immunobiotin or avidin, to eliminate as many extraneous factors as possible.

After applying these criteria, eight experimental studies remained: Breisch et al.'s use of electric fields to apply force (28), Panhorst et al.'s use of magnetic fields (29), Merkel et al.'s use of the BFP (30), and five separate studies using the AFM to conduct molecular force spectroscopy (MFS) (32,35–38). Fig. 1 shows the unbinding or rupture forces F_R reported in these studies as a function of the logarithm of the reported loading rate F' . It appears clear that the reported unbinding force F_R is not a unique function of F' : experiments differing by more than an order of magnitude in F' measured very similar unbinding force distributions, and unbinding forces measured at the same F' differ by as much as 200%. One possible explanation is that discrepancies in reported unbinding forces could arise from subtle differences in experimental technique, such as the type of molecular linker utilized. However, this would not account for results reported by a single research group utilizing the same ex-

perimental approach that do not agree within the reported range of error, such as those of Lo et al. (35–37). Another rationale is that F_R depends not just on loading rate, but also on the entire loading history of the complex; this is plausible yet difficult to quantify (24,25).

In light of these well-established discrepancies among experimental results for a model ligand-receptor complex, we performed new steered molecular dynamics (SMD) simulations (4) of forced unbinding of the biotin-streptavidin complex. These simulations allowed exploration of the effects of molecular structure, loading direction, and experimentally accessible parameters including force transducer stiffness k and velocity v on the observed unbinding force F_R and inferred kinetic and energetic properties of the complex. The biotin-streptavidin pair was one of the first systems studied with SMD (40); while that report was groundbreaking in terms of technique, we performed new simulations because there were several aspects that would benefit from advances in computational resources and protocols over the past decade, including the current capacity to simulate the entirety of the streptavidin tetramer over nanosecond timescales. In both the experimental and simulated loading rate regimes, we find that several experimentally accessible factors other than loading rate significantly affect both the observed F_R and the calculated binding parameters. Each of these factors can alter the ligand's exploration of the energy landscape presented by the receptor. In particular, an increase in the effective stiffness of the molecular force transducer k directly perturbs the energy landscape, leading to an increase in the observed F_R and to wide variation in extrapolated binding parameters. A new model, which corrects for the effects of k on unbinding force and kinetic dissociation rates, is introduced.

METHODS

Steered molecular dynamics

Grubmüller et al. (40) have reported SMD simulations of the forced unbinding of biotin from the streptavidin monomer, a choice due in large part to limited computational resources. As the residues of the biotin binding pocket are located on two streptavidin subunits, our physics-based procedure for equilibration of simulation proteins (47) confirmed that the biotin-streptavidin monomer was an inherently poor representation of this complex. For detailed information on the SMD simulations performed on the biotin-streptavidin monomer, see Supplementary Material. We subsequently conducted SMD simulations of the full streptavidin tetramer, with biotin bound in all four binding sites. The biotin-streptavidin tetramer (PDB ID 1STP (13)) was simulated as described previously (47). Briefly, using the GROMACS molecular dynamics package, version 3.3 (48,49), the protein was solvated in a cubic box of edge length 8.59 nm with 18,533 simple-point charge (SPC216) water molecules: 50 sodium ions and 42 chlorine ions were added to provide charge neutrality and to mimic physiological conditions. Steepest-descent minimization of the x-ray diffraction structure was implemented to reduce the maximum force in the system to 2000 kJ mol⁻¹ nm⁻¹. After minimization, unconstrained molecular dynamics simulation over 100 ns was performed to equilibrate the system. This required one week on 12 dual-processor Intel Xeon 3.0 GHz cluster nodes. The initial position of the force transducer (spring) in all SMD simulations coincided with one of the terminal oxygen atoms of the biotin (designated O2 in the PDB structure), the atom at

which intermediate linkers ostensibly bond in the molecular force spectroscopy experiments. The position of this atom in the structure of biotin is shown in Supplementary Material Fig. S2.

Using the protocol developed in Walton and Van Vliet (47), we determined that the complex had entered a local energy minimum within 15 ns of beginning the equilibration trajectory. Structures were taken from this trajectory at intervals of 10 ns from time 15 ns to 95 ns. These were used as initial configurations for subsequent, identical SMD simulations. One subunit of the tetramer was subjected to loading forces, although all four biotin binding sites were occupied. The tensile loading direction was defined as the vector between the initial center of mass of the streptavidin subunit and the O2 atom of the biotin bound to that subunit. The center of mass of the streptavidin tetramer was fixed, but the system was allowed to rotate about the center of mass. Transducer spring constants k ranged from 500 to 5000 kJ mol⁻¹ nm⁻² (0.83–8.3 N/m) while velocities v ranged from 0.4 to 10 m/s. Effective loading rates F' ranged from 0.4 to 11 N/s.

We performed three sets of simulations on the biotin-streptavidin tetramer. In the first set, the loading conditions (velocity v and spring constant k) were maintained while the initial equilibrated structure was varied as above. This set of simulations was designed to test the effects of initial complex structure on the measured unbinding force. In the second set, the loading direction was varied by vector rotation of $\pm 5^\circ$ and $\pm 10^\circ$ around the x , y , and z directions. In the third set, the initial structure was maintained while the loading conditions were varied. The structure taken from the equilibration trajectory at 20 ns was used. This set of simulations was designed to test the effects of experimentally accessible parameters on the unbinding force measurement—that is, parameters that are amenable to intentional variation in physical experiments.

