

SUPERPOSITION OF PHASORS-MULTIPATH

Transmitters radiate $E \cos \omega t$:

$$\cos \omega t + \cos (\omega t + \phi) = 2 \cos (\omega t + \phi/2) \cos (\phi/2)$$

{Since $\cos \alpha + \cos \beta = 2 \cos([\alpha + \beta]/2) \cos([\alpha - \beta]/2)$ }

$A + B/C/D =$

B	$\phi = 0$	\Rightarrow	$2 \cos \omega t$
C	$\phi = \pi$	\Rightarrow	0
D	$\phi = \pi/2$	\Rightarrow	$2^{0.5} \cos (\omega t + [\pi/2])$

Phasors:

$$E(t) = \text{Re} \{ \underline{E} e^{j\omega t} \} = \text{Re} [\text{Re} \{ \underline{E} \} + j \text{Im} \{ \underline{E} \}] [\cos \omega t + j \sin \omega t]$$

A, B	E	0
C	-E	0
D	0	E

L6-1

ANTENNA ARRAYS

Radiation:

$$\underline{E}(r, \theta, \phi) = \sum_i \underline{a}_i \underline{E}_i e^{-jk r_i}$$

$$= \underline{E} \left(\sum_i \underline{a}_i e^{-jk r_i} \right) = (\text{element factor } \underline{E})(\text{array factor})$$

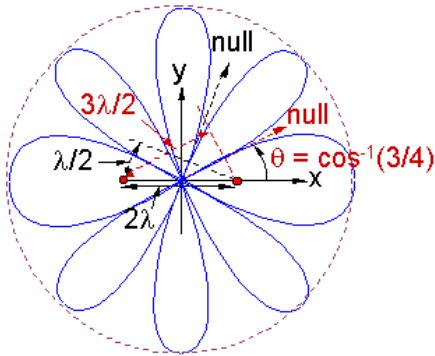
if elements have the same orientation and pattern (so $\underline{E}_i = \underline{E}$), but different locations \underline{r}_i , and amplitudes and phases \underline{a}_i , where \underline{a}_i characterizes the currents driving each radiating element

Example, horizontal arrays of vertical dipoles:

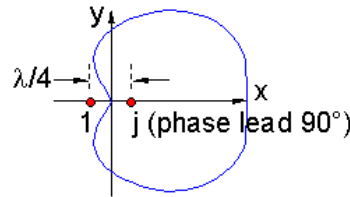
L6-2

MULTI-ELEMENT ANTENNA ARRAYS

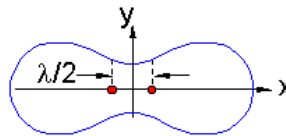
In phase, 2λ separation:



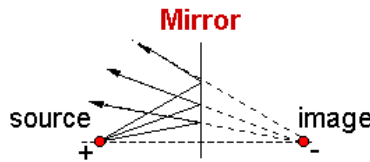
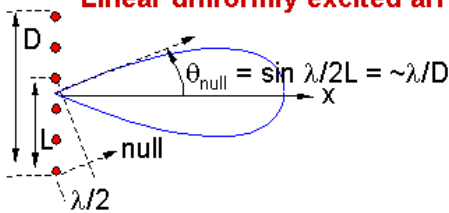
90° phase, $\lambda/4$ separation



**180° phase, $\lambda/2$ separation
unequal sources**

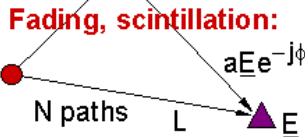


Linear uniformly excited array



L6-3

MULTIPATH EFFECTS



Causes of fading:

- Moving reflectors (trucks, trees) vary ϕ
- Moving sources and receivers
- Variations in c due to temperature, humidity
- Polarization rotation or variation

Examples:

- FM radios in moving cars click during nulls below FM threshold
- Snowy TV broadcast stations waiver as planes fly overhead or trucks pass
- Strength of radio stations varies with the weather (also due to refraction)
- Ionosphere faraday rotates linear polarization ≈ 3 GHz, causing fades

Doppler shift Δf :

If the path L to the source increases at $v = \partial L / \partial t$, we lose

$\Delta f_D = (\partial L / \partial t) / \lambda$ cycles per second = $v / \lambda = f_0 v / c$ Hz, so $f_D = f_0 (1 - v/c)$ Hz

Remedies:

- Doppler shift – retune receiver
- Fading – error-correction codes; space, frequency, polarization diversity

L6-4

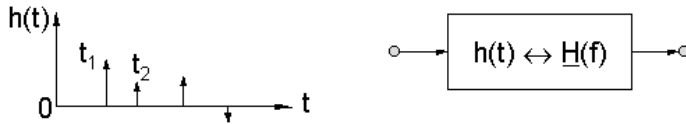
FREQUENCY RESPONSE OF MULTIPATH CHANNELS

Two-path fading:

Sinusoidal fading with frequency, new null as $\Delta(\text{path difference}) = \lambda$
 Null goes to zero if the two strengths are equal

Multipath fading:

Frequency response is square of Fourier transform of multipath impulse response $h(t)$



$$\text{Example: } H(f) = \int_{-\infty}^{+\infty} [\delta(t - t_1) + \delta(t - t_2)] e^{-j\omega t} dt = e^{-j\omega t_1} + e^{-j\omega t_2}$$

$$= e^{-j\omega(t_1+t_2)/2} [e^{j\omega(t_1-t_2)/2} + e^{-j\omega(t_1-t_2)/2}]$$

$$|H(f)|^2 = [2 \cos(\omega[t_1 - t_2]/2)]^2 = 0 \text{ when } \omega_n [t_1 - t_2]/2 = (2n + 1)\pi/2$$

