

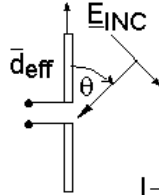
## RECEIVING ANTENNAS

**Recall:**  $A_e(\theta, \phi) = (\lambda^2/4\pi)G(\theta, \phi)$

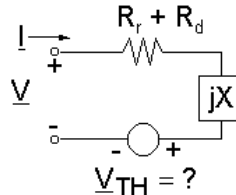
We never proved it; sometimes untrue (when?)

**Proof for Short Dipole Antenna:**

If  $d \ll \lambda/2\pi$ , quasistatics applies



We seek  $V_{Th}$  in equivalent circuit:



**Assume Normally Incident Uniform Plane Wave:**

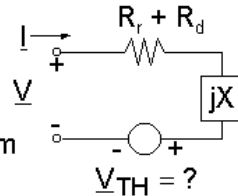
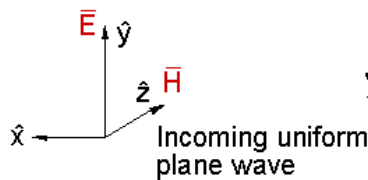
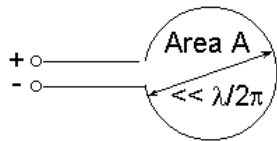
Case 1: small loop antenna ( $D \ll \lambda/2\pi$ )

Case 2: short dipole antenna ( $d \ll \lambda/2\pi$ )

L9-1

### SMALL LOOP ANTENNA: OPEN CIRCUIT VOLTAGE

**Quasistatic Limit:**



Faraday's Law:

$$\nabla \times \vec{E} = -\partial \vec{B} / \partial t \Rightarrow \int_A (\partial \vec{B} / \partial t) \cdot d\vec{a} = \int_C \vec{E} \cdot d\vec{s} = V_{Th}$$

**Open Circuit Voltage:**

$$V_{Th} = A\mu_0 (\partial[\vec{H} \cdot \hat{z}] / \partial t)$$

UPW: Power  $P [W/m^2] = \eta_0 |\vec{H}_0|^2 / 2$

Where:  $\vec{H} = \hat{z}H_0 \cos \omega t$  at  $z = 0$ , and

$$(\partial[\vec{H} \cdot \hat{z}] / \partial t) = -\omega H_0 \sin \omega t$$

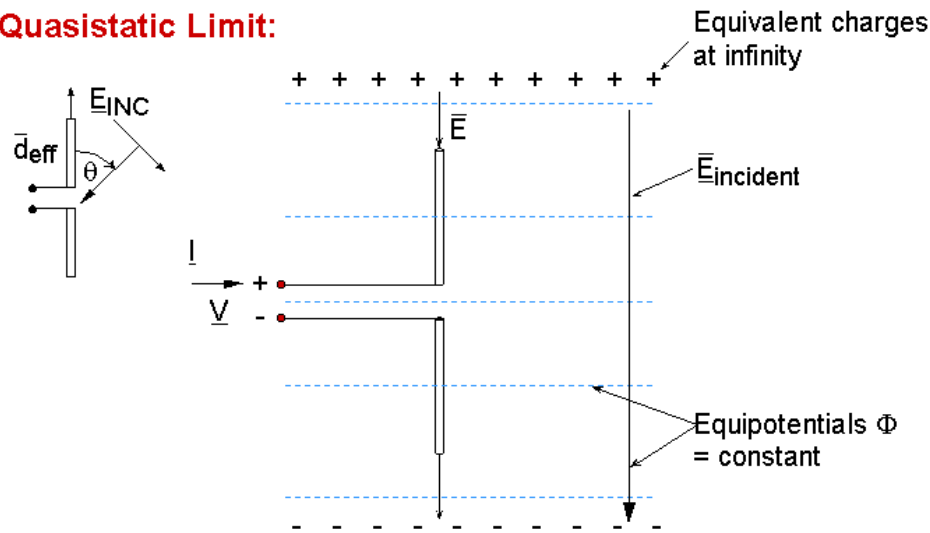
Therefore:  $(\partial[\vec{H} \cdot \hat{z}] / \partial t) = -\omega(2P/\eta_0)^{0.5} \sin \omega t$  and

