

# Shape factors for heat conduction inside and outside two-dimensional bodies

John H. Lienhard V

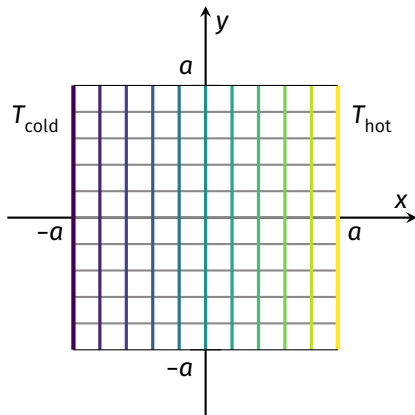
Rohsenow Kendall Heat Transfer Lab  
Massachusetts Institute of Technology  
Cambridge MA 02139-4307 USA

PRTEC 2019, Maui, 16 December 2019



# Shape factor inside a square of side length $2a$

One side hot, opposite side cold, other sides adiabatic



# Shape factor inside a square of side length $2a$

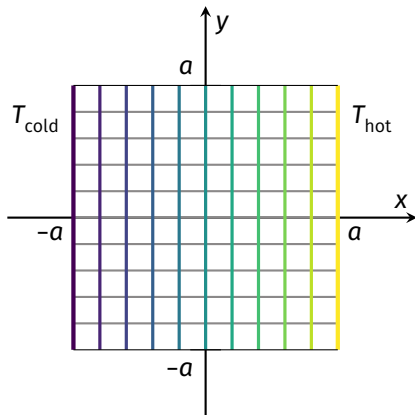
One side hot, opposite side cold, other sides adiabatic

Simple conduction

$$Q = k 2a (\Delta T / 2a)$$

$$Q \equiv k S \Delta T$$

$$\text{so } S = 1$$



# Shape factor inside a square of side length $2a$

One side hot, opposite side cold, other sides adiabatic

## Simple conduction

$$Q = k 2a (\Delta T / 2a)$$

$$Q \equiv k S \Delta T$$

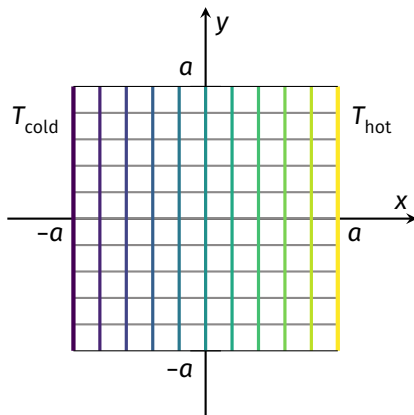
$$\text{so } S = 1$$

## As a flux plot

$n_a = 10$  adiabat increments

$n_i = 10$  isotherm increments

$$\text{so } S = n_a / n_i = 10 / 10 = 1$$



# Flux plot by Jakob and Dow (*Trans. ASME*, 1946)

Checking whether a convection test surface will be isothermal

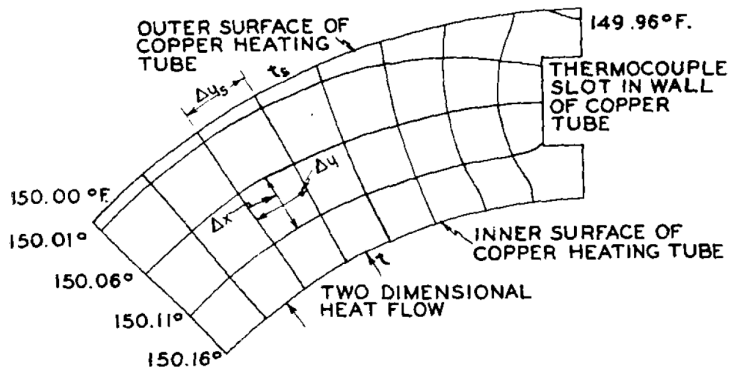
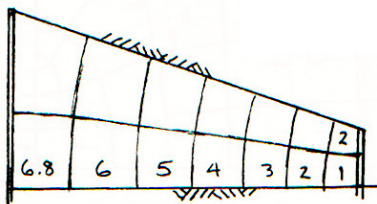


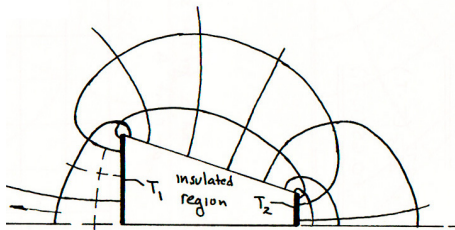
FIG. 8 TEMPERATURE FIELD IN COPPER TUBE WALL

