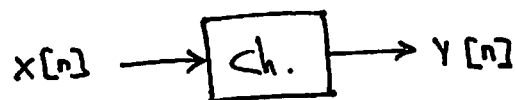


FREQUENCY RESPONSE

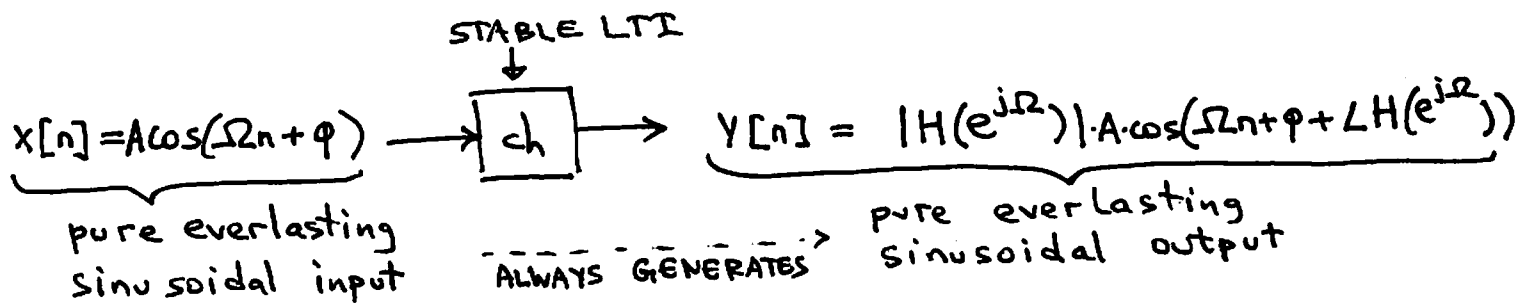
6.02/Oct. 21, 2010

①



↑
LTI

ALSO NOT COMPLETELY *STABLE (unit sample response
NECESSARY SOMETIMES DIMINISHES: $h[n] \rightarrow 0$ as $n \rightarrow \pm\infty$)
BUT THAT'S A TRICKY BUSINESS *NOT NECESSARILY CAUSAL



where $H(e^{j\Omega}) = \sum h[n] e^{-j\Omega n}$
 $H(z) = \sum_n h[n] z^{-n}$ FOR $z = e^{j\Omega}$

EQUIVALENT "COMPLEX EXPONENTIAL" FORMULA:

$$x_c[n] = X e^{j\Omega n} \rightarrow [ch] \rightarrow y_c[n] = H(e^{j\Omega}) X e^{j\Omega n}$$

CONNECTION: $A \cos(\Omega n + \phi) = \text{Re}[X e^{j\Omega n}]$
where $X = A e^{j\phi}$

$$x[n] = \text{Re}(X e^{j\Omega n}) \rightarrow [ch] \rightarrow y[n] = \text{Re}(H(e^{j\Omega}) X e^{j\Omega n})$$

WHY IS THIS USEFUL FOR OTHER INPUTS?

— BECAUSE "EVERY" [REASONABLE] INPUT
CAN BE APPROXIMATED BY A SUM OF SINUSOIDS !

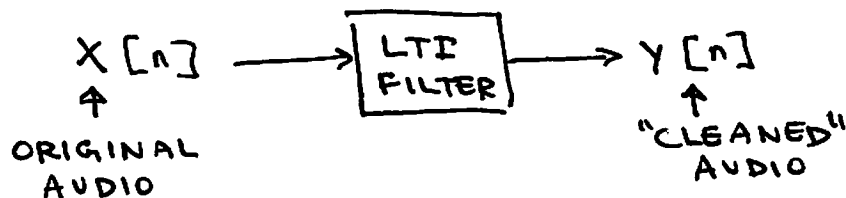
// IF THE SINUSOIDS HAVE A "START" TIME,
THE RESPONSE WILL APPROACH THE PRESCRIBED SINUSOID

Ex. 1

AUDIO RECODING, WHICH SAMPLES
SOUND AT 40 KHz, IS CORRUPTED BY
60 Hz SINUSOIDAL NOISE
DESIGN A FILTER

$$Y[n] = X[n] + a(X[n-1] + X[n+1]) \quad (a=?)$$

TO COMPLETELY ELIMINATE THE NOISE

STEP 1

LTI + SINUSOIDS $\rightarrow$ THINK FREQUENCY RESPONSE

$$h[n] = \delta[n] + a(\delta[n-1] + \delta[n+1])$$



$$H(e^{j\Omega}) = 1 + a(e^{-j\Omega} + e^{j\Omega})$$

$$= 1 + 2a \cos(\Omega) \quad \leftarrow \text{SANITY CHECK: MUST BE } 2\pi\text{-PERIODIC}$$

$$H(z) = 1 + \frac{a}{z} + az = \frac{a + z + az^2}{z} = \frac{1 + z/a + z^2}{z/a}$$

