

## GUIDED WAVES

### Applications:

- Low-loss transport: Microwave and optical signals
  - within and between systems
- In devices: Resonators, amplifiers, isolators, optical switches etc.

### Standing Waves:

- Free space: Waves at any  $\omega$ , angle, and polarization
- Single planar reflector: Same, plus reflected wave
  - forms periodic parallel null planes
- Parallel-plate waveguide: Same, but the spatial structure depends on  $\omega$ 
  - only fields with properly positioned null planes propagate

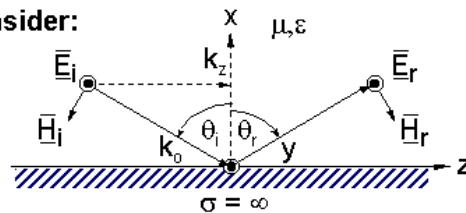
**Today:** Restricted to TE, TM reflected waves  
 Yields discrete modes, each propagating a continuum of  $\omega$

L17-1

## TE MODES IN PARALLEL-PLATE GUIDES

### Single Reflected Wave:

Consider:



$$\vec{E}_i = \hat{y}E_0 e^{jk_x x - jk_z z}$$

$$\vec{E}_r = -\hat{y}E_0 e^{-jk_x x - jk_z z}$$

$\mapsto$  Note:  $\vec{E}_i + \vec{E}_r = 0$  @  $x = 0$  is our Boundary Condition "B.C."

B.C. also requires  $k_z$  be the same, and therefore  $k_x$

$$\theta_i = \theta_r = \sin^{-1}(k_z/k_0) \text{ where } k_x^2 + k_z^2 = k_0^2 = \omega^2 \mu \epsilon$$

### Waveguide Solution:

Recall:  $\sin \alpha \equiv \frac{e^{j\alpha} - e^{-j\alpha}}{2j}$ , since:  $\vec{E} = \vec{E}_i + \vec{E}_r$ ,

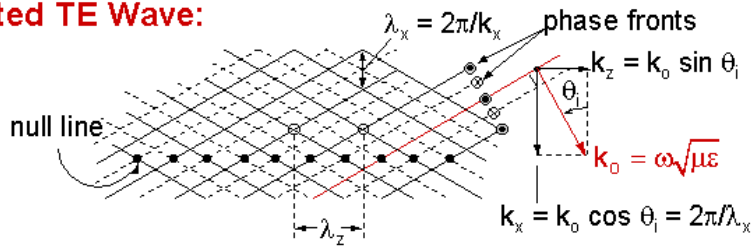
Therefore:  $\vec{E} = \hat{y}E_0 [2j \sin k_x x e^{-jk_z z}]$       Since:  $\vec{H} = \frac{\nabla \times \vec{E}}{-j\omega\mu}$ ,

Therefore:  $\vec{H} = \frac{1}{-j\omega\mu} [2k_x \cos k_x x + \hat{x}j k_z \sin k_x x] \cdot 2jE_0 e^{-jk_z z}$

L17-2

## NULL PATTERNS FOR STANDING WAVES

### Reflected TE Wave:



### Waveguide Wavelength:

$$\lambda_z = 2\pi/k_z \triangleq \lambda_g$$

Since:  $d = m(\lambda_x/2) = m\pi/k_x$  where  $d$  is waveguide plate separation

Therefore:  $k_x = m\pi/d$

### TE Modes:

$TE_m$  :  $TE_1, TE_2, \dots, TE_m, \dots$  ( $TM_0 \equiv TEM$ )

$TE_0$  does not exist because all  $\vec{E} = \vec{H} = 0$  to match boundary conditions

L17-3

## FIELD SKETCHES FOR TE MODES

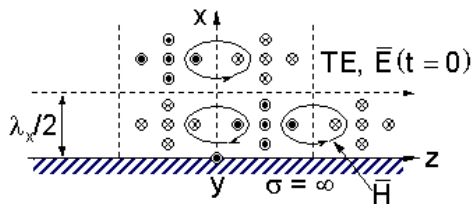
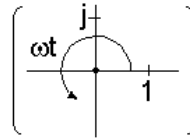
**Time-Domain Field Expressions:**  $\vec{E}(t) = \text{Re} \{ \vec{E} e^{j\omega t} \}; \vec{H}(t) = \text{Re} \{ \vec{H} e^{j\omega t} \}$

Where:  $\vec{E} = \hat{y} E_0 [ 2j \sin k_x x e^{-jk_z z} ]$  [from L17-2]

$$\vec{H} = \frac{1}{-j\omega\mu} [ \hat{z} k_x \cos k_x x + \hat{x} j k_z \sin k_x x ] \cdot 2j E_0 e^{-jk_z z}$$