## Shape factors for a wedge (AHTT Problem 5.22)

Graphical results are almost equal. **Why?!**



$$S = \frac{2}{6.8} = 0.29$$



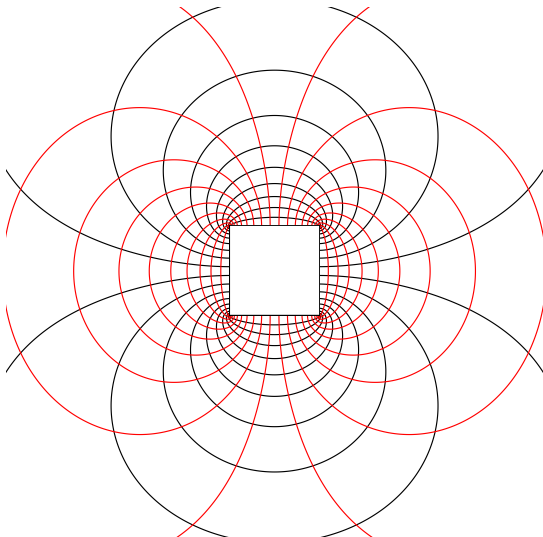
$$S = \frac{2.4}{8} = 0.30$$

# Shape factor *outside* a square of side $a$

One side hot, opposite side cold, other sides adiabatic

Not so easy!

FEM solution shown here



# Shape factor *outside* a square of side $a$

One side hot, opposite side cold, other sides adiabatic

Not so easy!

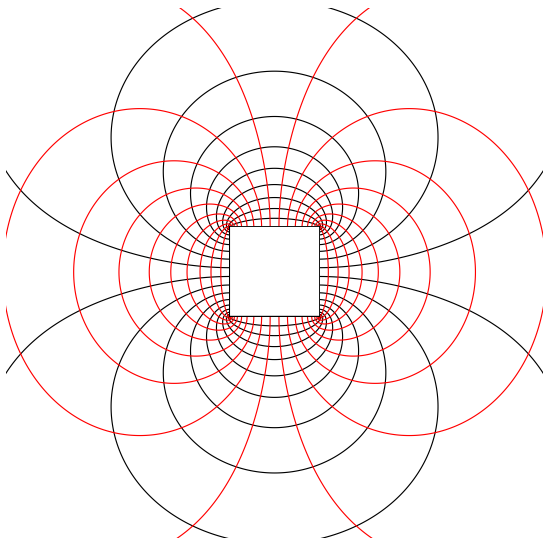
FEM solution shown here

Graphically

$n_a = 19$  adiab. increments

$n_i = 19$  isoth. increments

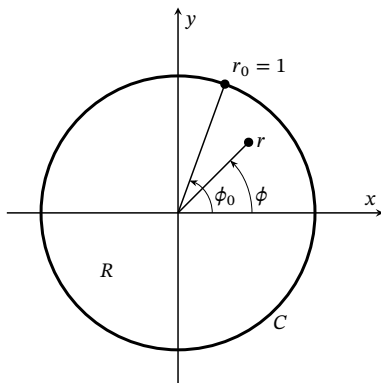
so  $S = n_a/n_i = 19/19 = 1$





# Solve conduction equation inside and outside a disk

Apply Poisson integral formula (from complex variables). Dimensionless temperature:  $0 \leq \theta \leq 1$



# Solve conduction equation inside and outside a disk

Apply Poisson integral formula (from complex variables). Dimensionless temperature:  $0 \leq \theta \leq 1$

## Interior

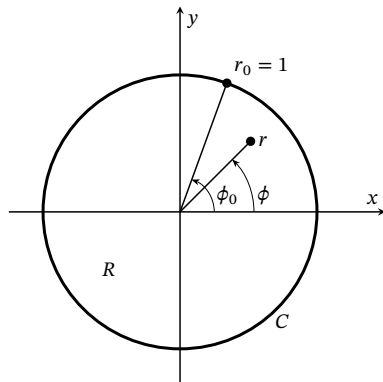
$$\nabla^2 \theta = 0 \quad \text{for } z \text{ in } R$$

$$\theta(1, \phi) = h(\phi) \quad \text{for } z = (r, \phi) \text{ on } C$$

$$\theta(r, \phi) = \int_{-\pi}^{\pi} P(r, \phi, \phi_0) h(\phi_0) d\phi_0$$

## Poisson kernel

$$P(r, \phi, \phi_0) = \frac{1}{2\pi} \frac{1 - r^2}{1 + r^2 - 2r \cos(\phi - \phi_0)}$$



# Solve conduction equation inside and outside a disk

Apply Poisson integral formula (from complex variables). Dimensionless temperature:  $0 \leq \theta \leq 1$

