

TABLE 1. Design Summary

Parameter	Specification	Calculated	Simulated
V_A	NA	4.0	4.0
V_B	NA	3.7	3.7
$ A_v $	> 77.5 dB	135.2 dB	78.3 dB
f_{3dB}	> 100 KHz	103.7 KHz	123 KHz
f_{unity}	> 40 MHz	73.3 Mhz	41.7 MHz
Output Voltage Swing	> 3 V	3.7 V	3.2 V
Power Dissipation	< 100 uW	8.84 uW	95.9 uW

88.4?

$\frac{W}{L}$? - 2
~~Report should~~

Chapter 2

Engineering Decisions

2.1 Drain Current I_d

Considering the maximum power dissipation was $100\mu\text{W}$ and the V_{dd} was 5 volts, we immediately knew that the maximum drain current was $20\mu\text{A}$. I_d can be controlled in two ways.

- Increasing the width effectively increases the current.
- Decreasing the voltage (V_a and V_b) increases the current.

There was a tradeoff involved, however. Increasing the current will increase the second-pole breakpoint frequency f_{3db} , but will decrease the gain. We want the gain to be as high as possible.

2.2 Choice of V_a and V_b

It was clear from the start that the choice of V_a and V_b were crucial because they would have major implications as far as current, power, and frequency are concerned. The constraints, coupled with some trial-and-error, helped us find the optimal choice. The process behind choosing V_a and V_b is outlined below.

- As discussed in the previous section, the power constraint makes the maximum drain current $20\mu\text{A}$. We began by assuming that I_{d1} (stage 1) and I_{d2} (stage 2) were each $10\mu\text{A}$, yielding a total drain current of $20\mu\text{A}$.
- We assumed the minimum length ($1.5\mu\text{m}$) and minimum width ($6\mu\text{m}$) to begin with and using a saturation current of $10\mu\text{A}$, calculated that V_a and V_b both are 4.7 Volts. Using this as a starting point, we kept lowering the voltages (keeping them equal) until $V_a = V_b = 4$ Volts. At this point, we noticed that the gain specification was met (well over 7500) but the 3 dB frequency was ~~too~~ too low (by 50 percent).
- In order to raise the 3 dB frequency, we had to adjust the open-circuit time constants associated with the Miller Approximation. As shown in the Miller equivalent circuit following the report, f_{3db} is dependent on the capacitances C_a , C_b and C_c , which in turn are dependent on the gain (A_{v1} and A_{v2}).

- In this configuration, C_c was *significantly* higher (by 3 orders of magnitude) than C_a and C_b . Clearly, the time constant associated with Capacitor C was the dominant term. Since $w(3dB)$ is the inverse of the sum of the individual open-circuit time constants, decreasing the capacitance of C would effectively increase the 3 dB frequency. Thus, as illustrated by the calculations accompanying the Miller Approximation circuit, A_{v2} must decrease, thereby resulting in a decrease in V_b . V_b was set at 3.7 Volts. Keeping V_a at 4 Volts was sufficient.

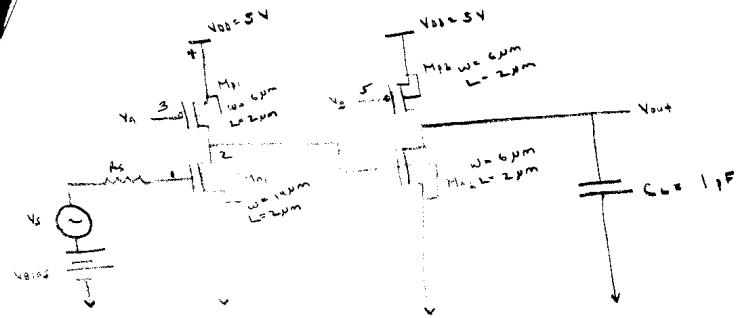
2.3 Lengths and Widths

The final adjustments involved the lengths and the widths of the 4 MOSFETS. For the PMOS transistors, keeping the dimensions close to the minimum configurations seemed optimal. The widths were kept at their minimum (6 μm) and the length was chosen in such a way that there was a ratio of 3:1.

