

## VARIABLE RELUCTANCE MOTORS

### Basic 2-Pole Reluctance Motor:

What is the torque on the rotor?

#### First find B and H:

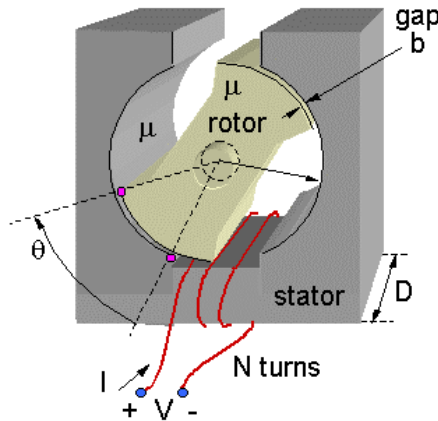
Since  $\nabla \cdot \vec{B} = 0$ , then  $\vec{B}_{\text{stator}} \cong \vec{B}_{\text{gap}}$   
 and  $\vec{H}_{\text{stator}} \cong (\mu_0/\mu)\vec{H}_{\text{gap}} \ll \vec{H}_{\text{gap}}$   
 ( $\mu \cong 10^4 \mu_0$ )

$$\nabla \times \vec{H} = \vec{J} \Rightarrow$$

$$NI = \int_c (\vec{H}_{\text{gap}} + \vec{H}_{\text{stator}}) \cdot d\vec{s} \cong 2bH_{\text{gap}}$$

$$\text{Therefore } H_{\text{gap}} \cong NI/2b$$

(independent of rotor cross-sectional area)



L22-1

## VARIABLE RELUCTANCE MOTORS (2)

### Find Torque T[Nm] by Differentiating Energy Storage:

Since:  $W_m \propto \mu |H|^2 / 2 [Jm^{-3}]$  and  $\vec{H}_{\text{stator}} \cong (\mu_0/\mu)\vec{H}_{\text{gap}}$

Therefore:  $W_{\text{gap}} \cong (\mu/\mu_0)W_{\text{stator}} [Jm^{-3}]$

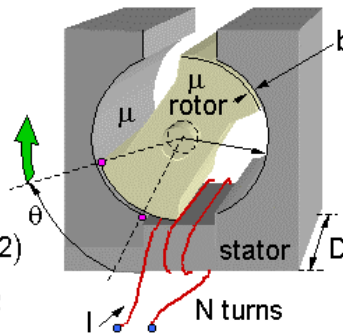
So if:  $b/2R \ll \mu_0/\mu$

Then:  $w_{\text{gap}} \gg w_{\text{stator}} [J]$  where

$$w_{\text{gap}} \cong 2bR\theta D \mu_0 |H_{\text{gap}}|^2 / 2$$

Where: Gap area =  $R\theta D [m^2]$  (for  $0 < \theta < \pi/2$ )

$$\text{Therefore(?): } T = -\partial w_{\text{gap}} / \partial \theta = -bRD\mu_0 |H_{\text{gap}}|^2$$



**WRONG SIGN!**

To find force we must always differentiate total energy, including the energy in the power supply!

### To Find Torque Correctly:

Can include the changing source energy, but easier to reformulate the energy expression

L22-2

## FLUX LINKAGE $\Lambda$ AND INDUCTANCE $L$

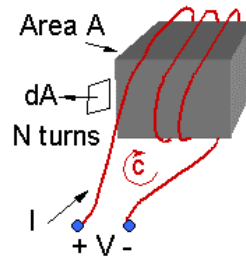
### Definition of Flux Linkage $\Lambda$ :

$$\text{Flux Linkage } \Lambda = N \int_A \vec{B} \cdot d\vec{a}$$

$$-\nabla \times \vec{E} = \partial \vec{B} / \partial t = N \int_A (d\vec{B} / dt) \cdot d\vec{a} = d\Lambda / dt$$

$$-\int_{\text{c coil}} \vec{E} \cdot d\vec{s} = V = \frac{d\Lambda}{dt} = L di / dt$$

Therefore:  $L = \Lambda / i$



### Reluctance-Motor Flux Linkage $\Lambda$ :

$V = d\Lambda / dt = 0$  if motor short-circuited; therefore

$\Lambda = \text{constant} \neq f(\theta)$  (key step)