## Interior

$$\nabla^2 \theta = 0 \quad \text{for } z \text{ in } R$$

$$\theta(1, \phi) = h(\phi) \quad \text{for } z = (r, \phi) \text{ on } C$$

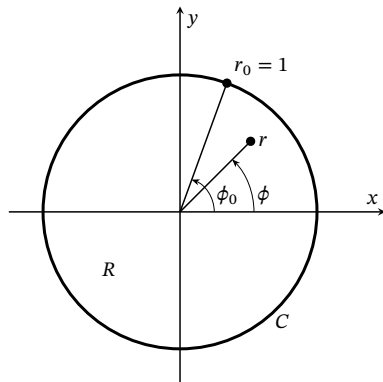
$$\theta(r, \phi) = \int_{-\pi}^{\pi} P(r, \phi, \phi_0) h(\phi_0) d\phi_0$$

## Poisson kernel

$$P(r, \phi, \phi_0) = \frac{1}{2\pi} \frac{1 - r^2}{1 + r^2 - 2r \cos(\phi - \phi_0)}$$

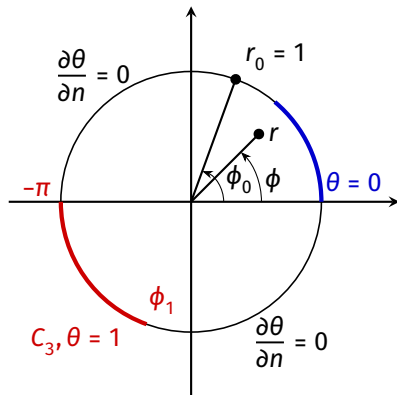
## Exterior

$$\theta^e(r, \phi) = - \int_{-\pi}^{\pi} P(r, \phi, \phi_0) h(\phi_0) d\phi_0$$



# Shape factor for a disk

Integrate heat flux along one isothermal boundary,  $C_3$

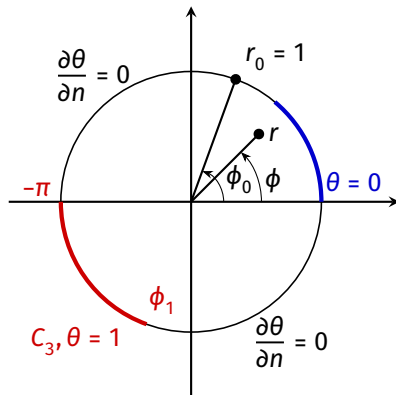


# Shape factor for a disk

Integrate heat flux along one isothermal boundary,  $C_3$

## Interior

$$\begin{aligned}\frac{\dot{Q}^i}{k^i(T_3 - T_1)} &= S^i = \int_{C_3} \frac{\partial \theta}{\partial n} dl = \int_{-\pi}^{\phi_1} \frac{\partial \theta}{\partial r} \bigg|_{r=1} d\phi \\ &= \int_{-\pi}^{\phi_1} \frac{\partial}{\partial r} \int_{-\pi}^{\pi} P(r, \phi, \phi_0) h(\phi_0) d\phi_0 \bigg|_{r=1} d\phi\end{aligned}$$



# Shape factor for a disk

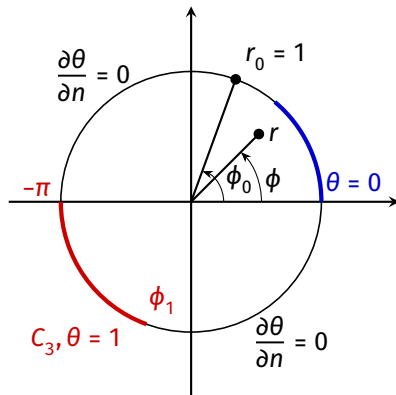
Integrate heat flux along one isothermal boundary,  $C_3$

## Interior

$$\begin{aligned}\frac{\dot{Q}^i}{k^i(T_3 - T_1)} &= S^i = \int_{C_3} \frac{\partial \theta}{\partial n} dl = \int_{-\pi}^{\phi_1} \frac{\partial \theta}{\partial r} \bigg|_{r=1} d\phi \\ &= \int_{-\pi}^{\phi_1} \frac{\partial}{\partial r} \int_{-\pi}^{\pi} P(r, \phi, \phi_0) h(\phi_0) d\phi_0 \bigg|_{r=1} d\phi\end{aligned}$$

## Exterior ( $k^e \neq k^i$ )

$$\begin{aligned}\frac{\dot{Q}^e}{k^e(T_3 - T_1)} &= S^e = \int_{C_3} \frac{\partial \theta^e}{\partial n^e} dl = - \int_{-\pi}^{\phi_1} \frac{\partial \theta^e}{\partial r} \bigg|_{r=1} d\phi \\ &= \int_{-\pi}^{\phi_1} \frac{\partial}{\partial r} \int_{-\pi}^{\pi} P(r, \phi, \phi_0) h(\phi_0) d\phi_0 \bigg|_{r=1} d\phi\end{aligned}$$