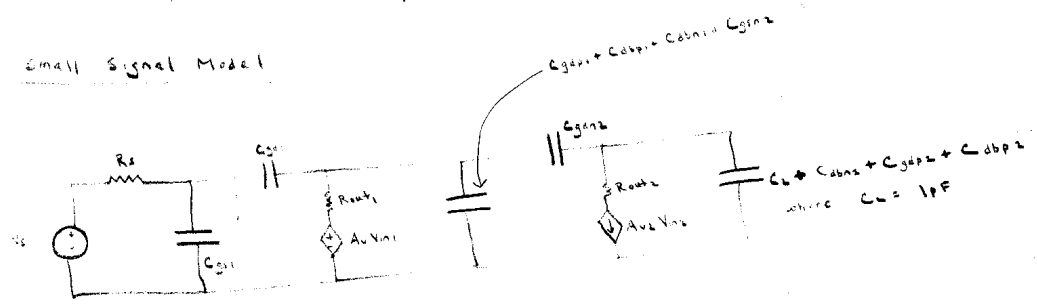
For the NMOS transistors, on the other hand, there was greater flexibility. We found that increasing the width further increased the 3 dB frequency as well as the overall gain because increasing the width increases C_a . As C_a increases, the time constants are closer in value, increasing $w(3dB)$.

Again a good report! - a bit
long though.

