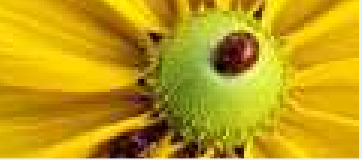

16.61 Spring 2006
Lecture Presentation Thu 23-Mar-06 ver 2.0

Charles P. Coleman

March 23, 2006



TODAY

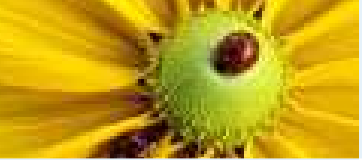
TODAY

SLM

Block

Atwood

- Single Link Robotic Manipulator
- Block Sliding on a Wedge
- Atwood's machine



Single-Link Manipulator

TODAY

SLM

Block

Atwood

Single-Link Manipulator with Friction

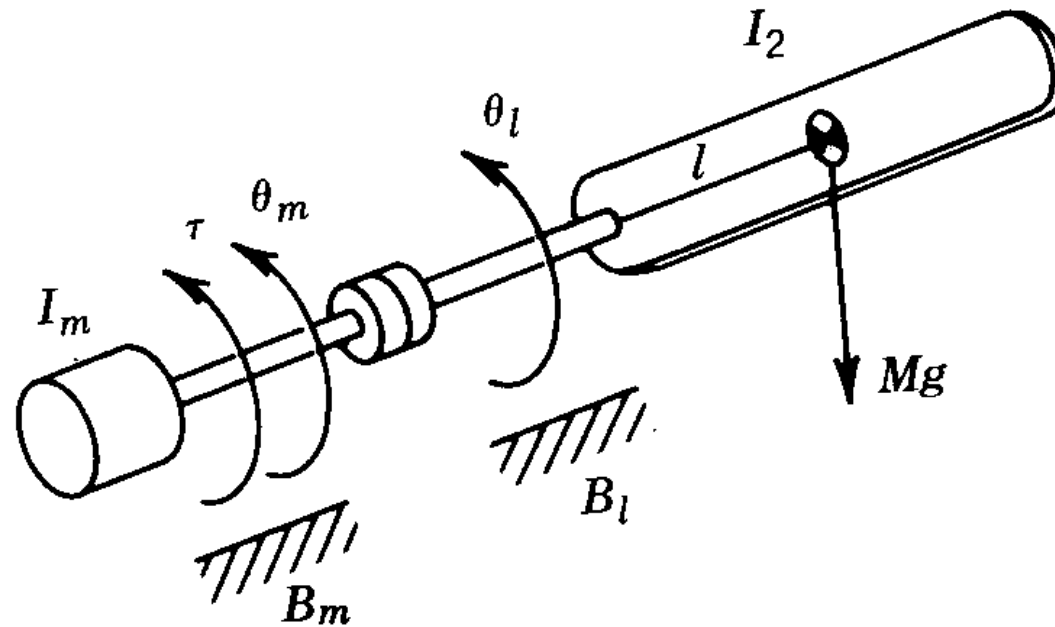


Figure 1: Single-Link Manipulator

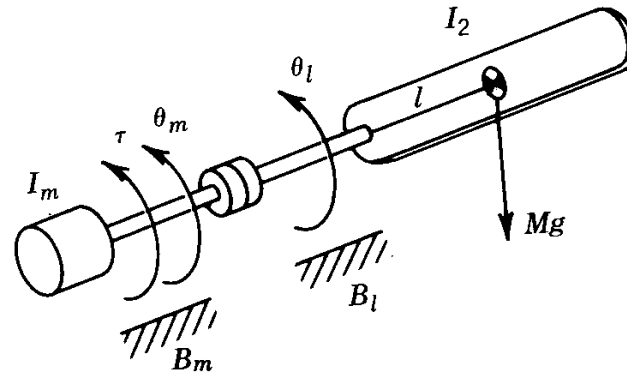
Single-Link Manipulator

TODAY

SLM

Block

Atwood



θ_l : angle of link

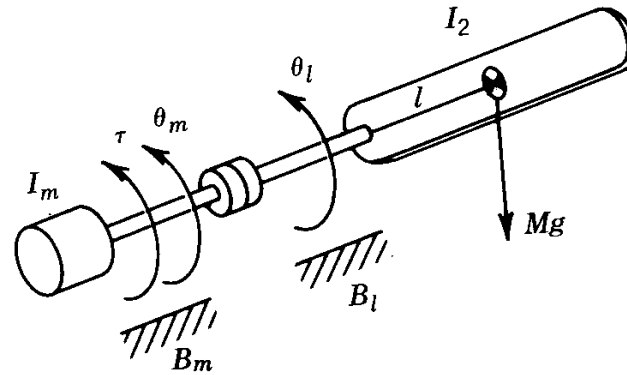
Single-Link Manipulator

TODAY

SLM

