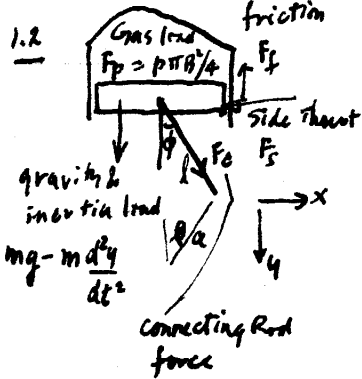
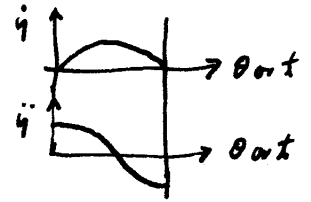


2.615 Solution to HW #1



Note: 1) The inertia load term changes direction during the piston descend

2) The side thrust F_s is a normal reaction to balance the x component of the connecting rod force F_c .

$$m \ddot{y} = mg + F_c \cos \phi + p \frac{\pi B^2}{4} - F_f$$

$$F_s = F_c \sin \phi$$

and the frictional force F_f is

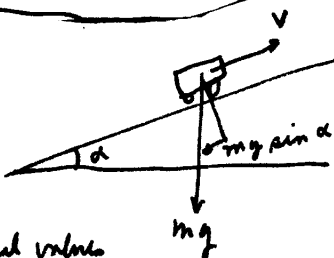
$$F_f = f F_s \text{ where } f \text{ is the frictional coeff.}$$

$$\phi \text{ and } \theta \text{ are related by } \phi = \sin^{-1}(a \sin \theta / L)$$

at $\theta = 45^\circ$, for $L/a = 3.5$, $\phi = 11.7^\circ$

	SI engine		DI engine	
	N	lbf	N	lbf
F_p	1.13×10^8	2.58×10^3	1.77×10^5	3.97×10^4
F_c	1.15×10^8	2.58×10^3	1.81×10^5	4.0×10^4
$F_c \sin \phi$	2.34×10^7	5.15×10^2	3.67×10^4	8.07×10^3

2.5



typical values

$$C_D = 0.4$$

$$A_v \text{ (frontal area)} = 2 \text{ m}^2$$

$$C_R = 0.013$$

$$V = 50 \text{ mph} = 22.4 \text{ m/s}$$

$$m = 1500 \text{ kg}$$

$$\alpha = 15^\circ$$

$$P_{\text{required}} = P_{\text{gravity}} + P_{\text{drag}} + P_{\text{friction}}$$

$$= [mg \sin \alpha + \frac{1}{2} \rho_a C_D A_v V^2 + C_R mg \cos \alpha] V$$

$$= [1500 \times 9.81 \times \sin 15^\circ + \frac{1}{2} \times 1.2 \times 0.4 \times 2 \times 22.4^2 + 0.013 \times 1500 \times 9.81 \times \cos 15^\circ] \times 22.4$$

$$= [3808.5 + 240.8 + 184.8] \times 22.4$$

$$= \underline{95 \text{ kW}}$$

Note: The drag and friction components are roughly

equal. The power to propel against gravity is much higher.

M. accel for 40 to 60 mph in 5 sec: (1 mph = 0.447 m/s)
 $a = \Delta v / t = (20 \times 0.447 / 5) = 1.79 \text{ m/s}^2$
 $m a = 2680 \text{ N}$

2.8

$$\eta_f \text{ (brake)} = 0.3$$

$$bsfc = \frac{m_f}{m_f Q_{HV} \eta_f} = \frac{1}{Q_{HV} \eta_f} ; \text{ Put in conversion factors } bsfc \left[\frac{\text{kg}}{\text{kWh}} \right] = \frac{1}{Q_{HV} (\text{J/kg}) \eta_f} \times 3.6 \times 10^6$$

	Fuel	2-octane	Gasoline	methanol	H ₂
$Q_{HV} \text{ (low)} (\text{J/kg})$		44.3×10^6	44.0×10^6	20.0×10^6	120×10^6
$bsfc \text{ (kg/kWh)}$		0.271	0.273	0.600	0.100

2.11 Design requirement: 300 kW Full Power

say max piston speed = 12 m/s, max mep 10 bar (stress limited)

$$\text{For number of cylinders } = C : \frac{1}{2} C V_D \text{ mep } N = \text{Power}$$

↑
(factor of 1/2 for 4 stroke)

$$\text{Thus Power} = \frac{1}{4} C \left(\frac{\pi B^2}{4} \right) \underbrace{(2NL)}_{\text{fixed}} \underbrace{\text{mep}}_{\text{fixed}}$$

The trade off between C & B has to do with other considerations. (knock, packaging, heat transfer etc.) will pick a 8 cylinder engine and do the numbers to see whether they are reasonable.