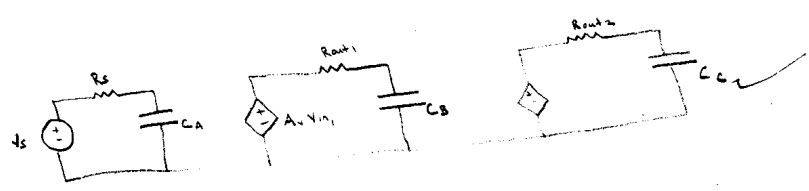
Final Circuit



Small Signal Model



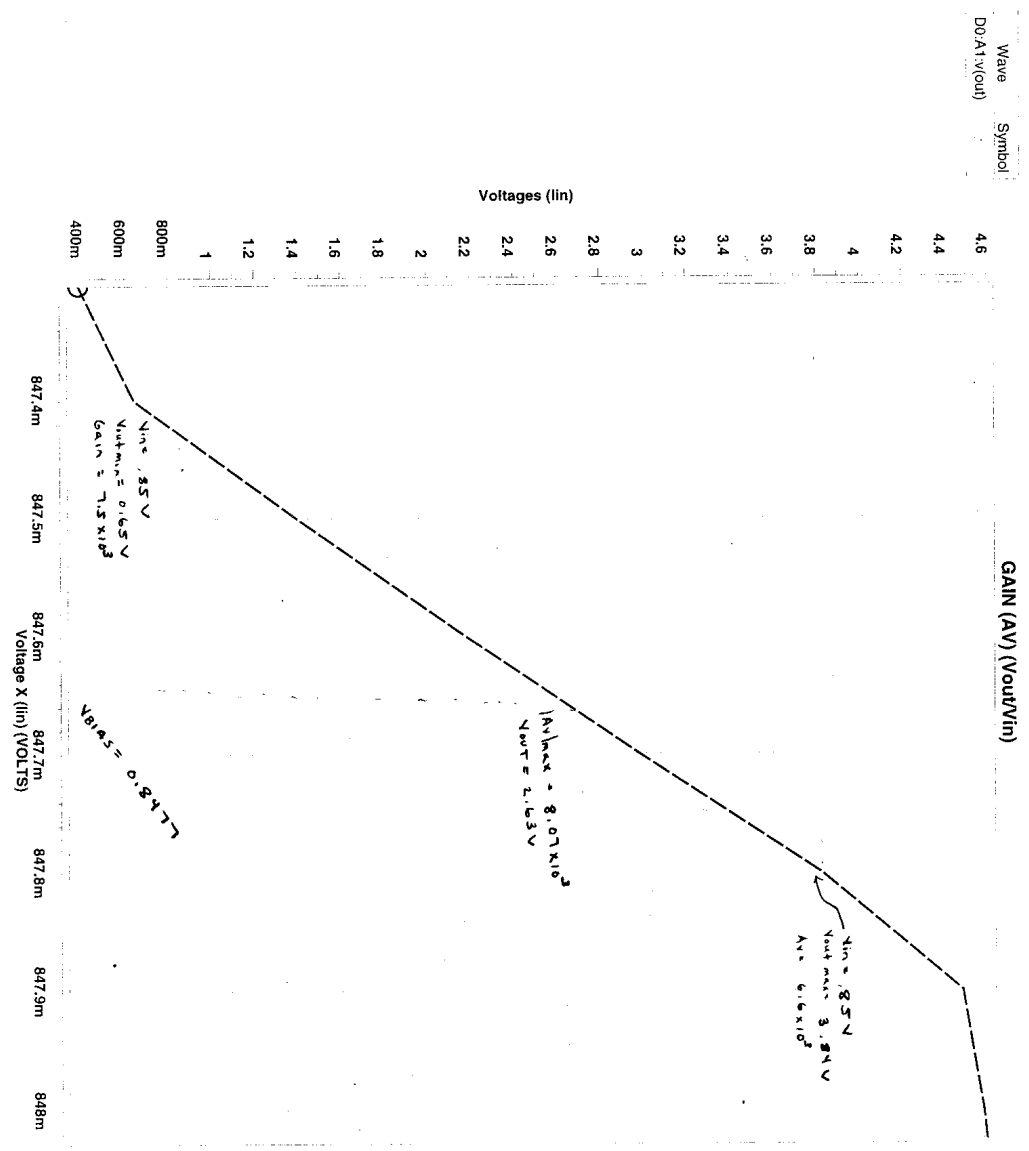
Miller Approximation



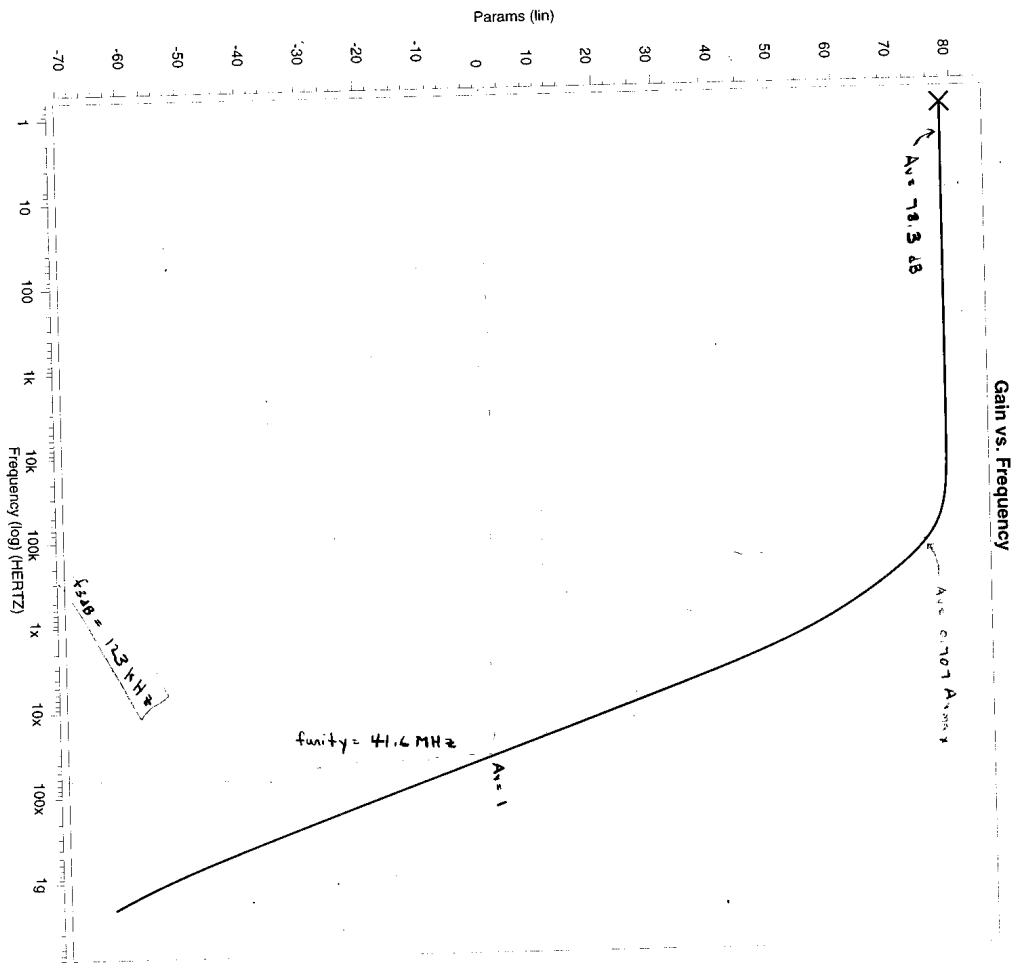
$$C_A = C_{gs1} + C_{gd1} (1 - A_{v1})$$

$$C_B = C_{gs2} + C_{osp} + C_{db1} + C_{gs2} + C_{gd2} (1 - A_{v2}) + C_{gd1} \left(\frac{1}{1 - A_{v1}} \right)$$

$$C_C = C_L + C_{db2} + C_{gs2} + C_{gd2} \left(\frac{1}{1 - A_{v2}} \right)$$



Wave	Symbol
D0:A0.par(mag)	-



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*****
***** Code for Project2 *****
*****

.options post
.op

***** N and P MOS definitions *****

.MODEL NMOS NMOS LEVEL=1 VTO=0.7 TOX=1.7E-08 UO=250
+ LAMBDA=5E-02 GAMMA=0.6 CGSO=5E-10 CGDO=5E-10 CJ=1E-04
+ CJSW=5E-10 PB=0.95