Block

Atwood



θ_l : angle of link

θ_m : angle of motor shaft

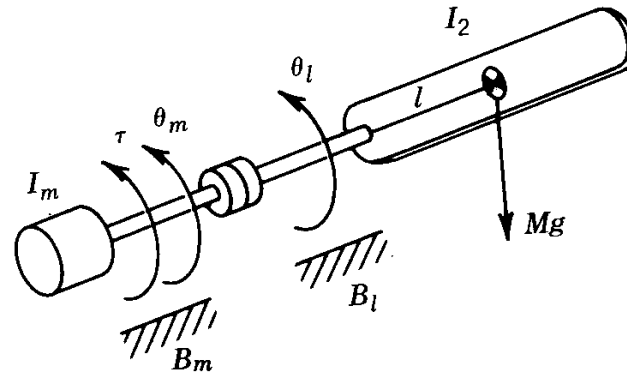
Single-Link Manipulator

TODAY

SLM

Block

Atwood



θ_l : angle of link

θ_m : angle of motor shaft

$n : 1$: gear ratio

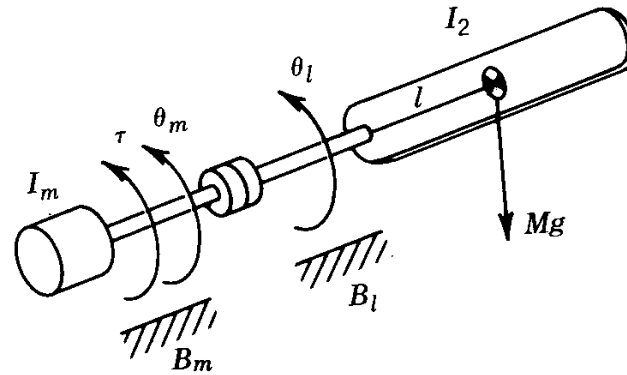
Single-Link Manipulator

TODAY

SLM

Block

Atwood



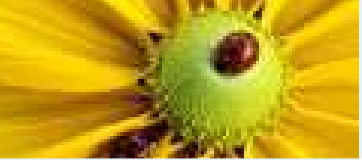
θ_l : angle of link

θ_m : angle of motor shaft

$n : 1$: gear ratio

$$\theta_l = 1/n \theta_m$$

Single-Link Manipulator

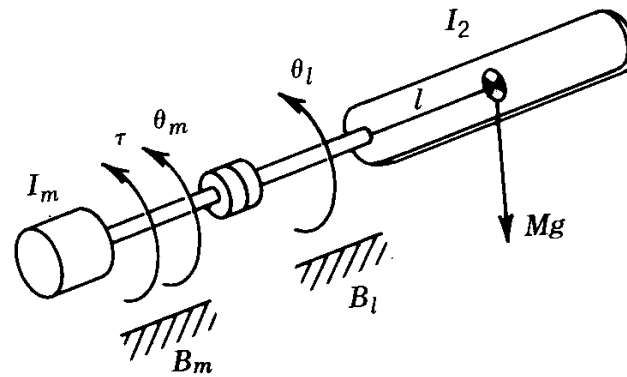


TODAY

SLM

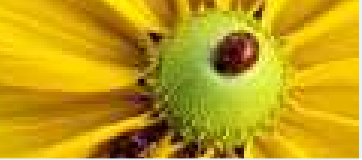
Block

Atwood



I_m and I_2 are the rotational inertias of the motor and link.