### Electric Field Sketches:

Therefore:  $\vec{E}(t) = -2\hat{y} E_0 \sin k_x x \cdot \sin(\omega t - k_z z)$



### Field Motion, Propagation:

For a fixed argument:  $\frac{d}{dt}(\omega t - k_z z) = 0 \Rightarrow \frac{dz}{dt} = \omega/k_z$

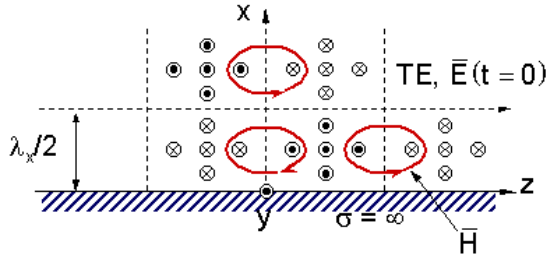
Phase velocity:  $v_p = \omega/k_z = \omega/(k_0 \sin \theta_1) > c$

L17-4

## FIELD SKETCHES FOR TE MODES (2)

### Magnetic Field Expressions:

$$\vec{H}(t) = \hat{z}2E_0 \left( \frac{-k_x}{\omega\mu} \right) \cos k_x x \cdot \cos(\omega t - k_z z) + \hat{x}2E_0 \left( \frac{k_z}{\omega\mu} \right) \sin k_x x \cdot \sin(\omega t - k_z z)$$



### Test Boundary Conditions:

$$E_{//}, \vec{H}_{\perp} = 0 \text{ at } x = 0, k_x x = m\pi (m = 0, 1, 2, \dots)$$

Therefore we can put waveguide walls at  $x = 0, d = m\pi/k_x = m\lambda_x/2$

L17-5

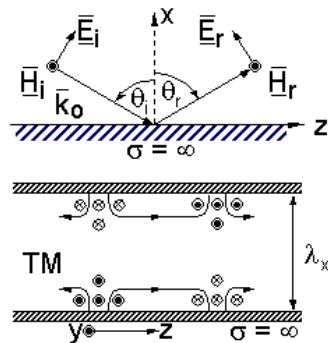
## TM WAVEGUIDE MODES

### Magnetic Fields:

$$\vec{H}_i = \hat{y}H_0 e^{jk_x x - jk_z z}$$

$$\vec{H}_r = \hat{y}H_0 e^{-jk_x x - jk_z z}$$

$$\vec{H} = \vec{H}_i + \vec{H}_r = \hat{y}H_0 2 \cos k_x x e^{-jk_z z}$$



### Electric Field Expressions:

$$\vec{E} = (\nabla \times \vec{H}) / j\omega\epsilon$$

$$= 2\eta H_0 \left( \hat{x} \frac{k_z}{k_0} \cos k_x x + \hat{z} \frac{jk_x}{k_0} \sin k_x x \right) e^{-jk_z z}$$

### TM Modes:

$$TM_0, TM_1, \dots k_x x = m\pi (m = 0, 1, 2, \dots)$$

$$[TM_0 \cong TEM]$$

L17-6

## MODAL CUT-OFF FREQUENCIES

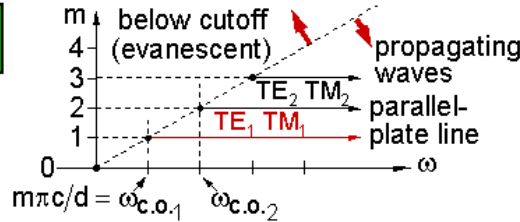
### Cut-Off Frequencies:

$$k_{zm} = \sqrt{k_0^2 - k_x^2} = \sqrt{\underbrace{k_0^2}_{(\omega/c)^2} - \underbrace{\left(\frac{m\pi}{d}\right)^2}} = \pm j\alpha \text{ if } \frac{m\pi}{d} > k_0 = \frac{\omega}{c} = \omega\sqrt{\mu\epsilon}$$

discrete "evanescent wave"  $\leftrightarrow \omega < m\pi c/d = \omega_{c.o.m}$

$k_z = 0$  at  $\omega_{c.o.}$  "cut-off frequency"

Note: discrete modes, each at a continuum of possible  $\omega$ 's



### Phase Velocity $v_p$ Above Cut-Off:

$$v_{pm} = \omega/k_{zm} = \omega/\sqrt{(\omega/c)^2 - (m\pi/d)^2}$$

$v_{pm} \rightarrow \begin{cases} c, \omega \rightarrow \infty \\ \infty, \omega \rightarrow c.o.m \end{cases}$