Therefore null frequencies $f_n = \omega_n/2\pi = (n + 1/2)/(t_1 - t_2)$, and therefore

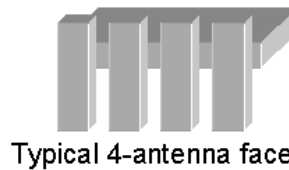
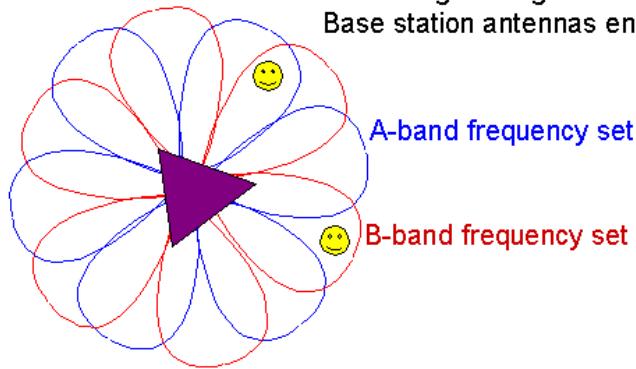
For two paths at t_1, t_2 , Δf between nulls is $1/(t_2 - t_1)$ Hz (1 MHz \leftrightarrow 300 m)

L6-5

FREQUENCY REUSE

Cell phones:

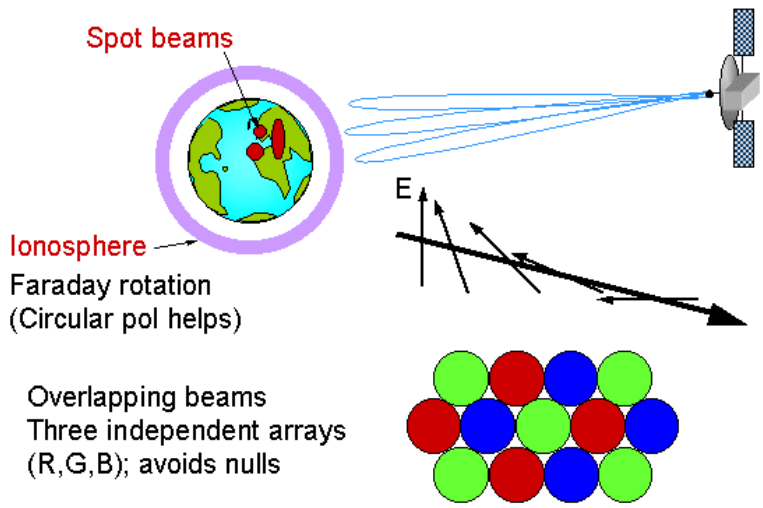
Frequency allocations are limited
 Therefore narrowband signals or otherwise orthogonal signals are used
 Base station antennas enable frequency reuse



Most clients can use non-faded frequencies

L6-6

SATELLITE COMMUNICATIONS SYSTEMS

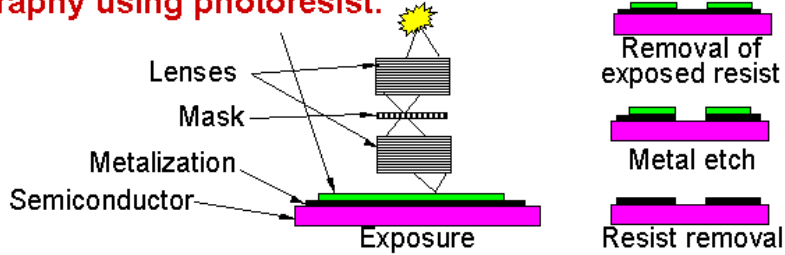


Rain is an increasingly serious problem at frequencies above 2-4 GHz, 99.99% availability \Rightarrow 99.9% \Rightarrow 99% \Rightarrow 90% with increasing frequency ("4 nines", "3 nines", "2 nines", etc.)

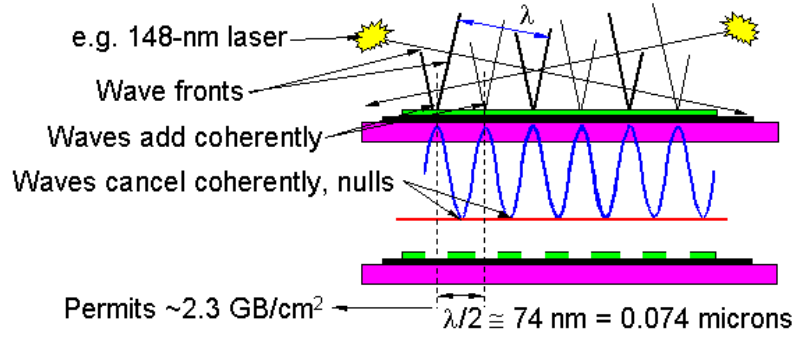
L6-7

WAVE INTERFERENCE X-RAY LITHOGRAPHY

Lithography using photoresist:



Wave Interference Lithography:



L6-8