# Shape factor for a disk

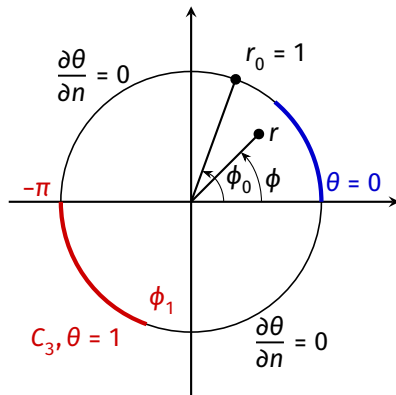
Integrate heat flux along one isothermal boundary,  $C_3$

## Interior

$$\begin{aligned}\frac{\dot{Q}^i}{k^i(T_3 - T_1)} &= S^i = \int_{C_3} \frac{\partial \theta}{\partial n} dl = \int_{-\pi}^{\phi_1} \frac{\partial \theta}{\partial r} \bigg|_{r=1} d\phi \\ &= \int_{-\pi}^{\phi_1} \frac{\partial}{\partial r} \int_{-\pi}^{\pi} P(r, \phi, \phi_0) h(\phi_0) d\phi_0 \bigg|_{r=1} d\phi\end{aligned}$$

## Exterior ( $k^e \neq k^i$ )

$$\begin{aligned}\frac{\dot{Q}^e}{k^e(T_3 - T_1)} &= S^e = \int_{C_3} \frac{\partial \theta^e}{\partial n^e} dl = - \int_{-\pi}^{\phi_1} \frac{\partial \theta^e}{\partial r} \bigg|_{r=1} d\phi \\ &= \int_{-\pi}^{\phi_1} \frac{\partial}{\partial r} \int_{-\pi}^{\pi} P(r, \phi, \phi_0) h(\phi_0) d\phi_0 \bigg|_{r=1} d\phi\end{aligned}$$



**$S^i = S^e$ : The interior and exterior shape factors of the disk are always equal!**

## Boundary condition for $|z| \rightarrow \infty$

Note that  $\theta^e$  has a specific and finite limit:

$$\theta_{\infty}^e \equiv \lim_{r \rightarrow \infty} \theta^e(r) = \frac{1}{2\pi} \int_{-\pi}^{\pi} h(\phi_0) d\phi_0$$

Temperature at infinity is average temperature around disk's perimeter.



## Boundary condition for $|z| \rightarrow \infty$

Note that  $\theta^e$  has a specific and finite limit:

$$\theta_{\infty}^e \equiv \lim_{r \rightarrow \infty} \theta^e(r) = \frac{1}{2\pi} \int_{-\pi}^{\pi} h(\phi_0) d\phi_0$$

Temperature at infinity is average temperature around disk's perimeter.

Further:

$$\theta^e(z) \sim \theta_{\infty}^e + a_1/z + a_2/z^2 + \dots \quad \text{as } r = |z| \rightarrow \infty$$

Heat flux  $q \sim 1/r^2$  and heat flow  $\dot{Q} \sim 2\pi r/r^2 = 2\pi/r$ : **no heat transfer to infinity.**

# Conformal maps

Analytic functions that map solutions of Laplace's equation from one shape to another in the complex plane

**Riemann mapping theorem:** Any simply-connected region  $R$  in  $z$ -plane can be conformally mapped, one-to-one, onto the unit disk in the  $w$ -plane.

# Conformal maps

Analytic functions that map solutions of Laplace's equation from one shape to another in the complex plane

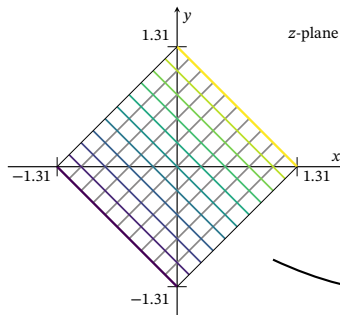
**Riemann mapping theorem:** Any simply-connected region  $R$  in  $z$ -plane can be conformally mapped, one-to-one, onto the unit disk in the  $w$ -plane.

- Isotherms map to isotherms and adiabats map to adiabats
- The boundary of  $R$  maps to the disk's circumference.
- The mapped temperature field still satisfies  $\nabla^2 \theta = 0$

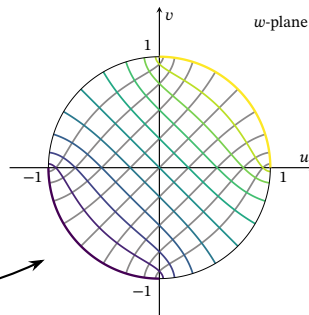
# Conformal mapping of square to disk

$\text{sn}(u|m)$  and  $\text{dn}(u|m)$  are complex-valued Jacobi elliptic functions (Schwarz, 1869)

$$w = f(z) = \sqrt{m} \frac{\text{sn}(z/\sqrt{m} | m)}{\text{dn}(z/\sqrt{m} | m)}, \quad \text{where } m = 1/2$$



$S = 1$



$S = 1$

$w = f(z)$

# Conformal maps

Analytic functions that map solutions of Laplace's equation from one shape to another in the complex plane

**Riemann mapping theorem:** Any simply-connected region  $R$  in  $z$ -plane can be conformally mapped, one-to-one, onto the unit disk in the  $w$ -plane.