$$V_{Th} = -A\mu_0 \omega (2P/\eta_0)^{0.5} \sin \omega t$$

L9-2

### SHORT DIPOLE ANTENNA: OPEN CIRCUIT VOLTAGE

**Quasistatic Limit:**

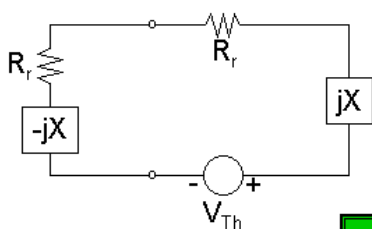


$$V_{Th} = -\vec{E}_{INC} \cdot \vec{d}_{eff} = -\vec{E}_{INC} d_{eff} \sin \theta$$

L9-3

### MAXIMUM POWER EXTRACTABLE FROM A SHORT DIPOLE ANTENNA

**Antenna Equivalent Circuit plus Matched Load:**



$$P_{rec,max} = \frac{1}{2} |V_{Th}/2|^2 / R_r$$

$$= |\vec{E}_{INC}|^2 \frac{d_{eff}^2 \sin^2 \theta}{8R_r}$$

where  $R_r = \eta_0 (kd_{eff})^2 / 6\pi$

$$\text{Define } A_{eff}(\theta, \phi) \triangleq \frac{P_{rec}}{|\vec{E}_{inc}|^2 / 2\eta_0} \text{ "Effective Area"}$$

For short dipole:  $A_{eff}(\theta) = \frac{2\eta_0 P_{rec}}{|\vec{E}_{inc}|^2} = \frac{\eta_0 d_{eff}^2 \sin^2 \theta}{4R_r} = \frac{\lambda^2 3}{8\pi} \sin^2 \theta$

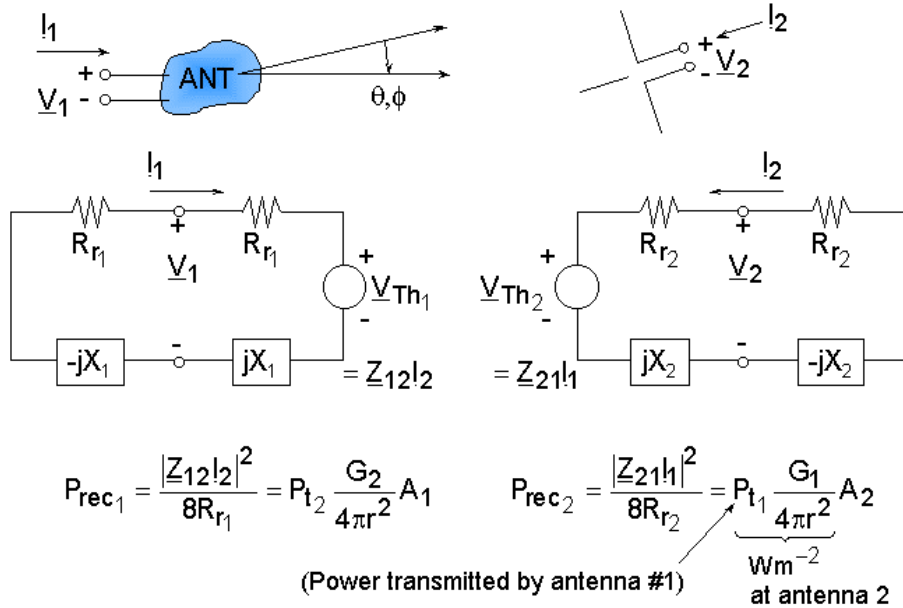
Therefore:  $A_e(\theta, \phi) = \frac{\lambda^2}{4\pi} G(\theta, \phi) (m^2)$  [true for almost all antennas]

Recall, for short dipole:  $G(\theta) = 1.5 \sin^2 \theta$  [ $\neq f(\omega)$ ]

L9-4

### PROOF THAT $A = G\lambda^2/4\pi$ FOR MOST ANTENNAS

Test Range = Unknown plus Short Dipole Antenna:



L9-5

### PROOF THAT $A = G\lambda^2/4\pi$ FOR MOST ANTENNAS (2)

$$P_{rec1} = \frac{|Z_{12}I_2|^2}{8R_{r1}} = P_{t2} \frac{G_2}{4\pi r^2} A_1 \quad P_{rec2} = \frac{|Z_{21}I_1|^2}{8R_{r2}} = P_{t1} \frac{G_1}{4\pi r^2} A_2$$

$$\therefore \frac{P_{rec2}}{P_{rec1}} = \frac{G_1 A_2 P_{t1}}{G_2 A_1 P_{t2}} = \frac{A_1}{G_1} = \frac{A_2}{G_2} \left[ \frac{P_{t1}}{P_{t2}} \cdot \frac{P_{rec1}}{P_{rec2}} \right]$$

$$\text{But } \frac{P_{rec1}}{P_{rec2}} = \frac{|Z_{12}I_2|^2}{|Z_{21}I_1|^2} \cdot \frac{R_{r2}}{R_{r1}} = \frac{|Z_{12}|^2}{|Z_{21}|^2} \cdot \frac{P_{t2}}{P_{t1}}$$

Therefore, if  $|Z_{12}|^2 = |Z_{21}|^2$ , then  $\frac{A_1}{G_1} = \frac{A_2}{G_2} = \frac{\lambda^2}{4\pi}$  Q.E.D.

L9-6

## RECIPROCITY AND NON-RECIPROCAL DEVICES

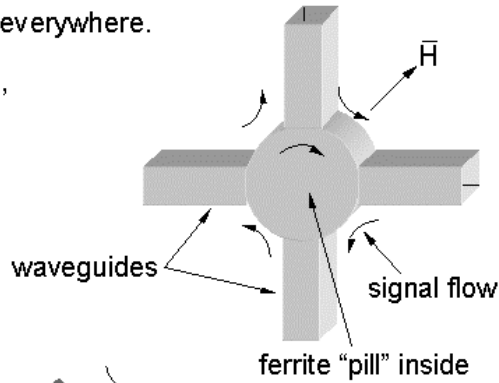
### Reciprocity:

$$|Z_{12}|^2 = |Z_{21}|^2 \text{ if } \vec{\epsilon} = \vec{\epsilon}^t, \vec{\mu} = \vec{\mu}^t \text{ everywhere.}$$

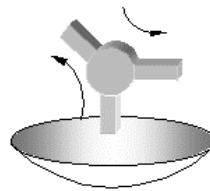
Exceptions: magnetized plasmas, magnetized ferrites

### Non-reciprocal Devices:

4-Port Circulators



### Non-reciprocal Antennas:

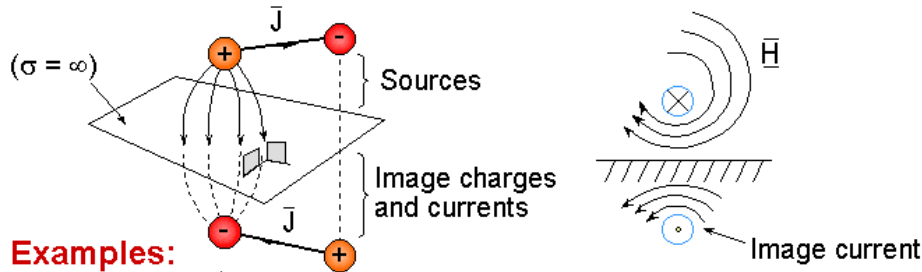


L9-7

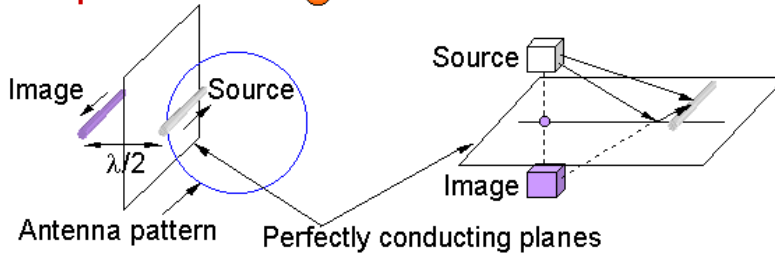
## MIRROR IMAGES

**Mirror Images:** Infinite flat conducting surfaces are "mirrors"

Consider the charges and currents shown, and how  $\vec{E}$  must everywhere be perpendicular to the mirror, and  $\vec{H}$  must be parallel



### Examples:



L9-8