STEP 2

WHAT KIND OF DT FREQUENCY IS 60 Hz
WHEN SAMPLED AT 40 KHz?

$$\text{CT SINUSOID AT 60 Hz: } w(t) = A \cos(2\pi \cdot 60 \cdot t + \phi)$$

$$40 \text{ KHz SAMPLING} = 4 \cdot 10^4 \text{ SAMPLES/SEC}$$

$$= 1 \text{ SAMPLE IN } T = 0.25 \cdot 10^{-4} \text{ SEC}$$

SAMPLED SINUSOID:

$$v[n] = w(nT) = A \cos(\underbrace{2\pi \cdot 60 \cdot \frac{1}{4} \cdot 10^{-4}}_{\Omega_0} n + \phi)$$

$$\Omega_0 = 3\pi \cdot 10^{-3}$$

6.02/Oct. 21, 2010

STEP 3 TO CANCEL THE SINUSOIDS AT FREQUENCY Ω_0

THE
MOST
IMPORTANT
PART!

$$\text{NEED } H(e^{j\Omega_0}) = 0$$

STEP 4 ALGEBRA: FIND a SUCH THAT $H(e^{j\Omega_0}) = 0$

i.e. $1 + \frac{z}{a} + z^2$ HAS ROOT $z = e^{j\Omega_0}$

THEN $z = e^{-j\Omega_0}$ IS THE OTHER ROOT

$$\text{HENCE } 1 + \frac{z}{a} + z^2 = \underbrace{(e^{j\Omega_0} e^{-j\Omega_0})}_1 + \underbrace{(-e^{j\Omega_0} e^{-j\Omega_0})}_{-2\cos\Omega_0} z + z^2$$

$$\frac{1}{a} = -2\cos\Omega_0$$

$$a = -\frac{1}{2\cos(3\pi 10^{-3})}$$

DISCUSSION: WHILE ELIMINATING THE NOISE,
BOTH PHASE AND AMPLITUDE OF
"OTHER SINUSOIDS" WILL BE MODIFIED
IS THIS BAD?

CHANGE IN AMPLITUDE: HOW LOUD A TONE IS...
HUMAN EAR SENSITIVITY IS
"LOGARITHMIC", I THINK

~~$1 + \frac{z}{a} + z^2$~~ $|1 + 2a\cos\Omega|$ does not
change dramatically,
EXCEPT AT $\Omega \approx 0$

CHANGE IN PHASE: (THE RELATIVE PHASE
IS WHAT'S IMPORTANT)

HUMAN EAR APPEARS TO BE
QUITE INSENSITIVE TO
PHASE ERRORS

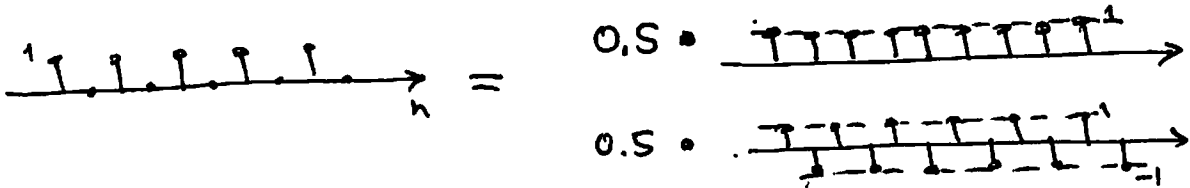
PERHAPS
BECAUSE THE
SENSING IS
BASED ON
EXCITING
RESONATORS

Ex. 2



WHAT DOES THIS TELL ABOUT THE FREQUENCY RESPONSE?

STEP 1 INPUT AS A SUM OF SINUSOIDS?



$$x[n] = 0.5 \cos(0 \cdot n + \cancel{\pi/4}) + 0.5 \cos(\pi n)$$

$$y[n] = 3 \cdot \cos(0.1n)$$

STEP 2 IN TERMS OF THE (UNKNOWN) FREQUENCY RESPONSE :

$$Y[n] = |H(e^{j0})| \cdot 0.5 \cdot \cos(0 \cdot n + \angle H(e^{j0})) \\ + |H(e^{j\pi})| \cdot 0.5 \cdot \cos(\pi n + \angle H(e^{j\pi}))$$

Hence $H(e^{j \cdot 0}) = 6$

$$H(e^{j\pi}) = 0$$

Ex. 3 WHICH VALUES OF a, b ~~MAKES~~ IN $h[n] = a\delta[n] + b\delta[n-1]$

Wanted MATCH THE FREQUENCY RESPONSE PLOT?

$$Y(z) = a + b/z$$

$$2 \quad H(z) = a + b/z$$

$$\{ H(e^{+j\omega}) = 0 \Rightarrow b = -a$$

$$\{ H(e^{j\pi}) = 1 \Rightarrow a = b = 1$$

$$\begin{cases} a = 0.5, & b = -0.5 \end{cases}$$