- Isotherms map to isotherms and adiabats map to adiabats
- The boundary of  $R$  maps to the disk's circumference.
- The mapped temperature field still satisfies  $\nabla^2\theta = 0$

# Conformal maps

Analytic functions that map solutions of Laplace's equation from one shape to another in the complex plane

**Riemann mapping theorem:** Any simply-connected region  $R$  in  $z$ -plane can be conformally mapped, one-to-one, onto the unit disk in the  $w$ -plane.

- Isotherms map to isotherms and adiabats map to adiabats
- The boundary of  $R$  maps to the disk's circumference.
- The mapped temperature field still satisfies  $\nabla^2\theta = 0$
- At each point, the mapping: i) preserves angles (e.g., rotates axes); and ii) stretches the original coordinates by a scalar  $J$ .

# Conformal maps

Analytic functions that map solutions of Laplace's equation from one shape to another in the complex plane

**Riemann mapping theorem:** Any simply-connected region  $R$  in  $z$ -plane can be conformally mapped, one-to-one, onto the unit disk in the  $w$ -plane.

- Isotherms map to isotherms and adiabats map to adiabats
- The boundary of  $R$  maps to the disk's circumference.
- The mapped temperature field still satisfies  $\nabla^2 \theta = 0$
- At each point, the mapping: i) preserves angles (e.g., rotates axes); and ii) stretches the original coordinates by a scalar  $J$ .
- The mapping is unique to within an arbitrary rotation of the disk.

# Conformal maps

Analytic functions that map solutions of Laplace's equation from one shape to another in the complex plane

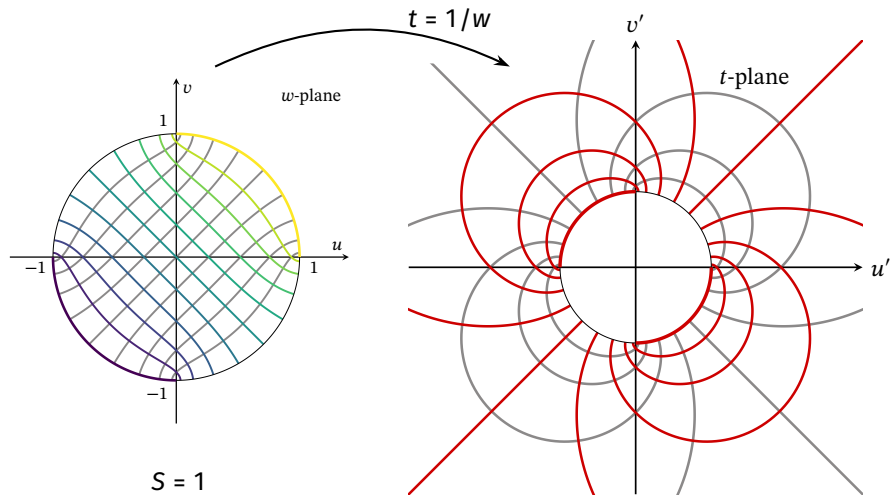
**Riemann mapping theorem:** Any simply-connected region  $R$  in  $z$ -plane can be conformally mapped, one-to-one, onto the unit disk in the  $w$ -plane.

- Isotherms map to isotherms and adiabats map to adiabats
- The boundary of  $R$  maps to the disk's circumference.
- The mapped temperature field still satisfies  $\nabla^2 \theta = 0$
- At each point, the mapping: i) preserves angles (e.g., rotates axes); and ii) stretches the original coordinates by a scalar  $J$ .
- The mapping is unique to within an arbitrary rotation of the disk.
- The region  $E$  exterior to  $R$  can also be mapped to the unit disk



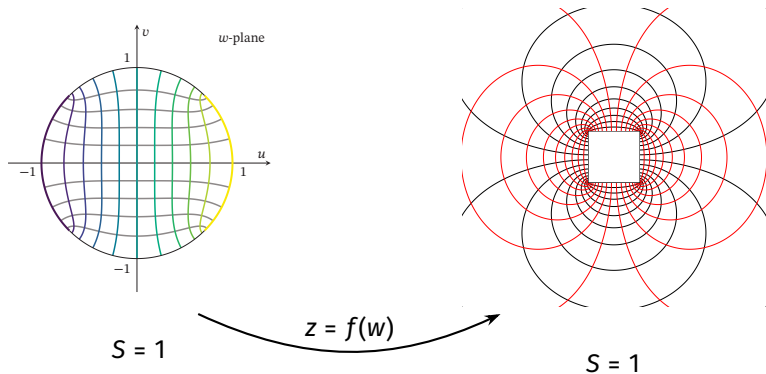
# Mapping of disk interior to disk exterior

Confirms what we'd already shown with Poisson integral formula



# Conformal map of disk interior to exterior of a square

We can map, one-to-one, the square's interior to the disk's interior to the square's exterior



$$z = f(w) = \int_{w_0}^w \frac{\sqrt{1-t^4}}{t^2} dt$$

Here  $|w| \leq 1$ , and  $|w_0| \rightarrow 0$  maps to the point at infinity in extended  $z$ -plane.