L17-7

## MODAL CUT-OFF FREQUENCIES (2)

### Group Velocity $v_g$ Above Cut-Off:

$$k_{zm} = \sqrt{k_0^2 - k_x^2} = \sqrt{\underbrace{k_0^2}_{(\omega/c)^2} - \left(\frac{m\pi}{d}\right)^2}$$

$$v_{gm} = (\partial k_{zm}/\partial \omega)^{-1} = \left\{ \frac{\partial}{\partial \omega} \left[ \left(\frac{\omega}{c}\right)^2 - \left(\frac{m\pi}{d}\right)^2 \right]^{0.5} \right\}^{-1} = c \left[ 1 - \left(\frac{m\pi c}{\omega d}\right)^2 \right]^{1/2}$$

$v_{gm} \rightarrow \begin{cases} c, \omega \rightarrow \infty \\ 0, \omega \rightarrow \omega_{c.o.m} \end{cases}$

Here,  $v_p v_g = c^2$

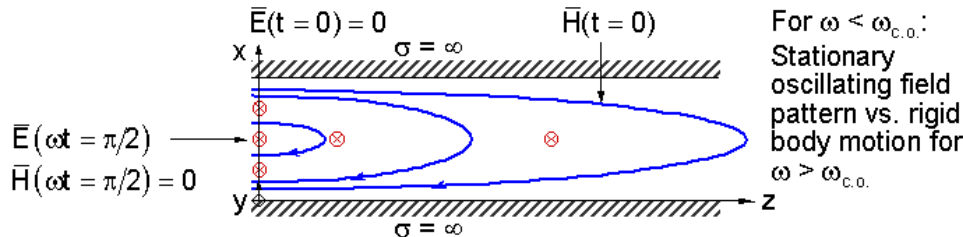
L17-8

## EVANESCENT TE MODES

### Evanescent TE<sub>1</sub> Mode Fields:

Recall:  $\vec{E} = \hat{y} 2jE_0 \sin k_x x e^{-jk_z z}$  where  $\begin{cases} k_z = \sqrt{k_0^2 - (\pi/d)^2} = \pm j\alpha \\ e^{-j(\pm j\alpha)z} = e^{-\alpha z} \Rightarrow "-j\alpha" = k_z \end{cases}$

Therefore:  $\vec{E}(t) = \text{Re} \{ \vec{E} e^{j\omega t} \} = \hat{y} 2E_0 \sin k_x x (-\sin \alpha t) e^{-\alpha z}$



### Evanescent TE<sub>1</sub> Magnetic Fields:

Similarly:  $\vec{H} = \frac{\nabla \times \vec{E}}{-j\omega\mu} = \frac{j}{\omega\mu} [\hat{z} k_x \cos k_x x + \hat{x} \alpha \sin k_x x] \cdot 2jE_0 e^{-\alpha z}$

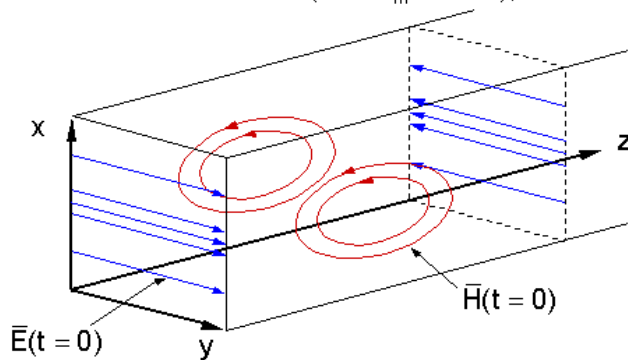
$\vec{H}(t) = -\frac{2E_0}{\omega\mu} [\hat{z} k_x \cos k_x x + \hat{x} \alpha \sin k_x x] \cos \alpha t e^{-\alpha z}$

L17-9

## TE<sub>10</sub> MODE IN RECTANGULAR WAVEGUIDE

### Add Sidewalls to TE<sub>1</sub> Waveguide:

Note: can add  $\sigma = \infty$  sidewalls! (for TE<sub>m</sub> modes), eliminates fringing fields



Note:

**Surface Charge:** Use  $\nabla \cdot \vec{D} = \rho_s$

$\vec{E} \perp (\sigma = \infty)$ ,  $\vec{H} \parallel (\sigma = \infty)$

**Surface Current:** Use  $\vec{J}_s = \hat{n} \times \vec{H}$

$\vec{E} \times \vec{H}$  in  $+\hat{z}(\pm\hat{x})$  direction

Evanescent waves for  $\omega < \omega_{c.o.}$

L17-10