

## Lecture Notes on Fluid Dynamics

(1.63J/2.21J)

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1-8Rayleigh.tex

### 1.8 Rayleigh's Problem - solid wall as a source of vorticity

Owing to terms representing convective inertia, the Navier-Stokes equations are highly non-linear. Explicit solutions are usually limited to a class of problems where inertia is identically zero. This happens when the flow is unidirectional and uniform. Flow quantities depend only on a transverse coordinate. We discuss one such example with a view to examining the role of viscosity.

Consider a two-dimensional flow in the upper half plane of  $(x, y)$  bounded below by a rigid plate coinciding with the  $x$  axis. At  $t = 0$  the plate suddenly moves in the tangential direction at constant velocity  $U$ . Find the development of the fluid motion in the region  $y > 0$ .

Because the plate is infinite in extent, the flow must be uniform in  $x$ , i.e.  $\frac{\partial}{\partial x} = 0$ . It follows from continuity that

$$\frac{\partial v}{\partial y} = 0, \quad y > 0$$

implying that  $v = \text{constant}$  in  $y$ . Since  $v(0, t) = 0$ ,  $v \equiv 0$  for all  $y$ . Therefore, the only unknown is  $u(y, t)$  which must satisfy the momentum equation,

$$\frac{\partial u}{\partial t} = \nu \frac{\partial^2 u}{\partial y^2} \tag{1.8.1}$$

where

$$\nu = \frac{\mu}{\rho} \tag{1.8.2}$$

denotes the kinematic viscosity. The boundary conditions are :

$$u = U, \quad y = 0, \quad t > 0; \quad \text{no slip} \tag{1.8.3}$$

$$u = 0, \quad y \sim \infty, \quad t > 0 \tag{1.8.4}$$

The initial condition is

$$u = 0, \quad t = 0, \quad \forall y \tag{1.8.5}$$

Mathematically this is the heat conduction problem for a semi-infinite rod. The solution is well-known (Carlaw & Jeager, *Conduction of Heat in Solids* or Mei, *Mathematical Analysis in Engineering*),

$$u = U \left( 1 - \operatorname{erf} \frac{y}{2\sqrt{\nu t}} \right) \tag{1.8.6}$$

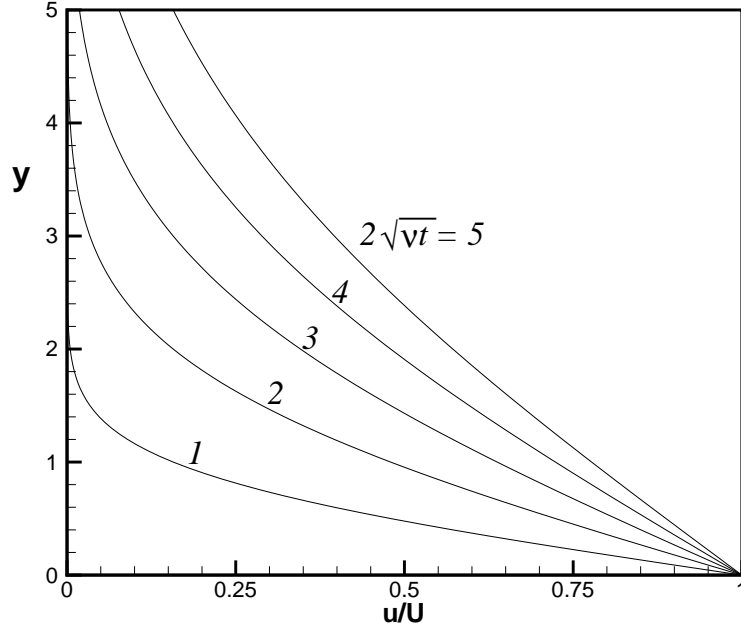


Figure 1.8.1: Velocity profile due to impulsive motion of  $x$ -plane

where

$$\operatorname{erf} \zeta = \frac{2}{\sqrt{\pi}} \int_0^{\zeta} e^{-\lambda^2} d\lambda. \quad (1.8.7)$$

is the error function. As shown in Figure 1.8.1,

fluid momentum is diffused away from the plane  $y = 0$ . The region affected by viscosity (the boundary layer) grows in time as  $\delta \sim \sqrt{\nu t}$ . This observation can be confirmed, indeed anticipated, merely by a scaling argument based on the momentum equation (1.8.1) without solving it. Let  $U, t, \delta$  denote the scales of velocity, time and region of viscosity respectively. For viscosity to be important, the two terms in (1.8.1) must be comparable in order of magnitude, i.e.,

$$\frac{U}{t} \sim \nu \frac{U}{\delta^2}$$

It follows that

$$\delta \sim \sqrt{\nu t}$$

Let us use this simple example to study the role of vorticity

$$\vec{\zeta} = \left( \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right) \vec{k} \quad (1.8.8)$$

In this problem there is only one vorticity component,

$$\zeta_3 = -\frac{\partial u}{\partial y} = U \frac{\partial}{\partial y} \operatorname{erf} \frac{y}{2\sqrt{\nu t}} = \frac{2U}{\sqrt{4\pi\nu t}} e^{-y^2/4\nu t}. \quad (1.8.9)$$

which is just the velocity shear. Mathematically (1.8.9) is the solution to the diffusion equation

$$\frac{\partial \zeta}{\partial t} = \nu \frac{\partial^2 \zeta}{\partial y^2}. \quad (1.8.10)$$

which follows from (1.8.1), and the initial condition that there is a plane source of at  $y = 0$ :

$$\zeta_3(y, 0) = 2U\delta(y). \quad (1.8.11)$$

Thus vorticity is diffused away from the solid wall which acts as a vorticity source. Note that the shear stress at the wall is

$$\tau_{xy}(0, t) = \mu \left. \frac{\partial u}{\partial y} \right|_{y=0} = -\rho U \sqrt{\frac{\nu}{\pi t}}. \quad (1.8.12)$$

which is initially infinite but decays with time.

Why is the wall a source of vorticity? Just after the plane started to move there is a velocity discontinuity at  $y = 0+$ . The associated velocity gradient is  $\partial u/\partial y = -U\delta(y)$  hence the vorticity is a highly concentrated function of  $y$ :  $-\partial u/\partial y = U\delta(y)$ . Furthermore the half space ( $0 < y < \infty$ ) problem can be thought of as one half of the whole plane problem for  $-\infty < y < \infty$  if the top of the fluid in the lower half plane suddenly moves to the left at the speed  $U$ . This would give an initial vorticity  $U\delta(y)$  at  $y = 0-$ . Thus for the a whole space problem there is a vorticity source of total strength  $2U\delta(y)$  at the initial instant. As time proceeds, half of the released vorticity is diffused to the region of  $y > 0$  and half to  $y < 0$ . Thus, the solid wall is the source of vorticity.

The reader can verify the solution (1.8.9) by assuming a similarity form,

$$\zeta_3(y, t) = \frac{C}{\sqrt{t}} f\left(\frac{y}{\sqrt{t}}\right) \quad (1.8.13)$$