Single-Link Manipulator

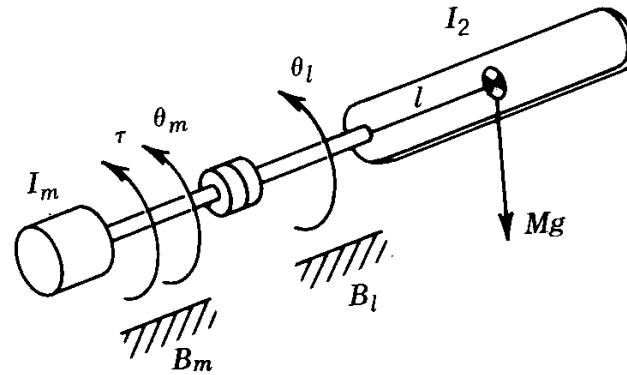


TODAY

SLM

Block

Atwood



I_m and I_2 are the rotational inertias of the motor and link.

Kinetic Energy

Single-Link Manipulator

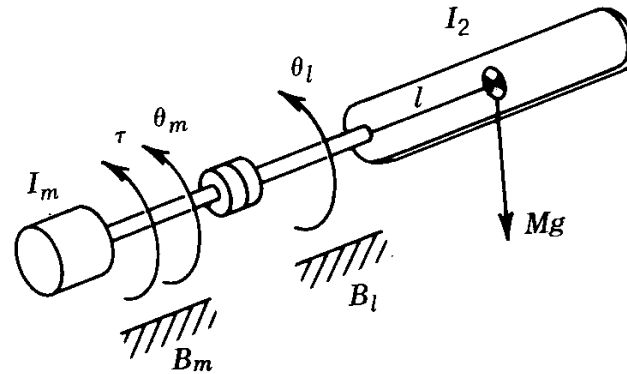


TODAY

SLM

Block

Atwood

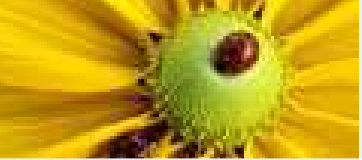


I_m and I_2 are the rotational inertias of the motor and link.

Kinetic Energy

$$\begin{aligned} T &= 1/2 I_m \dot{\theta}_m^2 + 1/2 I_2 \dot{\theta}_l^2 \\ &= 1/2 (I_m + I_2/n^2) \dot{\theta}_m^2 \end{aligned}$$

Single-Link Manipulator

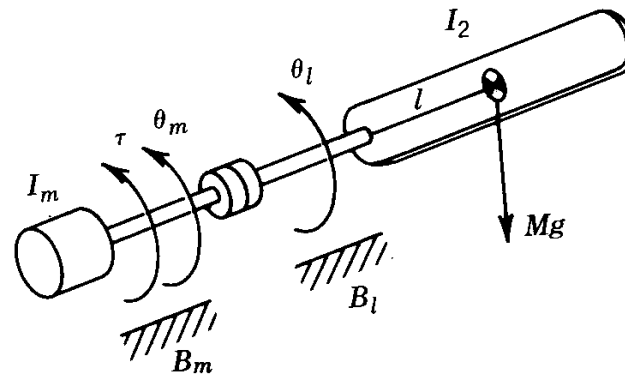


TODAY

SLM

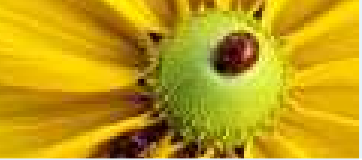
Block

Atwood



M is the total mass of the link and l is the distance from the joint axis to the link center of mass.