The resulting trajectories were analyzed to extract the force exerted by the spring and the reaction coordinate of the ligand as functions of simulation time. Here, the reaction coordinate χ is defined as the distance of the biotin O2 atom from its initial position, $\chi = \sqrt{(x - x_0)^2 + (y - y_0)^2 + (z - z_0)^2}$. In analysis of the tetramer, we examined the forces at 200 fs intervals to investigate how the applied force varied with reaction coordinate χ . Other time intervals were also explored; 200 fs was selected because this interval allowed for examination of the trajectory without significant changes in the maximum unbinding force selected by visual inspection of force F versus reaction coordinate χ ($\Delta F_R \sim 1\%$). When the unbinding force F_R is referenced, it is the maximum force recorded during a particular trajectory (e.g., see Supplementary Material Fig. S1 B). The energetic unbinding distance x_b and kinetic dissociation rate k_{off} were determined via a least-squares linear regression of F_R versus $\ln F'$ to obtain the slope (m) and x -intercept (b). From Bell's model, it is easily found that $x_b = (k_B T/m)$ and $k_{\text{off}} = b x_b / k_B T$.

Experiments

AFM-enabled molecular force experiments on biotin-streptavidin were conducted to obtain F_R , k_{off} , and x_b as a function of experimentally accessible variables such as loading rate and force transducer stiffness. Silicon nitride AFM cantilevers of varying nominal spring constant k_c (11, 35, 58, and 121 pN/nm or mN/m) were used as force transducers (MLCT-AUHW, Veeco Instruments, Woodbury, NY; MAC-IV levers, Agilent/Molecular Imaging, Palo Alto, CA). These cantilevers were cleaned in piranha solution (30% hydrogen peroxide: 70% sulfuric acid) for 30 min, followed by rinsing in deionized water. Cantilevers were then dried in a stream of nitrogen. *N,N*-Di-isopropylethylamine (300 μ L, Sigma-Aldrich, St. Louis, MO) and 3-aminopropyltriethoxysilane (900 μ L, Sigma-Aldrich) were used for amine derivatization of cleaned cantilevers and freshly cleaved mica in a vacuum desiccator via chemical vapor deposition for 2 h. Biotinylated BSA (B-BSA, Pierce Biotechnology, Rockford, IL) in sodium bicarbonate (pH = 8.9, 0.5 mg/mL) was added to cantilevers and mica, and the adsorption reaction proceeded overnight at 37°C (50,51). Cantilevers and mica were rinsed with 150 mM NaCl phosphate-buffered saline (PBS) twice, followed by covalent attachment of B-BSA to the cantilevers and mica with 52 mM 1-Ethyl-3-[3-dimethylaminopropyl]carbodiimide hydrochloride (EDC, Pierce Biotech-

nology) for 2 h. After the covalent conjugation of B-BSA via EDC, cantilevers and mica were rinsed five times with PBS. B-BSA-conjugated mica was incubated with 100 μ L of streptavidin (Pierce Biotechnology) in PBS (0.5 mg/mL) for 20 min, followed by rinsing 10 times with PBS.

Streptavidin-conjugated mica was imaged with biotin-functionalized cantilevers in contact mode and TopMAC mode within a fluid cell (PicoPlus AFM, Agilent/Molecular Imaging), using backside magnetically coated Si₃N₄ cantilevers. The tip was positioned for forced unbinding events based on this image (see Supplementary Material Fig. S3). The sensitivity of the photodetector (nm/V) was measured from the slope of force-displacement curves on bare mica. Cantilever spring constants (k_c , mN/m) were measured via thermal fluctuations, as reported elsewhere (52,53). At least 50 replicate force-piezoactuator displacement ($F-\Delta$) responses were acquired for each (k_c , v) condition; retraction rate v of the piezoactuated cantilever was approximately constant for a given k_c , ranging from 0.015 to 0.254 μ m/s across this F' range. Force-displacement responses were corrected for effects of hydrodynamic drag as described in the literature (54,55). Effective loading rate F' ($\sim 100, 300$, and 2000 pN/s) was calculated as the product of v and the effective spring constant $k = dF/d\Delta$ just before unloading for each $F-\Delta$ curve (32,56). The average effective spring constants for the two cantilever types were $k = 3.9$ mN/m and 6.9 mN/m, respectively, but the value derived from each force-displacement slope was used to analyze the corresponding unbinding force and loading rate. Note that there exist commercially available AFM cantilevers of lower nominal stiffness than those used here, including $k_c = 11$ pN/nm which we used to validate our predictions for these stiffer cantilevers. In this study, we primarily used these stiffer cantilevers for two reasons. First, we significantly increased the efficiency of acquiring force spectra by initially imaging the streptavidin-conjugated mica in TopMAC mode; this intermittent contact mode of imaging is not achievable in fluid for the most compliant cantilevers available. Second, in our experience with this AFM, more compliant cantilevers ($k_c < 30$ mN/m) provide an insufficiently stable signal for a wide range of loading rates; and stiffer cantilevers ($k_c > 60$ pN/nm) provide an insufficiently sensitive signal to detect pN-scale unbinding over these loading rates. These stabilities and sensitivities depend on the particular AFM laser-photodiode configuration. From these experimentally obtained spectra, x_b and k_{off} were determined as in Steered Molecular Dynamics, using the full distribution of unbinding forces in the linear regression. In short, more compliant cantilevers provide an insufficiently stable signal for a wide range of loading rates; and stiffer cantilevers provide an insufficiently sensitive signal to detect pN-scale unbinding.

