

### Homework#3

Given: October 23, 2002 Due: November 6, 2002

1. **Weld design:** Solve Problem 7.2-11, page 541, Gere. Establish the Tresca plastic yield condition and brittle rupture condition for the weld. If the weld material has Young's modulus  $E$  and Poisson's ratio  $\nu$ , calculate the strains acting on the weld.

2. **Thick-walled cylindrical pressure vessel design:** A *closed-end* cylindrical pressure vessel of inner radius  $a$  and outer radius  $b$  is subject to internal pressure  $p$ . The stresses are

$$\begin{aligned}\sigma_{rr} &= -\frac{p}{(b/a)^2 - 1} \left( \frac{b^2}{r^2} - 1 \right) \\ \sigma_{\theta\theta} &= \frac{p}{(b/a)^2 - 1} \left( \frac{b^2}{r^2} + 1 \right) \\ \sigma_{zz} &= \frac{p}{b^2/a^2 - 1}\end{aligned}$$

Find the Mises yield and brittle rupture conditions for the vessel.

3. **Thin-walled spherical and cylindrical pressure vessel design:** Let  $b = a + t$  where  $t$  is the thickness of the spherical pressure vessel/cylindrical pressure vessel.

Substitute the above relation in stress equations for the spherical pressure vessel (Eq. 6.1 Lecture#8 with  $p_e = 0, p_i = p$ ) and cylindrical pressure vessel (equations in Problem 2 above).

Then assume that the pressure vessels are *thin-walled*, or  $a \gg t$ , so that higher order terms of  $t$  are negligible. Simplify the stress relations for this case and compare your results with those of Gere (pg. 557-571). Establish the brittle rupture conditions for thin-walled spherical and cylindrical pressure vessels.

4. **Weight optimization design of a sandwich beam:** Suppose you are provided with many thin steel ( $E_{steel} = 240$  GPa,  $\rho_{steel} = 7.8 \times 10^3$  kg/m<sup>3</sup>) and aluminum ( $E_{aluminum} = 70$  GPa,  $\rho_{aluminum} = 2.7 \times 10^3$  kg/m<sup>3</sup>) sheets of thickness  $t$  and width  $b$ , and many thick aluminum foam slabs ( $E_{foam} = 7$  GPa,  $\rho_{foam} = 0.27 \times 10^3$  kg/m<sup>3</sup>) of thickness  $h$  and width

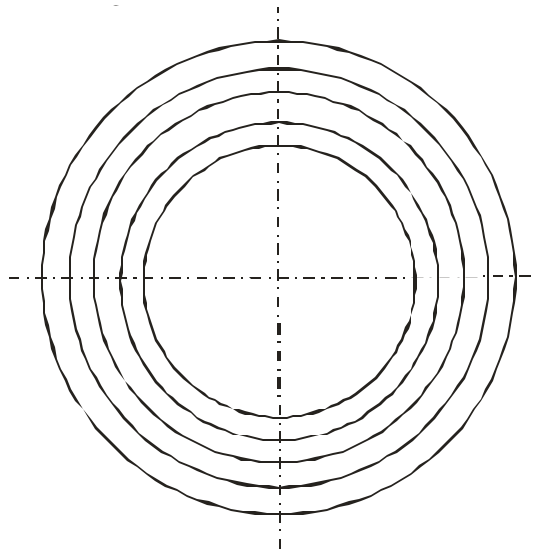
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b. Also given is that  $t \ll h$ . There is only enough adhesive (with shear strength  $\tau_c$ ) to bond only four surfaces so that some of the material will not be used. You are required to design a sandwich beam which strictly includes all the three materials! Design the sandwich beam for the combination of all the following three requirements:

- maximum bending resistance
- maximum shear resistance
- minimum weight

#### 5. Brittle rupture design of a multi-layered composite beam:



Consider a cylindrical multi-layered composite beam made up of hollow cylindrical beams of different *brittle* materials with Young's moduli;  $E_1 = 4E, E_2 = 3E, E_3 = 2E, E_4 = E$ .  $E = 400$  GPa. The internal radius of cylinder 1 is  $a = 25$  mm, while all hollow cylinders are of thickness  $t = 2.5$  mm. Observe  $a \gg t$ . The fracture strengths are;  $\sigma_f^1 = 2\sigma_f, \sigma_f^2 = \sigma_f, \sigma_f^3 = 0.5\sigma_f, \sigma_f^4 = 0.25\sigma_f$   $\sigma_f = 25$  MPa

- find the neutral axis for the composite beam
- what is the elastic bending stiffness of the beam?
- what is the critical bending moment  $M_y^f$  for brittle rupture?
- find the corresponding deflection  $w_o^f$  at brittle rupture if the beam is under 4-point bending (Let beam length be  $L$ ).