Single-Link Manipulator

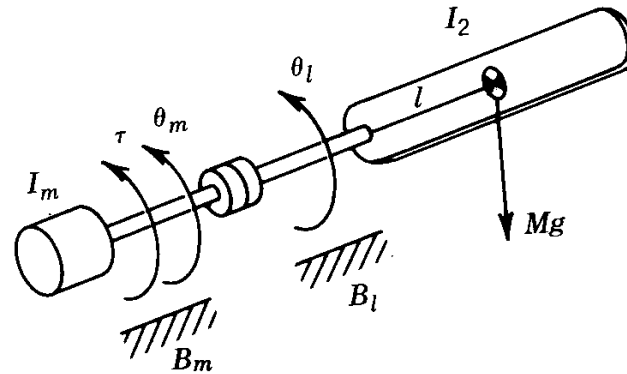


TODAY

SLM

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Atwood



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Potential Energy

Single-Link Manipulator

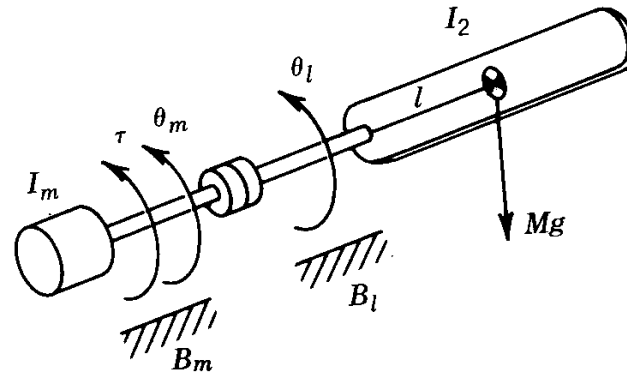


TODAY

SLM

Block

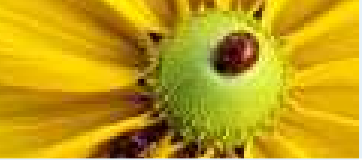
Atwood



M is the total mass of the link and l is the distance from the joint axis to the link center of mass.

Potential Energy

$$\begin{aligned} V &= Mgl(1 - \cos \theta_l) \\ &= Mgl(1 - \cos \theta_m/n) \end{aligned}$$



Single-Link Manipulator

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The Lagrangian is then

$$\begin{aligned} L &= T - V \\ &= \frac{1}{2}(I_m + I_2/n^2)\dot{\theta}_m^2 - Mgl(1 - \cos \theta_m/n) \end{aligned}$$



Single-Link Manipulator

TODAY

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The Lagrangian is then

$$\begin{aligned} L &= T - V \\ &= 1/2(I_m + I_2/n^2)\dot{\theta}_m^2 - Mgl(1 - \cos \theta_m/n) \end{aligned}$$

Lagrange's Equation is

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}_j} \right) - \frac{\partial L}{\partial q_j} = \tau_j$$

Single-Link Manipulator



TODAY

SLM

Block

Atwood

The Lagrangian is then

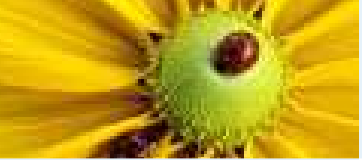
$$\begin{aligned} L &= T - V \\ &= 1/2(I_m + I_2/n^2)\dot{\theta}_m^2 - Mgl(1 - \cos \theta_m/n) \end{aligned}$$

Lagrange's Equation is

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}_j} \right) - \frac{\partial L}{\partial q_j} = \tau_j$$

Which leads to

$$(I_m + I_2/n^2)\ddot{\theta}_m + \frac{Mgl}{n} \sin \theta_m/n = \tau_j$$



Single-Link Manipulator

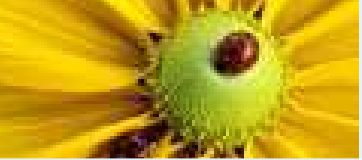
TODAY

SLM

Block

Atwood

Generalized Forces:



Single-Link Manipulator

TODAY

SLM

Block

Atwood

Generalized Forces:

The generalized force τ consists of the motor torque u , and the (nonconservative) link-motor shaft damping torques: $B_m \dot{\theta}_m$ and $B_l \dot{\theta}_l$.