$\Lambda = N\mu_0 H_{\text{gap}} A_{\text{gap}} = N^2 \mu_0 I A_{\text{gap}} / 2b$ , where  $H_{\text{gap}} = NI / 2b$  [see L22-1]

$A_{\text{gap}} = R D \theta$  here [L22-2]

$L = \Lambda / I = N^2 \mu_0 A_{\text{gap}} / 2b$

L22-3

## RELUCTANCE MOTOR TORQUE

### Energy Storage and Torque with the Source Short-Circuited:

$$w_m = LI^2 / 2 = \Lambda^2 / 2L \quad (I = \Lambda / L)$$

$$T = -\partial w_m / \partial \theta = -\Lambda^2 \partial (1/2L) / \partial \theta = -\Lambda^2 \partial (b / N^2 \mu_0 A_{\text{gap}}) / \partial \theta \quad [A_{\text{gap}} = R\theta D]$$

$$= -(\Lambda^2 b / N^2 \mu_0 R D) \partial \theta^{-1} / \partial \theta = \Lambda^2 b / N^2 \mu_0 R D \theta^2$$

Recall  $\Lambda = N^2 \mu_0 I A_{\text{gap}} / 2b$  [see L22-3]

$$T = (N^2 \mu_0 I R \theta D / 2b)^2 b / N^2 \mu_0 R D \theta^2$$

Therefore:

$$T = N^2 \mu_0 I^2 R D / 4b \text{ [Nm]} = (\mu_0 H_{\text{gap}}^2 / 2) (2b R D) \neq f(\theta) \quad (\text{e.g. for } 0 < \theta < \pi/2)$$

$$T = W_{\text{mgap}} (dV_{\text{olume}} / d\theta) \text{ [Nm]}$$

~Same as for electric motors!

T is limited by maximum energy density

Maximize T: maximize  $(NI)^2$  and RD (~weight), minimize b (tolerances)

### Motor Drive Circuit:

I is turned on when  $A_{\text{gap}}$  is minimum; torque then increases  $A_{\text{gap}}$  as the rotor is pulled by the stator. When  $A_{\text{gap}} = \text{maximum}$ , I is set to zero and the rotor coasts until  $A_{\text{gap}} = \text{minimum}$ , and the cycle repeats. (<50% duty cycle here)

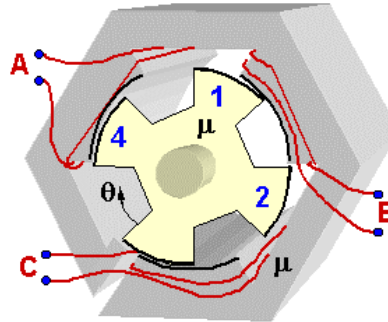
L22-4

## 3/4-POLE VARIABLE RELUCTANCE MOTOR

### Winding Excitation Plan:

Start by exciting windings A,B; this pulls pole 1 into pole B; for winding A, the pole area is temporarily constant. When  $\Delta\theta = \pi/3$ , the currents are switched to B,C; when  $\Delta\theta = 2\pi/3$  we excite C,A. Repeating this cycle results in nearly constant clockwise torque.

To go counter-clockwise, excite BC, then AB, then CA.



### Torque:

Only one pole is being pulled in; the other winding has either one rotor pole fully in, or one entering and one leaving that cancel. Many pole combinations are used (more poles, more torque).

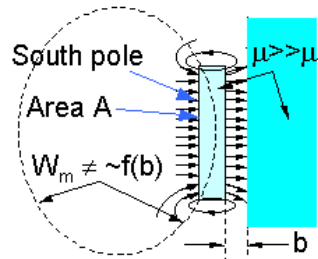
L22.6

## PERMANENT MAGNET SYSTEMS

### Refrigerator Magnets:

Force:  $f = -dw_m/db$   
 Variable energy:  $w_m \cong bA\mu_0 H_{gap}^2/2 [J]$   
 $= bAB_{gap}^2/2\mu_0$

Force density:  $f/A = B_{gap}^2/2\mu_0 [Nm^{-2}]$



Example: Let  $B = 1$  Tesla (10,000 gauss),  $A = 10 \text{ cm}^2$   
 Then  $f = 0.001 \times 1^2/2 \times 4\pi \times 10^{-7} \cong 400 \text{ N} \cong 100\text{-lb force}$