In our AFM MFS experiments, we did not observe any loading rate dependence in effective spring constant $k = dF/d\Delta$ over the range of loading rates explored (100 to 50,000 pN/s). However, we did not use distensible linkers, which may be several nanometers in length (e.g., polyethylene glycol 800); such linkers may have an effective stiffness that depends on loading rate. Since unbinding force depends on both effective stiffness and loading rate, careful analysis of this loading rate dependence of effective k would be required to calculate accurate kinetic and energetic constants.

We note that in AFM MFS experiments, there are two potential definitions of the force transducer stiffness: cantilever stiffness k_c , as measured by methods such as simple harmonic oscillator displacement at room temperature (52,53); and the effective stiffness of the cantilever-linker system k , as calculated from $dF/d\Delta$ just before each unbinding event. For typical bifunctional molecular linkers, k is smaller than k_c by one order of magnitude (31,57). Therefore, when comparing results among experiments, it is important to consider whether a particular study defined the effective loading rate as $k_c v$ or $k v$.

RESULTS AND DISCUSSION

Effects of initial macromolecular structure

We simulated identical, forced unbinding experiments on a range of ostensibly equilibrated biotin-streptavidin tetramer

structures to consider how slight variation of the initial atomic positions and velocities in the ligand-receptor complex affects the observed unbinding force and inferred unbinding kinetics. Rather than choosing a single structure from the equilibration trajectory as a starting point for the SMD simulations (see Methods), we selected nine distinct sets of atomic coordinates from that trajectory, spaced at 10-ns intervals. We used each of these sets of atomic coordinates as initial structures for separate SMD simulations with the same set of initial atomic velocities (as described in Methods). Additionally, we considered one of these structures (i.e., one set of atomic coordinates) with three different sets of initial atomic velocities in separate SMD simulations. These simulations were designed to probe the stochastic nature of individual ligand-receptor unbinding events by varying initial configurations (atomic positions and velocities) independently from loading conditions.

We found marked variation in the force-distance responses (e.g., Supplementary Material Fig. S1 B) among different equilibrated configurations (both initial atomic positions and initial atomic velocities) subjected to the same loading conditions. This distribution led to a range of $\sim 20\%$ in observed unbinding forces, as shown in Fig. 2. We achieved this range whether we varied the initial atomic positions or the initial atomic velocities, indicating that either can be varied to enhance sampling in SMD simulations. Further, this range suggests the minimum variation in F_R that corresponding experiments can be expected to achieve, independent of instrument precision.

We also considered the effects of slight changes in the loading history of the ligand-receptor complex by changing loading vector orientation with respect to the binding pocket normal and also by varying the loading profile. Vector rotation by $\pm 5^\circ$ and $\pm 10^\circ$ around the x , y , and z axes led to variations in F_R of $\sim 10\%$. We further found that changing the loading history of the complex by first pushing and then pulling along the loading vector (as would occur in AFM MFS experiments) had no effect on the measured unbinding force; the limited effect of loading history observed here was expected because the ligand was intentionally placed in the most energetically favorable bound state during the equilibration trajectory.

Effects of experimentally accessible parameters

We designed a set of simulated experiments to investigate the effect of experimentally accessible parameters on the measured value of F_R by systematically varying the force transducer spring constant k and the velocity v to produce three different effective loading rates F' , while maintaining the initial structure (atomic positions and velocities) of the complex constant. As shown in Fig. 3, we observe the expected loading rate dependence of F_R for a given transducer stiffness k . These results also show that the magnitude of k strongly affects observed F_R . At the same loading rate F' ,

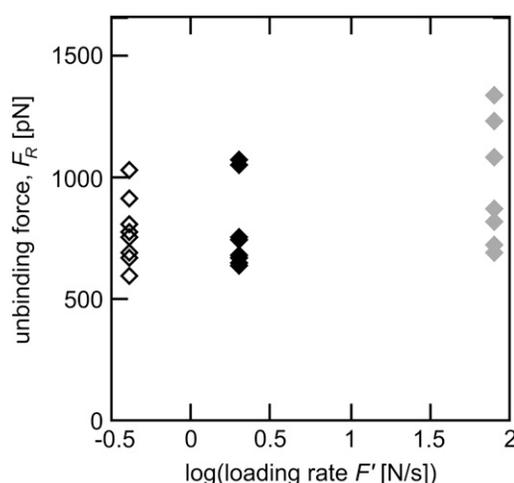


FIGURE 2 Steered molecular dynamics simulations were performed on nine different biotin-streptavidin complex configurations (some symbols overlap), with three sets of simulated experiments, differing in loading rate F' (*open*, *solid*, *shaded*). Within each set of experiments the only difference among unbinding trajectories was the starting configuration of the atoms within the complex. Between each set of simulated experiments, the only difference is the velocity v , and therefore the loading rate $F' = kv$ (*open*, $v = 0.4$ m/s; *solid*, $v = 0.8$ m/s; and *shaded*, $v = 4$ m/s). The force transducer stiffness k was 2.8 N/m in all simulations. The large range in observed unbinding force (20%), based only on the initial configuration of the molecular complex, suggests a structural reason for the experimentally observed variation in unbinding force.