Single-Link Manipulator

TODAY

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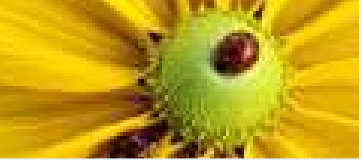
Block

Atwood

Generalized Forces:

The generalized force τ consists of the motor torque u , and the (nonconservative) link-motor shaft damping torques: $B_m\dot{\theta}_m$ and $B_l\dot{\theta}_l$.

$$\tau = u - (B_m + B_l/n)\dot{\theta}_m$$



Single-Link Manipulator

TODAY

SLM

Block

Atwood

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The generalized force τ consists of the motor torque u , and the (nonconservative) link-motor shaft damping torques: $B_m \dot{\theta}_m$ and $B_l \dot{\theta}_l$.

$$\tau = u - (B_m + B_l/n) \dot{\theta}_m$$

Complete Dynamics:

$$J \ddot{\theta}_m + B \dot{\theta}_m + C \sin \theta_m / n = u$$



Single-Link Manipulator

TODAY

SLM

Block

Atwood

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Complete Dynamics:

$$J\ddot{\theta}_m + B\dot{\theta}_m + C \sin \theta_m/n = u$$

where

$$J = I_m + I_2/n^2$$



Single-Link Manipulator

TODAY

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where

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$$B = B_m + B_l/n$$



Single-Link Manipulator

TODAY

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Block

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$$\tau = u - (B_m + B_l/n)\dot{\theta}_m$$

Complete Dynamics:

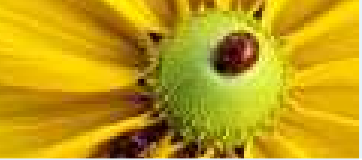
$$J\ddot{\theta}_m + B\dot{\theta}_m + C \sin \theta_m/n = u$$

where

$$J = I_m + I_2/n^2$$

$$B = B_m + B_l/n$$

$$C = Mgl/n$$



Single-Link Manipulator

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Complete Dynamics:

$$J\ddot{\theta}_m + B\dot{\theta}_m + C \sin \theta_m/n = u$$



Single-Link Manipulator

TODAY

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Complete Dynamics:

$$J\ddot{\theta}_m + B\dot{\theta}_m + C \sin \theta_m/n = u$$

- In general a system of second order nonlinear differential equations in the generalized coordinates will result.



Single-Link Manipulator

TODAY

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Complete Dynamics:

$$J\ddot{\theta}_m + B\dot{\theta}_m + C \sin \theta_m/n = u$$

- In general a system of second order nonlinear differential equations in the generalized coordinates will result.
- In robotics and multibody applications the resulting system of equations will have the following form:

$$D(q)\ddot{q} + C(q, \dot{q})\dot{q} + g(q) = \tau$$



Single-Link Manipulator

TODAY

SLM

Block

Atwood

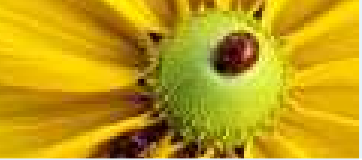
Complete Dynamics:

$$J\ddot{\theta}_m + B\dot{\theta}_m + C \sin \theta_m/n = u$$

- In general a system of second order nonlinear differential equations in the generalized coordinates will result.
- In robotics and multibody applications the resulting system of equations will have the following form:

$$D(q)\ddot{q} + C(q, \dot{q})\dot{q} + g(q) = \tau$$

D will be called the mass or inertial matrix, C will contain centrifugal and Coriolis terms, and the g terms arise from the conservative forces.