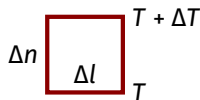
# Shape factors are invariant under conformal maps

At each point, the coordinates stretch by a factor  $J$

Two isotherms a distance  $\Delta n$  apart are at  $T$  and  $T + \Delta T$ .

The heat flow through a section of length  $\Delta l$  is:

$$\Delta \dot{Q} = k \frac{\Delta T}{\Delta n} \Delta l$$



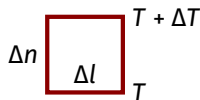
# Shape factors are invariant under conformal maps

At each point, the coordinates stretch by a factor  $J$

Two isotherms a distance  $\Delta n$  apart are at  $T$  and  $T + \Delta T$ .

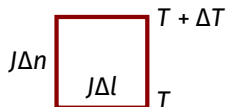
The heat flow through a section of length  $\Delta l$  is:

$$\Delta \dot{Q} = k \frac{\Delta T}{\Delta n} \Delta l$$



After mapping, the section has length  $J\Delta l$ . The isotherms have same temperatures but are a distance  $J\Delta n$  apart:

$$\Delta \dot{Q} = k \frac{\Delta T}{J\Delta n} (J\Delta l) = k \frac{\Delta T}{\Delta n} \Delta l$$



$\Delta \dot{Q}$  is the same.

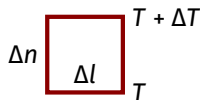
# Shape factors are invariant under conformal maps

At each point, the coordinates stretch by a factor  $J$

Two isotherms a distance  $\Delta n$  apart are at  $T$  and  $T + \Delta T$ .

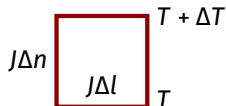
The heat flow through a section of length  $\Delta l$  is:

$$\Delta \dot{Q} = k \frac{\Delta T}{\Delta n} \Delta l$$



After mapping, the section has length  $J\Delta l$ . The isotherms have same temperatures but are a distance  $J\Delta n$  apart:

$$\Delta \dot{Q} = k \frac{\Delta T}{J\Delta n} (J\Delta l) = k \frac{\Delta T}{\Delta n} \Delta l$$



$\Delta \dot{Q}$  is the same. Summing over all sections on the unmapped or mapped boundaries (i.e., integrating), gives the same total heat flow,  $\dot{Q}$ , for each.

**Thus,  $S$  is the same before and after conformal mapping.**

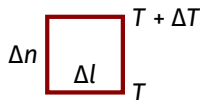
# Shape factors are invariant under conformal maps

At each point, the coordinates stretch by a factor  $J$

Two isotherms a distance  $\Delta n$  apart are at  $T$  and  $T + \Delta T$ .

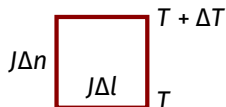
The heat flow through a section of length  $\Delta l$  is:

$$\Delta \dot{Q} = k \frac{\Delta T}{\Delta n} \Delta l$$



After mapping, the section has length  $J\Delta l$ . The isotherms have same temperatures but are a distance  $J\Delta n$  apart:

$$\Delta \dot{Q} = k \frac{\Delta T}{J\Delta n} (J\Delta l) = k \frac{\Delta T}{\Delta n} \Delta l$$



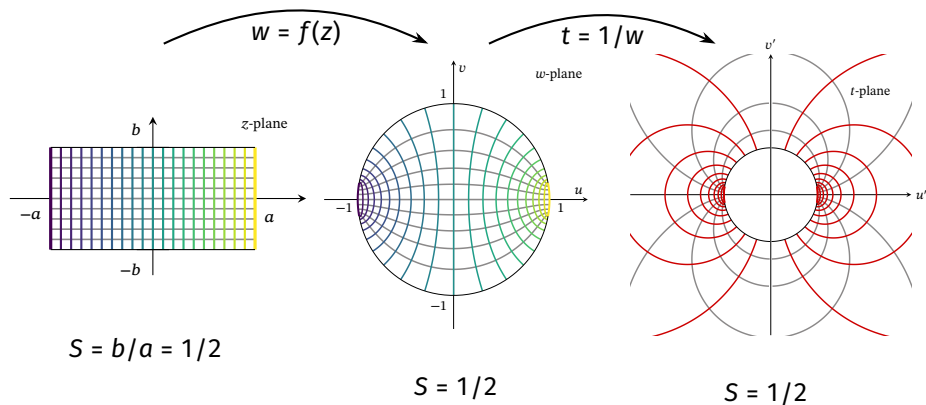
$\Delta \dot{Q}$  is the same. Summing over all sections on the unmapped or mapped boundaries (i.e., integrating), gives the same total heat flow,  $\dot{Q}$ , for each.

