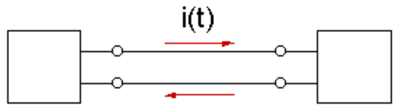
INDUCTORS

Inductance is ubiquitous:



Ampere's Law: $\nabla \times \bar{H} = \bar{J} + \partial \bar{D}/\partial t$

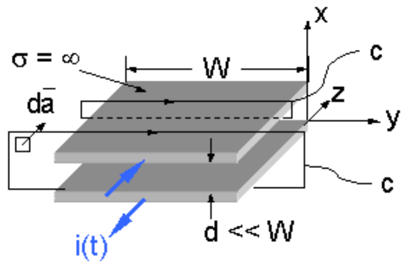
Let $\partial/\partial t \cong 0$

Example—printed circuit:

$\int_c \bar{H} \bullet d\bar{s} = \int_A \bar{J} \bullet d\bar{a}$

= 0 around both wires

= i(t) around the top wire



Magnetic Field H:

Outside: $\bar{H} \cong 0$

Inside: $\bar{H} \cong -\hat{y}i/W$

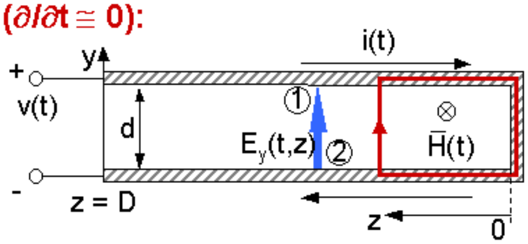
(since d << W we ignore fringing fields)

L11-1

INDUCTANCE

Quasistatic Behavior ($\partial/\partial t \cong 0$):

Side view:



Maxwell's Equations:

Faraday's Law: $\nabla \times \bar{E} = -\partial \bar{B}/\partial t$

$\Rightarrow \int_c \bar{E} \bullet d\bar{s} = -\int_A \mu(\partial \bar{H}/\partial t) \bullet d\bar{a}$

$E_y(t,z)d = -(\mu z d/W)\partial i(t)/\partial t$ [recall H = i/W]

Therefore when z = D: $v(t) = \int_1^2 \bar{E} \bullet d\bar{s} = -E_y d = (\mu D d/W)(\partial i(t)/\partial t)$

Note: Dd = cross-sectional area A

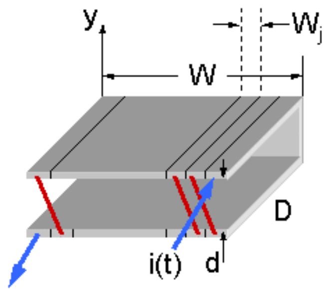
$v(t) = L\, \partial i(t)/\partial t$ where $L = \mu A/W$ Henries

Note: Kirchoff's voltage law not obeyed here; $E_y = f(z)$

L11-2

SOLENOIDAL INDUCTORS

N-Turn Solenoidal Inductor:



$v(t) = \int_1^2 \bar{E} \bullet d\bar{s} = -E_y d = (\mu Dd/W)(\partial i(t)/\partial t)$

$v_j(t) = (\mu Dd/W_j)(\partial i(t)/\partial t)$ for j^{th} turn

But: $W = NW_j$

$v(t) = Nv_j(t)$

Therefore: $v(t) = (N^2 \mu Dd/W)(\partial i(t)/\partial t)$; $Dd = A$

Inductance of N-Turn Solenoid:

$L = N^2 \mu A/W$ Henries

Magnetic Energy Storage:

$W_m = \mu |\bar{H}(t)|^2/2 \quad [\mathrm{J\ m^{-3}}]$

$w_m = \mu DdW |\bar{H}(t)|^2/2 = \mu AW(Ni/W)^2/2$ [J] [recall $H = Ni/W$]

Therefore: $w_m = Li^2(t)/2$ [J]

L11-3

RESISTIVE INDUCTORS

Single-Turn Inductor:

Conductance of slab of cross-sectional area S: σS =[Siemens m]

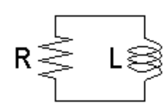
Resistance of slab of length D: $D/\sigma S$ [ohms]

Resistance of a single-turn inductor: $2(D + d)/\sigma S$ [ohms]

Resistance of an N-turn inductor: $2N(D + d)/\sigma(S/N) = 2N^2(D + d)/\sigma S$

L/R Time Constant of Solenoidal Inductor:

$\tau = L/R$ seconds (e.g. $i(t) = i_o e^{-t/\tau}$)

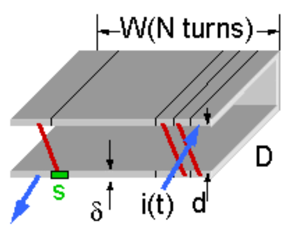


$= (N^2 \mu A/W)/(2N^2(D+d)/\sigma S) \cong \mu d\delta\sigma/2N$

where $D >> d$, $S = \delta(W/N)$, $A = Dd$

For finite size and mass, τ is limited

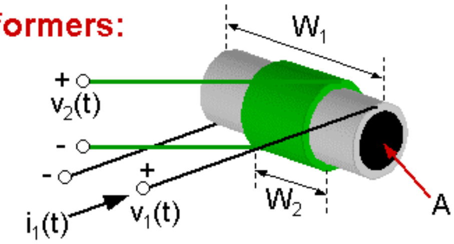
Want $d \to D$, $\delta \tilde{\to} d/3$, $N \to 1$, $d \to W$



L11-4

TRANSFORMERS

Air-Wound Solenoidal Transformers:



$\int_c \bar{E} \bullet d\bar{s} = -\int_A \mu (\partial \bar{H}/\partial t) \bullet d\bar{a}$

Say $A_1 = A_2$, $W_1 = W_2$ here
N_i = number of turns in coil i

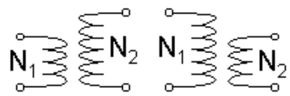
Therefore:

The voltage induced in one turn of coil 2 is the same as induced in one turn of coil 1,

And the total voltage induced in coil 2 is N_2/N_1 times the total voltage induced in coil 1, regardless of whether it is generated by i_1 or i_2.

N_2/N_1 is called the transformer turns ratio

Step-up and Step-down Transformers:



Step-up or step-down the output voltage, correspondingly.
The flux coupling between the two coils may be imperfect and the output voltage is correspondingly reduced

[flux $\Lambda = \mu HA$, and linked flux = $N\mu HA$].

L11-5

IRON-CORE TRANSFORMERS (1)

Boundary Conditions:

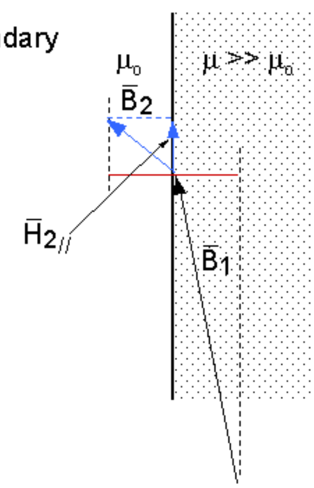
$H_{//}$ and $\bar{B}_\perp$ are continuous across the boundary
$(\nabla \times \bar{H} = \bar{J} + \partial \bar{D}/\partial t;\ \nabla \bullet \bar{B} = 0)$

$\bar{H} // \bar{B}$ and $\bar{B} = \mu \bar{H}$

μ/μ_o can be as large as 10^6.

Since $\mu >> \mu_o$, $\bar{B}_1$ is essentially parallel to the interface, and trapped within the high permeability medium.

The magnetic flux $\bar{B}$ is "trapped" inside.

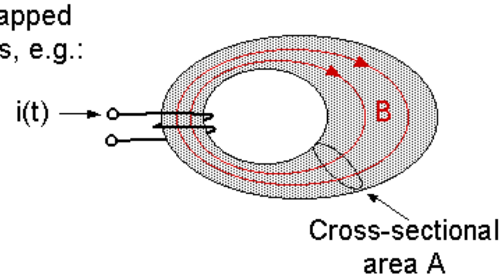


L11-6

IRON-CORE TRANSFORMERS (2)

Flux trapping inside high permeability materials:

The magnetic flux density $\overline{B}$ is trapped inside high-permeability materials, e.g.:

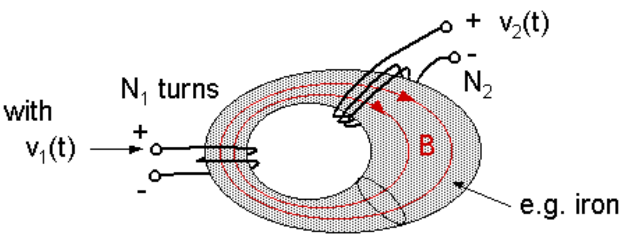


Flux $\Lambda = \int_A \overline{B} \bullet d\overline{a} \cong$ constant

Transformer Output:

$v_2(t) = (N_2/N_1)v_1(t)$

The flux is highly linked with little leakage



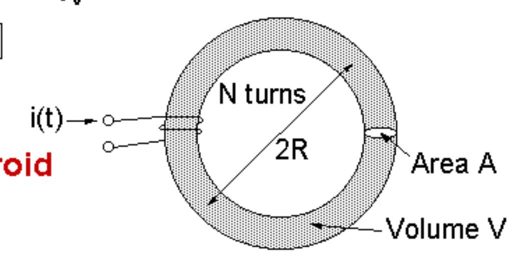
L11-7

INDUCTANCE OF IRON TOROID (1)

Inductance L of N turns around toroid ($N_2 = 0$):

Recall: $w_m = Li^2(t)/2 = \int_V W_m dv \;\; [J] = \int_V \left(\mu|\overline{H}|^2/2\right) dv$

where $W_m = \mu|\overline{H}(t)|^2/2 \;\; \left[Jm^{-3}\right]$



Example: Constant Area Toroid

Since:

$$L = \left(\mu\int_V |\overline{H}(t)|^2 dv\right)/i^2(t)$$

$$\nabla \times \overline{H} = \overline{J} + \partial\overline{D}/\partial t \Rightarrow \int_c \overline{H} \bullet d\overline{s} \cong Ni(t)$$

($\partial\overline{D}/\partial t \cong 0$)

Therefore:

$2\pi R|\overline{H}| \cong Ni$ (R varies slightly over A)

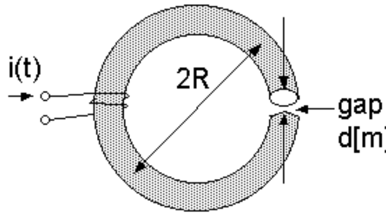
$$L = \mu\int_V (N/2\pi R)^2 dv \cong \mu(N/2\pi R)^2 V = \mu N^2 A/2\pi R \;\; [\text{Henries}]$$

where $V \cong 2\pi RA\left[m^3\right]$

L11-8

INDUCTANCE OF IRON TOROID (2)

Inductance L of a toroid with a gap:



Recall: $w_m = Li^2(t)/2 = \int_V W_m dv$ [J]

where $W_m = \mu|\overline{H}(t)|^2/2$ $[Jm^{-3}]$

Therefore: $L = \left(\mu\int_V |\overline{H}(t)|^2 dv\right)/i^2(t)$, as before

Finding $|\overline{H}(t)|$:

Since: $\int_c \overline{H} \bullet d\overline{s} \cong Ni(t)$

Therefore: $|\overline{H}_\mu|(2\pi R - d) + |\overline{H}_{\mu_o}|d \cong Ni(t)$

But $\nabla \bullet \overline{B} = 0$, so $\mu_o H_o = \mu H$ where we assume $\mu >> \mu_o$

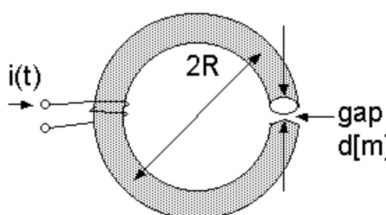
Therefore: Magnetic energy density in gap is $(\mu/\mu_o)^2$ greater than inside the torus, and dominates unless $(\mu/\mu_o)^2 << 2\pi R/d$

(we require $d \lesssim 2\pi R(\mu_o/\mu)^2$)

L11-9

INDUCTANCE OF IRON TOROID (3)

Inductance L of a toroid with a gap:



Recall: $L = \left(\mu(t)\int_V |\overline{H}|^2 dv\right)/i^2$

$|\overline{H}_\mu|(2\pi R - d) + |\overline{H}_{\mu_o}|d \cong Ni(t)$

Where: $|\overline{H}_{\mu_o}|d \cong Ni(t)$ for a small gap with little fringing ($d << A^{0.5}$) and we neglect the energy storage inside the torus

Therefore: $L \cong \mu A d (N/d)^2$ or, for a small-gap torus:

$$L \cong \mu_o AN^2/d \quad \text{Henries}$$

provided that $d \lesssim 2\pi R(\mu_o/\mu)^2$

L11-10