Sliding Block

TODAY
SLM
Block
Atwood

Block Sliding Down a Ramp

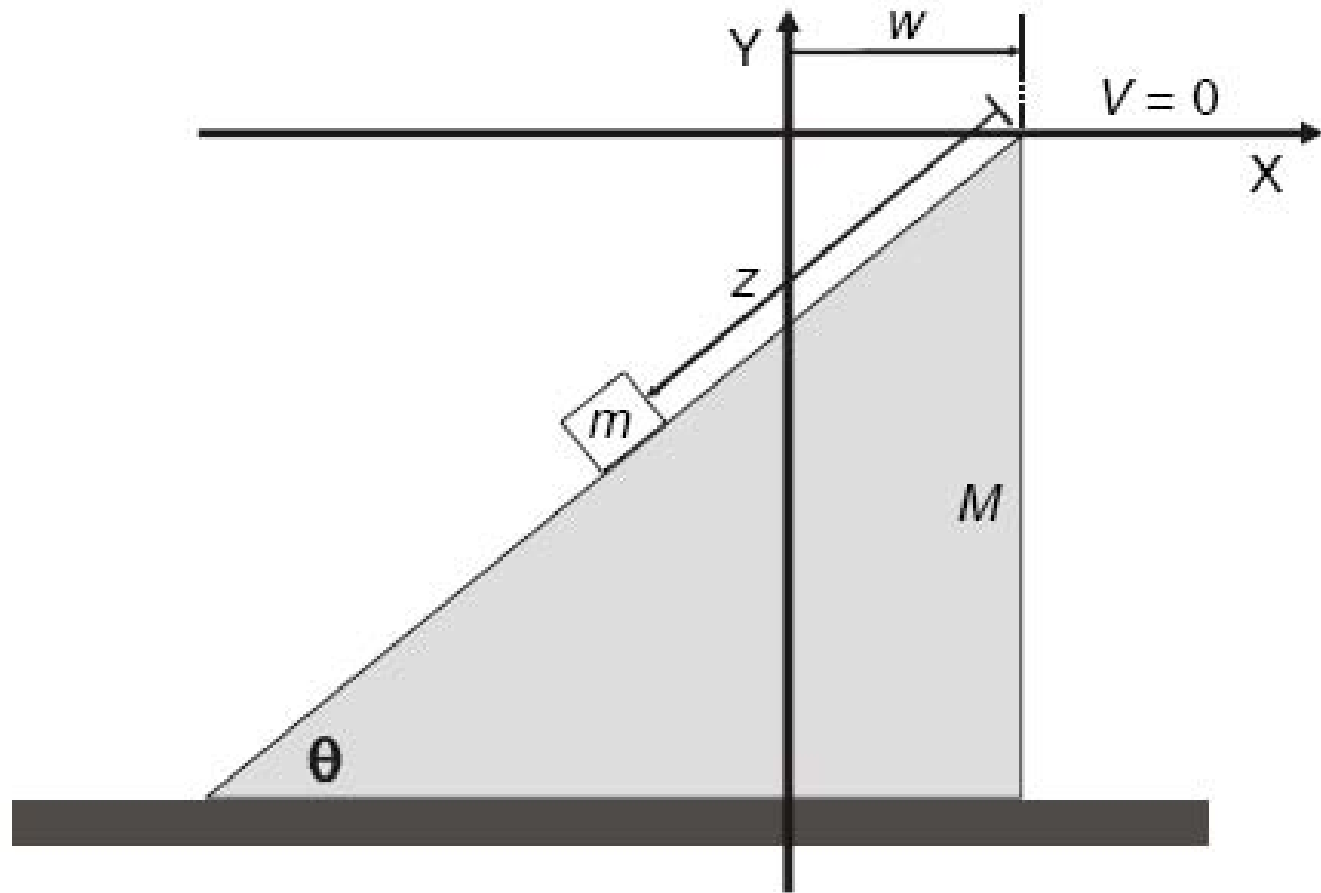
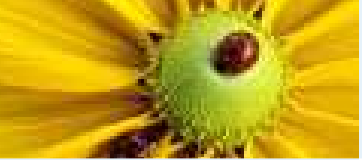