(2-11 cont.)

Using $c=8 \Rightarrow 300 \times 10^3 = \frac{1}{4} \times 8 \times \left(\frac{\pi B^2}{4}\right) \times 12 \times 10 \times 10^5 \rightarrow B = \underline{\underline{13 \text{ cm}}} \text{ (}\approx 5 \text{ in.)}$

Say bore to stroke ratio $B/L \approx 1$ Then $L = 13 \text{ cm}$ and $2\pi L = 12 \text{ m/s}$

would give $N = 46.15 \text{ cps}$ or $\underline{\underline{2769 \text{ rpm}}}$.

Torque: $T = 2\pi N = \frac{N}{2} V_D m_{ep} \Rightarrow T = \left(\frac{1}{4\pi}\right) V_D \cdot m_{ep} \cdot c = \frac{1}{4\pi} \times \frac{\pi \cdot 13^3}{4} \times 10 \times 8 = \underline{\underline{1100 \text{ N}\cdot\text{m}}}$
for 4 stroke

Fuel flow rate: Say $\eta_f = 0.3$; $P = Q_{fw} \eta_f m_f$

Thus $m_f = P / (Q_{fw} \eta_f) = 3 \times 10^5 / (4.3 \times 10^7 \times 0.3) = 2.33 \times 10^{-2} \text{ kg/s} = \underline{\underline{84 \text{ kg/hr}}} \approx 28 \text{ gallon/hr.}$

(These figures are typical for a commercial V-8 truck engine.)

2-13

1.6 litre displacement engine, 4 cylinder, WOT @ 2500 rpm.

Say $B/L = 1 \Rightarrow \frac{\pi}{4} L^3 = 400 \text{ cc}$ or $L = 8 \text{ cm}$

mean piston speed $\bar{S}_p = 2\pi L = 2 \times \frac{2500}{60} \times 0.08 = \underline{\underline{6.67 \text{ m/s}}}$

Max piston speed (see fig. 2-2 of Text) $\approx 1.6 \bar{S}_p = \underline{\underline{10.7 \text{ m/s}}}$

Max charge velocity at intake = Max piston speed \times Area ratio = $10.7 \times 5 = \underline{\underline{54 \text{ m/s}}}$

(The following are estimates of the time taken for the various

processes. Refer to figure 1-8 in Text for more precise numbers.)

— Time per cycle @ 2 revolution per cycle = $\left(\frac{60}{2500} \times 25\right) = \underline{\underline{48 \text{ ms}}}$

— Intake, compression, expansion and exhaust each takes up $\sim 1/4$ of the cycle time $\sim \underline{\underline{12 \text{ ms}}}$

— Combustion: Starts $\sim 20^\circ \text{ BTC}$, ends $\sim 40^\circ \text{ ATC}$. Duration = 60°
time = $\frac{60}{720} \times 48 \text{ ms} = \underline{\underline{4 \text{ ms}}}$

— Flame velocity: Say flame starts at the center (spark plug centrally located). It has to traverse the radius in 4 ms

Flame velocity = $\frac{0.04 \text{ m}}{4 \times 10^{-3} \text{ s}} = \underline{\underline{10 \text{ m/s}}}$

— WOT intake "run length" = $\frac{V_D}{A_{port}} = \frac{V_D}{A_{piston} \times 1/5} = \frac{\text{stroke}}{1/5} = \underline{\underline{40 \text{ cm}}}$

— Exhaust "run length" = $\frac{V_D}{A_{port}} \times \text{Temperature ratio} = 40 \text{ cm} \times \frac{425+273}{300} = \underline{\underline{93.07 \text{ cm}}}$