**Thus,  $S$  is the same before and after conformal mapping.**

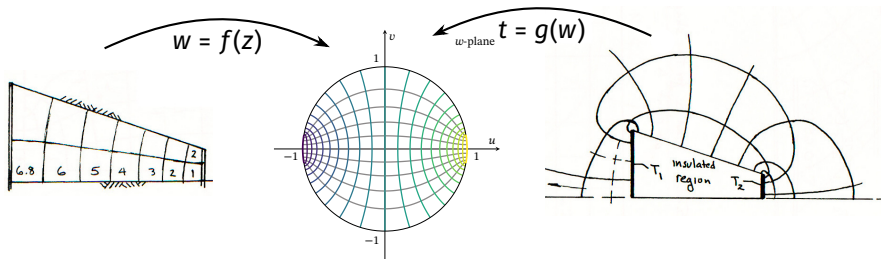
With more math, we can prove: 
$$\int_{\sigma_z} \vec{n} \cdot \nabla_z T dl_z = \int_{\sigma_w} \vec{n} \cdot \nabla_w T dl_w$$

# Conformal mapping of rectangle to disk ( $a : b = 2 : 1$ )

$$w = f(z) = \frac{\operatorname{sn}(\lambda z | m) \operatorname{dn}(\lambda z | m)}{\operatorname{cn}(\lambda z | m)} \quad \text{for } \lambda = K/2a \text{ with } K(m) \text{ the real quarter period}$$



# What we have learned from conformal mapping

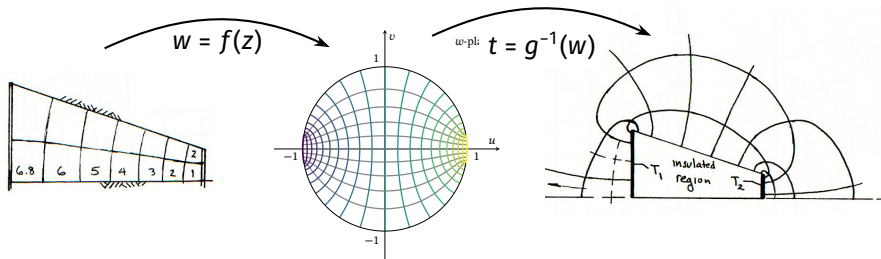


Riemann: the inside and outside can be mapped to the unit disk.

*Disk in center is only schematic, not computed.*



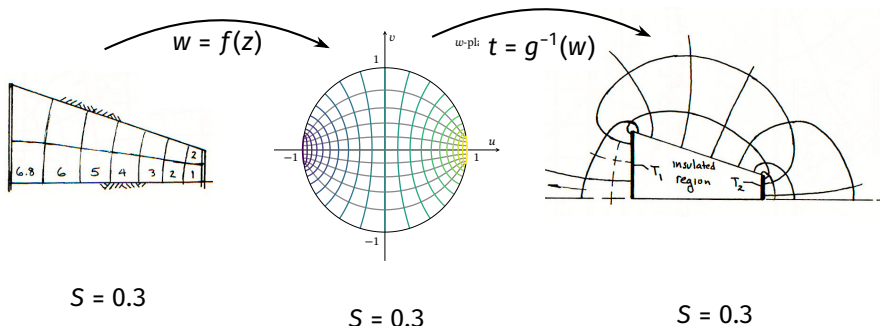
# What we have learned from conformal mapping



These mappings are 1-1 and so have inverse mappings.

*Disk in center is only schematic, not computed.*

# What we have learned from conformal mapping



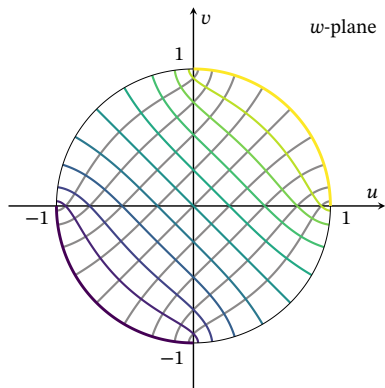
The shape factors are the same before and after mappings.