.MODEL PMOS PMOS LEVEL=1 VTO=-0.7 TOX=1.7E-08 UO=125
+ LAMBDA=5E-02 GAMMA=0.6 CGSO=5E-10 CGDO=5E-10 CJ=3E-04
+ CJSW=3.5E-10 PB=0.9

***** initial resistor *****
Resistor 1 in 1k

***** first gate *****
Minv1 2 1 0 0 NMOS L=1.5u W=10.5u pd=26u ps=26u ad=84p as=84p
Minv2 2 3 4 4 PMOS L=1.5u W=4.5u pd=18u ps=18u ad=36p as=36p

***** second gate *****
Minv3 out 2 0 0 NMOS L=1.5u W=4.5u pd=18u ps=18u ad=36p as=3p
Minv4 out 5 4 4 PMOS L=1.5u W=4.5u pd=18u ps=18u ad=36p as=36p

***** Capacitor at end of circuit *****
Capacitor out 0 1p

***** Voltages *****

Vin in 0 ac 1 dc 1
Vdd 4 0 dc 5

Va 3 0 dc 4
Vb 5 0 dc 3.7

.ac dec 40 1 40g
.dc vin 0.5 1 0.0001

***** Measurements *****

.MEASURE AC VMAX MAX V(out)
.MEASURE AC F3DB WHEN V(out)='VMAX*.707' FALL=1
.MEASURE AC funity when v(out)='vmax/vmax' fall=1

.print ac mag=par('20*log10(v(out))')

.end

```

```

total voltage source power dissipation= 95.9353u watts
*****
***** ac analysis tnom= 25.000 temp= 25.000
*****
vmax= 8.2192E+03 at= 1.0000E+00
from= 1.0000E+00 to= 4.2170E+10
f3db= 1.2320E+05
funity= 4.1737E+07
**** job concluded
***** Star-HSPICE -- 2000.2 (20000615) 00:08:04 12/08/2000 solaris
*****
***** job statistics summary tnom= 25.000 temp= 25.000
*****
total memory used 198 kbytes
# nodes = 8 # elements= 10
# diodes= 0 # bjts = 0 # jfets = 0 # mosfets = 4
analysis time # points tot. iter conv.iter
op point 0.02 1 11
dc sweep 2.03 5001 10036
ac analysis 0.07 426 426
readin 0.04
errchk 0.01
setup 0.00
output 0.02
total cpu time 2.20 seconds
job started at 00:08:04 12/08/2000
job ended at 00:08:07 12/08/2000

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lic: Release hspice token(s)

Formula Sheet

These formulas were inputted to an Excel Spreadsheet, allowing for us to calculate all the parameters in parallel. The excel spreadsheet with the final values for all parameters is included.

$$W_{3dB} = \frac{1}{2\pi \zeta \tau}$$

$$\gamma_A = CA R_s$$

$$\gamma_B = CB R_{out1}$$

$$\gamma_C = CC R_{out2}$$

$$R_{out1} = \frac{1}{(\lambda_{o1} + \lambda_{p1}) I_{o1}} = \frac{7.5}{I_{o1}}$$

$$R_{out2} = \frac{1}{(\lambda_{o2} + \lambda_{p2}) I_{o2}} = \frac{7.5}{I_{o2}}$$

$$R_s = 1k\Omega$$

$$C_{gen1} = \frac{2}{3} W_{n1} L_{n1} C_{ox} + W_{n1} C_{ov}$$

$$C_{gd1n1} = W_{n1} C_{ov}$$

$$C_{gs1p1} = W_{p1} C_{ov}$$

$$C_{db1n1} = (W_{p1} L_{d1}) C_{j1} + (W_{p1} + 2L_{d1}) C_{jswp1}$$

$$C_{db1p1} = (W_{n1} L_{d1}) C_{j1} + (W_{n1} + 2L_{d1}) C_{jswn1}$$

$$C_{gs2n2} = \frac{2}{3} W_{n2} L_{n2} C_{ox} + W_{n2} C_{ov}$$

$$C_{gd2n2} = W_{n2} C_{ov}$$

$$C_L = 1pF$$

$$C_{db2n2} = (W_{n2} L_{d2}) C_{j2} + (W_{n2} + 2L_{d2}) C_{jswn2}$$

$$C_{gs2p2} = W_{p2} C_{ov}$$

$$C_{db2p2} = (W_{p2} L_{d2}) C_{j2} + (W_{p2} + 2L_{d2}) C_{jswp2}$$

$$C_{gd2n2} = W_{n2} C_{ov}$$

$$V_{min} = V_{GS} - V_T$$

$$= 0.838 - 0.7$$

$$= 0.138$$

$$V_{swing} = V_{max} - V_{min}$$

$$3.84 - 0.138$$

How did you find

$V_{max}?$

-3