simulations using larger values of k consistently exhibited higher unbinding forces F_R . In contrast to these results, Bell's model implies that the loading rate is the controlling variable for the observed unbinding force (44,58).

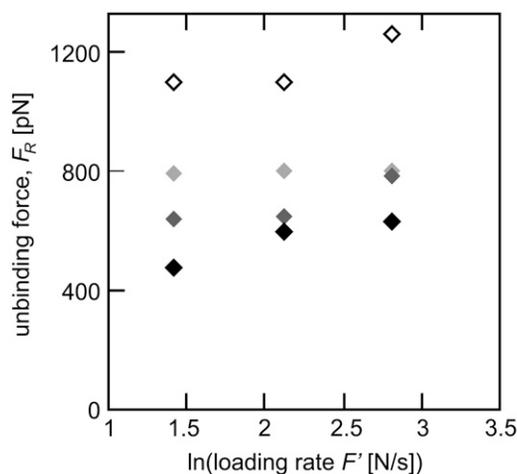


FIGURE 3 Testing the assumption that loading rate is the controlling variable for unbinding force, we systematically varied force transducer stiffness k (*solid*, 0.83 N/m; *dark shaded*, 1.66 N/m; *light shaded*, 4.15 N/m; *open*, 8.3 N/m) and velocity v to produce three different loading rates ($F' = 4.15$ N/s, 8.3 N/s, and 16.6 N/s) in SMD simulations of biotin-streptavidin rupture. At the same loading rate, a stiffer force transducer correlated with a higher unbinding force (*open points* are the stiffest force transducers, shading to *black*, which are the most compliant).

In our simulations, the force transducer stiffness k increased by more than an order of magnitude, and correlating with an increase of $\sim 200\%$ in observed unbinding forces. Consequently, the calculated dissociation rate k_{off} of the biotin-streptavidin complex varied by more than an order of magnitude, from $1.32 \times 10^{-8} \text{ s}^{-1}$ for the stiffest force transducer ($k = 8.3 \text{ N/m}$) to $5.3 \times 10^{-9} \text{ s}^{-1}$ for the most compliant force transducer ($k = 0.83 \text{ N/m}$). In contrast, calculations of the location of the energetic barrier x_b , which depend only on the slope of the linear fit to F_R versus $\ln(F')$, resulted in a range of x_b between 0.05 and 0.06 nm. Estimates of x_b from a combination of dynamic force spectroscopy experiments, flow chamber studies, and molecular dynamics simulations indicate an energetic barrier distance of $\sim 0.1 \text{ nm}$ (25,30,41).

Comparison with experimental measurements

We performed AFM MFS experiments on the biotin-streptavidin system to consider whether our simulation predictions—that higher unbinding forces are measured with stiffer force transducers for a fixed loading rate—held true in the experimental loading-rate regime.

An initial investigation was carried out with two cantilevers of differing spring constants ($k_c = 35 \text{ mN/m}$ and 58 mN/m), and the cantilever retraction velocity v was varied to measure unbinding forces at the same effective loading rates. The effective force transducer stiffness k was approximately one order-of-magnitude lower than k_c for each biotin-functionalized cantilever, as expected ($k = 3.9 \text{ mN/m}$ and 6.9 mN/m , respectively); see Methods and the literature (32,56). The unbinding force F_R , measured between a biotin-functionalized cantilever and a streptavidin-functionalized mica surface (Supplementary Material Fig. S3), was determined as the mean of a Gaussian fit to histograms constructed from at least 50 replicate single rupture events acquired under the same loading conditions (force transducer stiffness k and

velocity v), as shown in Fig. 4 A. The resulting unbinding forces are presented in Fig. 4 B as a function of $\ln(F')$, showing that the apparent strength of the complex increases as k increases—even if the loading rate F' is maintained constant. That is, the correlation of stiffer cantilevers with higher measured unbinding forces continued in the experimental loading rate regime (on the order of nN/s). It is interesting to note that an equivalent effect was reported as an incidental observation for the biotin-streptavidin system, even before the appreciation that unbinding force depended on loading rate: for a fixed velocity (ranging from 1 to $50 \mu\text{m/s}$) and unbinding force, a stiffer AFM cantilever yielded a shorter measured lifetime of the complex (38). In our experiments, the apparent strengthening effect of a stiffer cantilever had notable effects on calculated energetic and kinetic quantities, with an increase in effective k of 185% resulting in an increase in the measured unbinding force F_R of $\sim 150\%$, a decrease in the calculated energetic unbinding length x_b of $\sim 100\%$ (0.15 nm to 0.07 nm), and an increase in the calculated dissociation rate k_{off} of $\sim 250\%$ ($8.3 \times 10^{-7} \text{ s}^{-1}$ to $2.0 \times 10^{-6} \text{ s}^{-1}$). Here, k_{off} and x_b were calculated from a linear regression to the full distribution of unbinding forces, rather than the mean unbinding forces F_R .