Figure 2: Sliding Block



Atwood's Machine

TODAY
SLM
Block
Atwood

Atwood's Machine

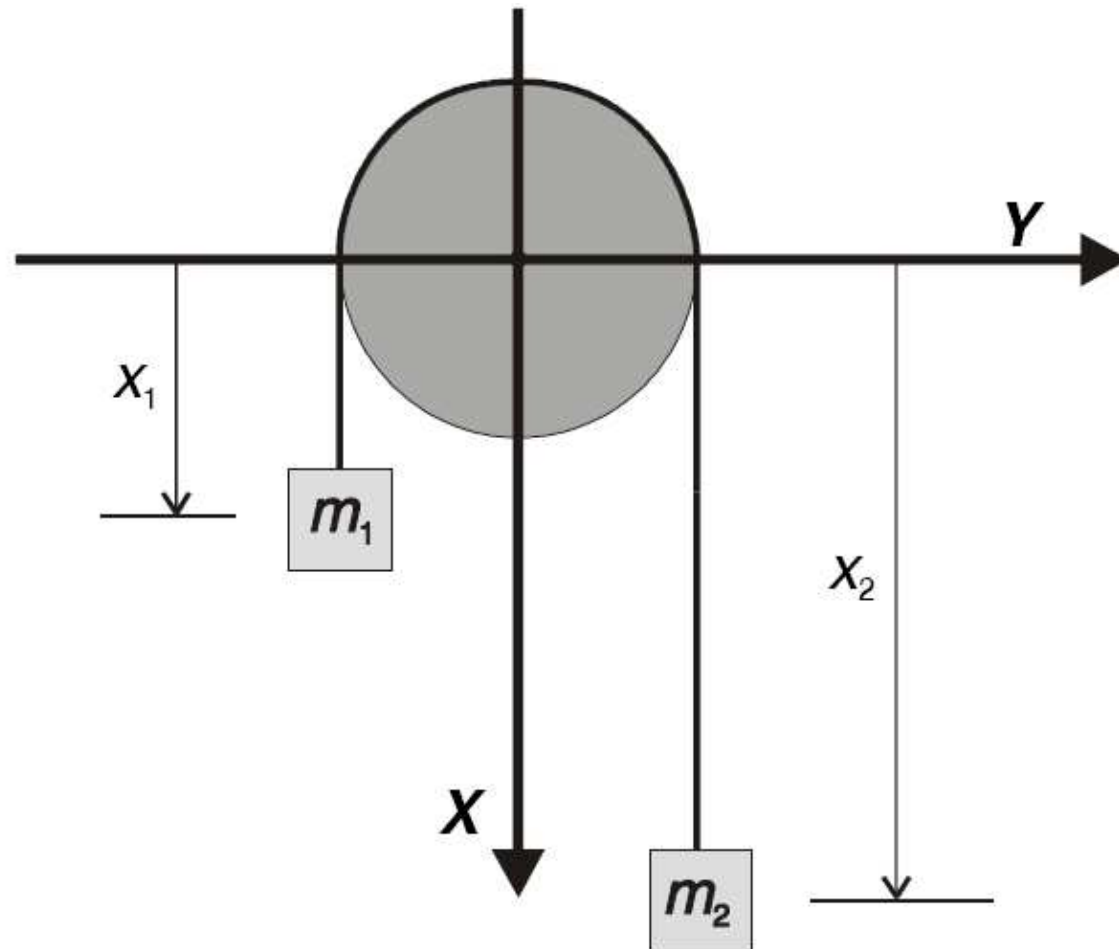


Figure 3: Atwood's Machine