### Permanent Magnet Properties:

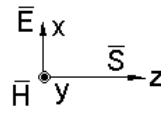
Strength: Typical strong magnets  $\sim 0.2\text{T}$ ; can  $\rightarrow 1\text{Tesla}$   
 Temperature: Above  $\sim 200\text{C}$  they fail; some fail at low temperatures

L22.6

## FORCES FROM ELECTROMAGNETIC WAVES

### Waves Impacting Conductors:

$$\begin{aligned} \bar{E}_x(z=0) = 0 &= [\bar{E}_+ \cos(\omega t - kz) + \bar{E}_- \cos(\omega t + kz)] \\ H(z=0) = \hat{y}(2E_+/\eta_0) \cos \omega t &\Rightarrow \bar{J}_s = \hat{x}(2E_+/\eta_0) \cos \omega t \end{aligned}$$



### Forces on Conductor:

$$\begin{aligned} \bar{f} = q(\bar{E} + \bar{v} \times \mu_0 \bar{H}) &\Rightarrow \text{quasistatic pressure } P [\text{Nm}^{-2}]; \\ F [\text{Nm}^{-3}] = nqv\mu_0 H &= J\mu_0 H \text{ where } n = \#/\text{m}^3 \text{ charge carriers} \\ \bar{P} = \int_0^\infty \bar{J}(z) \times \mu_0 \bar{H}(z) dz &\text{ where } \bar{J}(z) = \nabla \times \bar{H}(z) \text{ for } \sigma \rightarrow \infty \end{aligned}$$



$$\bar{J}(z) \equiv \nabla \times \bar{H} = \det \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \partial/\partial x & \partial/\partial y & \partial/\partial z \\ H_{x0} & H_{y0} & H_{z0} \end{vmatrix} = -\hat{x} \partial H_y / \partial z$$

$$\bar{P}(t) = -\hat{z} \mu_0 \int_0^\infty (\partial H_y / \partial z) H_y dz = -\hat{z} \mu_0 \int_{H_y(z=0)=H_{y0}}^{H_y=0} H_y dH_y = \hat{z} \mu_0 H_{y0}^2(t) / 2$$

[same as L22-6]

$\langle \bar{P}(t) \rangle = \hat{z} \mu_0 \langle H_{y0}^2(t) \rangle / 4 = 2 \langle \bar{S}(t) \rangle / c$

where  $H_{y0} = 2H_+$  and

$$\langle S(t) \rangle = \eta_0 H_+^2 / 2 = \mu_0 c H_+^2 / 2$$

L22-7

## PHOTON PRESSURE

**Photon Energy:**  $hf$  [J] = "m"  $c^2$

$h$  = Planck's constant =  $6.625 \times 10^{-34}$  [Js],  $f$  = frequency [Hz]

**Photon Momentum:** "m"  $c$  =  $hf/c$  [Nms<sup>-1</sup>]

Transferred to mirror upon reflection:  $\Delta$  momentum =  $2hf/c$

### Photon Pressure P [Nm<sup>-2</sup>]:

Pressure  $P$  is change of momentum  $s^{-1}m^{-2}$  [Mechanics:  $f = d(mv)/dt$ ]

$\langle P \rangle = n2hf/c = 2 \langle S(t) \rangle / c$  [Nm<sup>-2</sup>]

where  $n$  = # photons reflected  $s^{-1}m^{-2}$

If a photon is absorbed, then  $\Delta$  momentum =  $hf/c$ , and  $P = \langle S(t) \rangle / c$   
 In general, if the incident and reflected fluxes are  $S_1$  and  $S_2$  [Wm<sup>-2</sup>],

$\langle P \rangle = \langle S_1 - S_2 \rangle / c$  [Nm<sup>-2</sup>]

### Solar Sailing Across Solar System:

Say 1 km<sup>2</sup> at 1.4 kW/m<sup>2</sup>  $\Rightarrow A \langle P \rangle = A2 \langle S \rangle / c = 10^6 \times 2800 / 3 \times 10^8 = 9N$   
 (say  $10^{-6}$  thick,  $\rho = 1g/cm^3$ )

$v = at = (f/m)t \cong (9/1000)3 \times 10^7 \cong 3 \times 10^5 \text{ ms}^{-1}$  in 1 year =  $10^{-3}c$

L22-8