The unbinding force distribution can be expressed as full-width half maximum (FWHM) of the experimentally measured histograms of F_R observed in replicate AFM MFS experiments at a given loading rate (see, e.g., Fig. 4 A). This FWHM corresponded well with the observed range in SMD-simulated unbinding forces among ostensibly equilibrated structures ($\sim 20\%$ of the mean F_R). However, due to the computational resources required for SMD simulations of solvated proteins, it is currently not feasible to execute the large number of forced unbinding simulations for a given parameter set (structure, k , and v) that would be required to construct the histograms and probability density functions of F_R attainable in experiments. Thus, simulations suggest but

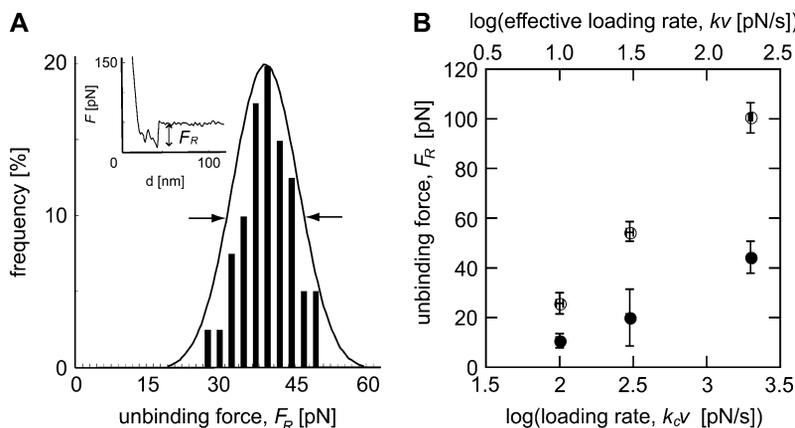


FIGURE 4 (A) Experimental measurements of biotin-streptavidin unbinding force F_R were performed via atomic-force microscope-enabled molecular force spectroscopy, utilizing cantilevers of two different spring constants. For each set of loading conditions (effective force transducer stiffness k and retraction rate v) at least 50 force-displacement ($F - \Delta$) responses for single rupture events were recorded, with F_R calculated as indicated. (Inset) A single rupture event of $F_R = 46 \text{ pN}$, under effective $k = 4.12 \text{ mN/m}$ and $v = 0.073 \mu\text{m/s}$. A Gaussian distribution was fit to the histogram of unbinding forces for each set of conditions (here, $k_c = 35 \text{ mN/m}$ and $v = 0.073 \mu\text{m/s}$), and the distribution maximum was reported as F_R . Arrows indicate the FWHM. (B) Unbinding force F_R as a function of the logarithm of the loading rate F' , as measured by AFM using two different cantilevers: $k_c = 35 \text{ mN/m}$ (solid circles) and $k_c = 58 \text{ mN/m}$ (open circles); error bars

represent one standard deviation in F_R and effective F' , and may appear smaller than symbols. In all cases, the stiffer cantilevers measured higher unbinding forces than the more compliant cantilever, indicating that the dependence of measured F_R on the stiffness of the force transducer k is not limited to the extreme loading rates achieved in simulation.

do not prove that the stochastic nature of forced unbinding of single ligand-receptor interactions is attributable in part to sampling small variations in atomic positions and velocities.

Due in part to the incomplete sampling of an ensemble response and the large difference in loading rates attainable in experiments (nN/s) and in simulations (N/s), it is not expected that the magnitude of F_R or the extrapolated kinetic and energetic parameters will agree quantitatively (41). However, SMD simulations remain valuable tools for studying forced unbinding because they can reveal atomic-level detail of mechanisms and pathways not accessible by experiment (4). Here, both simulations and experiments on the biotin-streptavidin complex show clear effects of force transducer stiffness k on measured unbinding forces. One important implication of this effect is that two experiments performed over the same loading rate range and with different, single values of k would not necessarily obtain the same magnitude or loading rate-dependence of the unbinding forces. This has been noted recently for SMD simulations (59) and optical trap experiments (60) on the mechanically forced unfolding of biopolymers. Thus, both simulations and experiments suggest that the accuracy of ligand-receptor binding parameters extracted from analyses of single complexes will be significantly enhanced by consideration of a range of both F' and k .

Effects of k on the energy landscape of the complex

Through SMD simulations and complementary AFM MFS experiments, we have shown that macromolecular structure, loading direction, and the loading conditions (k and v) can significantly affect the measured unbinding force F_R and inferred unbinding kinetics. The commonality among these factors is that they all either perturb or alter exploration of the three-dimensional energy landscape $E(x, y, z)$ of the complex.

