MASSACHUSETTS INSTITUTE OF TECHNOLOGY Department of Electrical Engineering and Computer Science

6.014 Electrodynamics

Problem Set 7 Solutions

Available in Tutorials:

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Problem 7.1

a)

$$w_{m} = \int_{v}^{1} \frac{1}{2} \mathbf{m} |\overline{H}|^{2} dv$$

$$= \frac{1}{2} \mathbf{m} |\overline{H}|^{2} (2\mathbf{p}RA)$$

$$= \mathbf{p}RA\mathbf{m} |\overline{H}|^{2}$$

$$\oint_{c} \overline{H} \cdot d \overline{l} = N_{1}i_{1} - N_{2}i_{2}$$

$$|\overline{H}| 2\mathbf{p}R = N_{1}i_{1} - N_{2}i_{2}$$

$$|\overline{H}| = \frac{N_{1}i_{1} - N_{2}i_{2}}{2\mathbf{p}R}$$

$$\therefore w_{m} = \mathbf{p}RA\mathbf{m} \left(\frac{N_{1}i_{1} - N_{2}i_{2}}{2\mathbf{p}R}\right)^{2} = \frac{A\mathbf{m}(N_{1}i_{1} - N_{2}i_{2})^{2}}{4\mathbf{p}R}$$
Therefore, $w_{m} \to \infty$ as $\mathbf{m} \to \infty$.

b)
$$V_{1} = N_{1} \frac{d\Phi}{dt} \text{ and } V_{2} = N_{2} \frac{d\Phi}{dt}$$

$$\oint_{c} \overline{E} \cdot d\overline{l} = -\int_{s} \frac{d\overline{B}}{dt} \cdot d\overline{s} = N_{2} \mathbf{m} A \frac{d |\overline{H}|}{dt}$$

$$\therefore \frac{d\Phi}{dt} = \mathbf{m} A \frac{d |\overline{H}|}{dt}$$

$$|\overline{H}| = \frac{N_{1}i_{1} - N_{2}i_{2}}{2\mathbf{p}R}$$

$$\therefore \frac{d\Phi}{dt} = \frac{\mathbf{m} A}{2\mathbf{p}R} \frac{d(N_{1}i_{1} - N_{2}i_{2})}{dt}$$

$$V_{1} = \frac{N_{1}\mathbf{m} A}{2\mathbf{p}R} \frac{d(N_{1}i_{1} - N_{2}i_{2})}{dt}$$

$$V_{2} = \frac{N_{2}\mathbf{m} A}{2\mathbf{p}R} \frac{d(N_{1}i_{1} - N_{2}i_{2})}{dt}$$
If V_{2} is positive when $i_{2} = 0$, then $\frac{di_{1}}{dt} > 0$.



Problem 7.2

In all what follows: the subscript d correspond to the dielectric slab; the subscript w correspond to the conductor wire.

a) The magnitude of the E-field for the parallel plate transmission line is:

$$E = \frac{V}{d_d} \Rightarrow V_{max} = (\frac{1 \times 10^6}{1 \times 10^{-2}})(0.1 \times 10^{-6}) = 10V$$

b) The dielectric is not lossy, hence $\eta = \sqrt{\frac{\mu}{\epsilon}}$ is real. We know that $Z_0 = \frac{\eta d_d}{W}$ where in this problem we have that $\mu = \mu_0$ and $\epsilon = 4\epsilon_0$. Substituting this into the above relationships we find that $Z_0 = \frac{(377)(0.1 \times 10^{-6})}{2(0.4 \times 10^{-6})} = 47.125\Omega$

- c) The resistance of the wire strip is $R = \frac{\ell}{\sigma A}$. The resistance of the ground path of the circuit is taken to be zero; the reason being that when $A_{ground} \rightarrow \infty \Rightarrow R_{ground} = 0$. We can calculate the length from setting $|R| = |Z_0| \Rightarrow \ell = |Z_0| \sigma d_w W = 75.4 \mu m$
- d) For f = 10GHz the wavelength of the EM wave is $\lambda = \frac{c}{f} = \frac{1}{\sqrt{\mu \epsilon f}} = 1.5 \times 10^{-2} \text{ m}$. Thus a quarter wavelength is $\lambda/4 = 3.75 \text{ mm}$.

e)
$$L = \frac{\mathbf{m}_0 d}{W} = 0.31416 \mathbf{m} H$$

- f) Answers that might concern me ...
 - We ignored fringing effects. The latter might decrease V_{max} . It is conceivable that we can have circuits operating near $\pm 10V$ (for instance the RS232 12V serial comminucation bus in a computer). We surely don't want dielectric breakdown of the material.
 - The length of the wire for which its resistance becomes comparable to the characteristic impedance of the line is short. It is not hard to imagine that printed circuit board will have wires in excess of this length. When that is the case the I²R losses might be significant.
 - The calculated quarter wavelength is comparable to the physical dimension of a printed circuit board. Thus it is not unreasonable to doubt the validity of lumped parameter approximation of circuit parameters.

Problem 7.3









 $V(t) \rightarrow 5$ Vas $t \rightarrow \infty$. Therefore, the flip flop never switches.

d)
$$V_L(t \to \infty) = \frac{Z_L}{Z_L + Z_s} V_s = 5V$$

e) If the TEM line impedance $Z_0 = Z_L$ then $\Gamma_L = 0$ (no reflections). Since $Z_s = Z_L$, $V_+ = 5V$. Therefore, with $Z_0 = Z_L$ we have a forward traveling wave of magnitude 5V. Therefore, the flip flop switches when this wave reaches z = 5cm at $t = 3.33 \times 10^{-10} s$.