The kinetics of any given reaction depends on the energetic barrier crossed during the reaction. The effects of applied force on the energy landscape (and, therefore, on k_{off} and x_b) have been well documented: applied force tilts the simplified one-dimensional energy landscape such that $E_F(\chi) = E_0(\chi) - F\chi$, where $E_0(\chi)$ is the unperturbed energy landscape, leading to a reduction in energetic barrier height (3,45,61). This reduction increases the kinetic off-rate as $k_{\text{off}}(F) = k_{\text{off}}^0 \exp(F_R/F_b)$, where k_{off}^0 is the equilibrium kinetic off-rate and F_b is $x_b/k_B T$. However, the effect of the force transducer stiffness k on the observed unbinding force and kinetics has been neglected. Evans has noted that a stiffer force transducer leads to a higher energetic barrier at a given applied force, but did not include this effect explicitly in analytical predictions of k_{off} under applied force (61). As we discuss below, this contribution can in fact be reasonably neglected for sufficiently compliant force transducers, such as the biomembrane force probe used in the experiments of Merkel et al. (30). Once the ligand is mechanically attached to the force

transducer, the potential energy of the force transducer must be accounted for in the energy landscape as

$$E^*(\chi) = E_0(\chi) + \frac{1}{2}k\chi^2. \quad (2)$$

Applying force to this perturbed energy landscape E^* then tilts the energy landscape such that

$$E^{**}(F, \chi) = E_0(\chi) - F\chi + \frac{1}{2}k\chi^2. \quad (3)$$

As shown in Fig. 5, the barriers presented by the tilted landscape $E^{**}(F, \chi)$ at a particular value of applied force also depend on k . When force is applied by an ideal spring

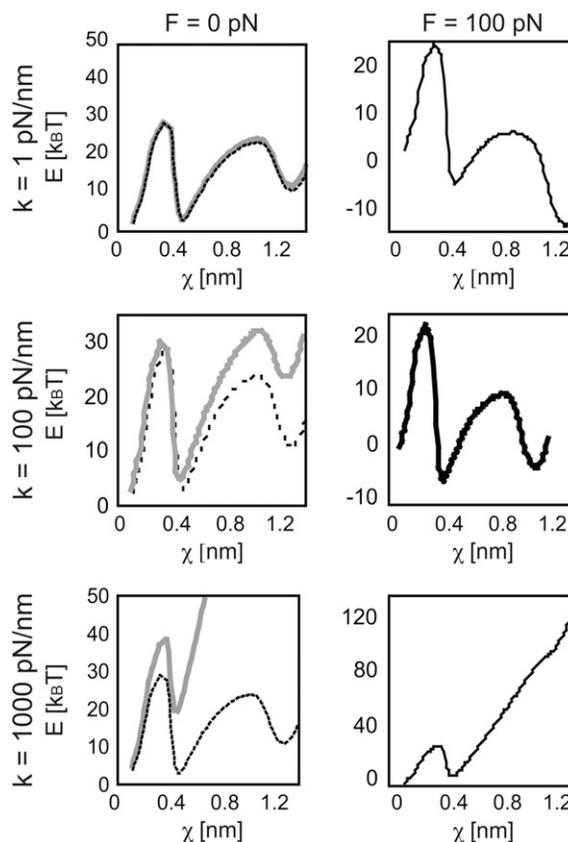


FIGURE 5 The stiffness of the force transducer not only limits the exploration of the ligand in the energy landscape, but also changes the energy landscape the ligand traverses. Here, the effects of stiffness on the biotin-streptavidin energy landscape $E^{**}(F, \chi)$ (adapted from (25,30,41)) are shown, both before pulling begins ($F = 0$, left column, gray solid line) and at an applied load of 100 pN (right column, black solid line). Compliant cantilevers of $k < 1$ pN/nm are typical of BFP and optical trap experiments (top row). For such small k , the perturbed energy landscape ($E^{**}(F, \chi)$, solid) remains close to the equilibrium energy landscape ($E_0(\chi)$, dashed) in the absence of applied force. Stiff cantilevers of $k > 1000$ pN/nm are typical of SMD simulations (bottom row). Even in the absence of significant applied force of the ligand, the perturbed energy landscape ($E^{**}(F, \chi)$, solid) is far from the equilibrium landscape ($E_0(\chi)$, dashed). AFM cantilevers of $k \approx 10$ –100 pN/nm are intermediate to these extremes (middle row). Since application of a nonzero force inherently implies a nonequilibrium state of the bound complex, no equilibrium landscape is depicted in the right column ($F = 100$ pN).

(force = $k\chi$), a stiffer force transducer leads to a higher energetic barrier to unbinding (and therefore a higher unbinding force) as shown by Eq. 3. The kinetic rate of dissociation is then

$$k_{\text{off}} = k_{\text{off}}^0 \exp\left(\frac{(F_{\text{R}} - \frac{1}{2}kx_{\text{b}})/F_{\text{b}}}{k_{\text{B}}T}\right), \quad (4)$$

where F_{b} is $x_{\text{b}}/k_{\text{B}}T$ and k_{off}^0 is the dissociation rate of the system at equilibrium (corresponding to $E_0(\chi)$). This implies that, rather than extracting the energetic and kinetic parameters of the complex from Eq. 1, x_{b} and k_{off} should be extrapolated from

$$F_{\text{C}} = F_{\text{R}} - \frac{1}{2}kx_{\text{b}} = \frac{k_{\text{B}}T}{x_{\text{b}}} \ln \frac{F'x_{\text{b}}}{k_{\text{B}}Tk_{\text{off}}}, \quad (5)$$

where F_{C} is the unbinding force at a particular loading rate F' that has been corrected for the barrier perturbation due to k .

For some experimental approaches such as BFP and optical traps, the force transducer stiffness is typically small enough ($k \approx 1$ pN/m) that the additional term $(1/2)kx_{\text{b}}$ may be negligible. In fact, this contribution to the observed unbinding force has been reasonably neglected in such experiments thus far. However, in both AFM MFS and SMD measurements of the unbinding force, the opposing force contribution $(1/2)kx_{\text{b}}$ can be on the same order of magnitude as F_{R} . It is important to note that the effective stiffness of the force transducer k may depend on loading rate as well as the mechanical compliance of any molecular linkers (see Methods). In Fig. 5, we demonstrate the effect of force transducer stiffness on the biotin-streptavidin energy landscape (25,30,41) for three different values of k (1 pN/nm, which corresponds to optical trap and BFP experiments; 100 pN/nm, which corresponds to AFM MFS; and 1000 pN/nm, which corresponds to SMD) and at two different instances of applied force ($F = 0$ pN, or before pulling begins, and $F = 100$ pN). Even before force is applied, the energy landscape is perturbed much more by the stiff force transducer than by more compliant force transducers. In the limit of an infinitely compliant force transducer ($k = 0$), the perturbed energy landscape $E^{**}(F, \chi)$ is equal to the equilibrium energy landscape E_0 . In this case, $E^*(F, \chi)$ and $E^{**}(F, \chi)$ reduce to a single expression for the height of the energetic barrier at x_{b} . Very compliant force transducers, such as those used in biomembrane force probe experiments ($k \approx 1$ pN/nm for the strongly-bound biotin-streptavidin system (30)), may be considered to adhere to this compliant limit. However, as the force transducer stiffness increases, the perturbation of the energy landscape increases and the difference between $E^*(F, \chi)$ and $E^{**}(F, \chi)$ becomes significant. Next, we show that this correction of the observed unbinding force (Eq. 5) eliminates the apparent dependence of k_{off} and x_{b} on force transducer stiffness k for both simulations (Fig. 3) and experiments (Fig. 4 B).

To determine x_{b} from experiments using our corrected model, we fit the experimental unbinding forces F_{R} from

two cantilevers ($k_{\text{c}} = 35$ and 58 mN/m) to Eq. 5, using least-mean-squares minimization of the residual defined as $\sum_n F_{\text{C}}(k_n) - F_{\text{C}}(k_0)$. Here, n is the number of different transducer stiffnesses considered for a given loading rate (for our experiments, $n = 2$); and k_0 is the stiffness of the most compliant transducer (for our experiments, $k_0 = 3.9$ mN/m). To determine x_{b} from the simulations, the identical procedure was performed with the simulated stiffnesses k and unbinding forces F_{R} (for our simulations, $n = 4$ and $k_0 = 0.83$ N/m). As shown in Fig. 6 for SMD simulations, correcting for the effects of k on the energy landscape as outlined above brings the corrected unbinding forces calculated with different force transducer stiffnesses k into agreement with each other, within the $\pm 10\%$ error attributable to the stochastic nature of ligand-receptor interactions. Corrections of the observed experimental unbinding forces F_{R} yielded similar results. Both x_{b} and k_{off} can be extracted from the corrected data, resulting in values of 0.05 nm and $5.1 \times 10^{-9} \text{ s}^{-1}$, respectively, for the simulations; and 0.11 nm and $2.1 \pm 0.5 \times 10^{-7} \text{ s}^{-1}$, respectively, for the AFM experiments. To validate this correction of effective force transducer stiffness on the energy landscape and inferred unbinding kinetics, we also repeated the calculation of k_{off} after including unbinding forces obtained with both stiffer cantilevers ($k_{\text{c}} = 121$ mN/m, $F_{\text{R}} = 112.0 \pm 4.9$ pN) and more compliant cantilevers ($k_{\text{c}} = 11$ mN/m, $F_{\text{R}} = 38.7 \pm 5.4$ pN) at a loading rate of 2000 pN/s: k_{off} calculated over this wider range of force transducer stiffness ($2.7 \pm 0.6 \times 10^{-7} \text{ s}^{-1}$ agreed within experimental error with that obtained over the narrower range of $k_{\text{c}} = 35$ and 58 mN/m. Our values of x_{b} from experiment and simulation agree well with previous experiments (25,30,41), which indicate that x_{b} is ~ 0.1 nm, the energetic distance of the innermost energy barrier accessible at these loading rates. The

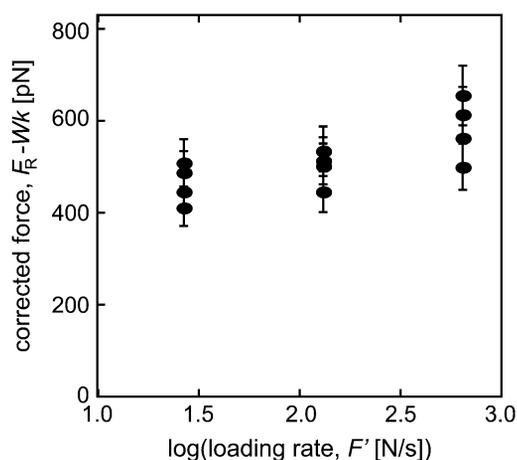


FIGURE 6 After correcting biotin-streptavidin unbinding forces measured via SMD simulations according to Eq. 3, the corrected unbinding force F_{C} for all values of k agree within estimated error ranges (error estimated as $\pm 10\%$, based on 20% FWHM of force distribution in both simulations and experiments). Uncorrected unbinding forces F_{R} are shown in Fig. 2.

equilibrium dissociation rate of biotin-streptavidin as measured by competitive binding is $2.4 \times 10^{-6} \text{ s}^{-1}$ (62), which is within an order of magnitude of our experimental k_{off} . Given our limited range of loading rates, we find this agreement to be reasonable. Although k_{off} inferred from SMD simulations does not extrapolate well to equilibrium dissociation rates, as anticipated for such large F' (4), it is notable that this correction of simulated F_{R} by $(1/2)kx_{\text{b}}$ results in extracted energetic and kinetic parameters of the complex that agree much more closely with experimental estimates.

Another interpretation of the experimentally observed stiffness dependence of the unbinding force is that, at a given loading rate, a stiffer cantilever will lead to the AFM probe being in contact with the surface for a longer period of time (at a given F' , a stiffer cantilever necessitates a slower v ; total displacement remains constant). Although the contact times in the range of experimental loading rates we employed are well above the generally reported association time for biotin-streptavidin ($\sim 1 \mu\text{s}$ (63)), with more time to interact, one could conjecture that biotin may have sufficient time to sample a lower energy minimum in the streptavidin binding pocket. Note that while the probability of the complex re-binding is also dependent on stiffness (61), re-binding is prohibited at the velocities employed in AFM MFS experiments and SMD simulations. As illustrated in Fig. 5, the biotin-streptavidin energy landscape has three major energy minima (25,30,41); the timescale of our AFM experiments ($\approx 0.2\text{--}2 \text{ s}$) is such that it is theoretically possible for both the deepest and the second-deepest minima to be populated (25). However, this would suggest that a multimodal distribution of unbinding forces would be observed for a given k and F' . We did not observe such a distribution in our experiments, suggesting that our AFM MFS experiments consistently sampled a single energy minimum.

CONCLUSIONS

Our computational and experimental analyses of forced unbinding for the biotin-streptavidin complex demonstrate that loading rate is not the only controlling factor of the observed unbinding force F_{R} and inferred unbinding kinetics. The effective stiffness k , which represents the mechanical resistance of the total force transducer inclusive of any molecular linkers, can lead to manifold changes in the magnitude and rate dependence of the observed F_{R} . Further, our consideration of multiple structures of this complex demonstrates that a common assumption of SMD simulations—namely, that a single equilibrated structure will not explore enough of its phase space to impact simulation results—is not true for forced unbinding of ligand-receptor pairs. Even in consideration of an incomplete ensemble of ostensibly equilibrated initial configurations, we observed variations of $>20\%$ in F_{R} attributable only to minute differences in atomic positions or velocities.

We have demonstrated that the measured unbinding force of a ligand-receptor complex depends on several experi-

mentally accessible factors that perturb or limit exploration of the energy landscape. These factors are especially important in interpretation of results utilizing effective force transducer stiffness of $k > 1 \text{ pN/nm}$, as is common in AFM MFS experiments and SMD simulations. Beyond the established dependence on F' , the magnitude of the force transducer k has the most dramatic effect on the inference of equilibrium behavior, as captured by the velocity of dissociation k_{off} and the energetic distance x_{b} . Consideration and quantification of these factors is necessary if forced unbinding experiments are used to infer the kinetics and energetics required for both predictive simulations and biomedical applications such as drug discovery. The demonstrated synergism between simulation and experiment elucidates several key parameters that affect the nature and interpretation of forced ligand-receptor unbinding. In particular, although it has been known that the magnitude of k effectively limits the exploration of the energy landscape of a ligand-receptor complex, these results show that this controllable parameter also directly perturbs that landscape to effect wide variations in F_{R} , k_{off} , and x_{b} . We have demonstrated that this perturbation of the energy landscape via force transducer stiffness can be accounted for to obtain an effective unbinding force at each loading rate, and thus the equilibrium energetic and kinetic parameters of the complex. Beyond these model systems and experiments, our results suggest that the force required to dissociate molecular complexes can be altered by the mechanical compliance of the macromolecular structures to which the ligand (or receptor) is tethered, e.g., that of the extracellular matrix. Both experimental and computational analyses of biologically relevant ligand-receptor complexes under mechanical constraints or strain (64) will benefit from consideration of the sources and magnitude of variation in the observed unbinding forces and inferred kinetics.

SUPPLEMENTARY MATERIAL

To view all of the supplemental files associated with this article, visit www.biophysj.org.

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