**Therefore, the interior and exterior shape factors are equal.**

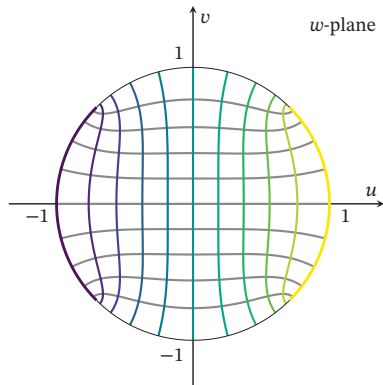
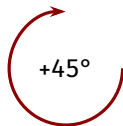
*Disk in center is only schematic, not computed.*

# Shape factors are invariant under rotation of b.c.s

The disk is conformally mapped to the square by:  $z = \int_0^w \frac{ds}{\sqrt{1-s^4}}$



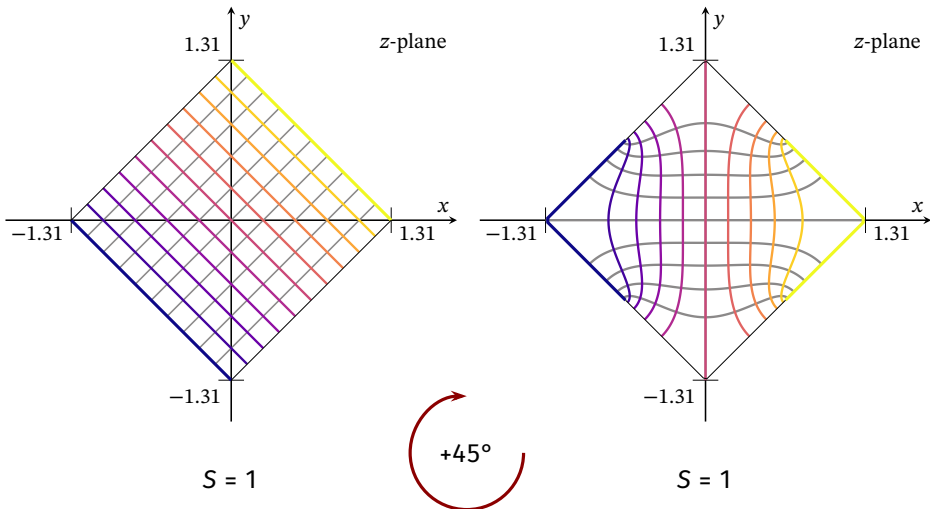
$S = 1$



$S = 1$

# Shape factors are invariant under rotation of b.c.s

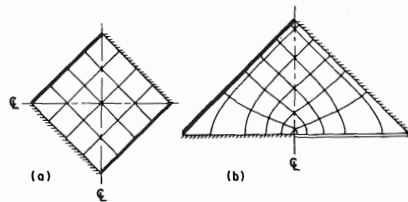
Yin-Yang bodies are equivalent through rotation of a  $90^\circ$  unit disk prior to mapping



# Shape factors for “Yin-Yang” bodies are $S = 1$

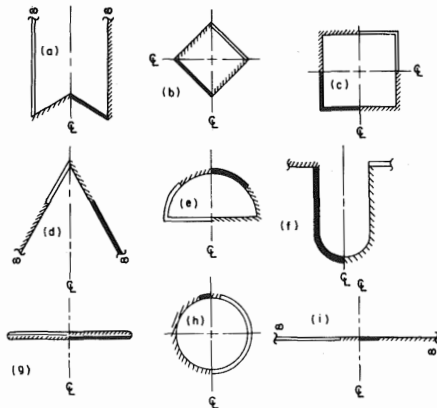
Isothermal and adiabatic edges are interchanged across an axis of symmetry

J.H. Lienhard (IV), 1981, *J. Heat Transfer*, **103**(3):600–1



— boundary at  $T_1$   
 — boundary at  $T_2$   
 - - - boundary insulated  
 — adiabatic and isothermal lines

Fig. 1 Two Yin-Yang figures

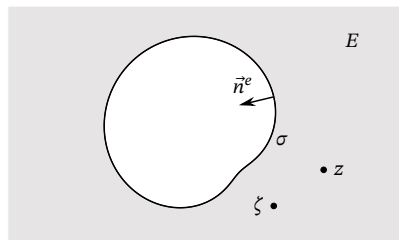
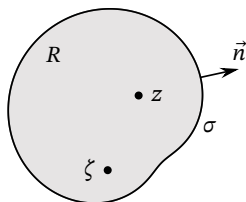


— boundary at  $T_1$   
 — boundary at  $T_2$   
 - - - boundary insulated

Fig. 2 Nine more Yin-Yang figures

# Green's functions an arbitrary 2D exterior region

See paper for details!!



$$\theta(z) = - \int_{\sigma} \frac{\partial g(z|\zeta)}{\partial n_{\zeta}} h(\zeta) dl_{\zeta} \equiv \int_{\sigma} l(z|\zeta) h(\zeta) dl_{\zeta}$$

The boundary influence function,  $l(z|\zeta)$ , is the temperature at  $z$  produced by a delta-function boundary temperature at  $\zeta$  (a unit-strength point source).

If  $f(z, \zeta)$  takes  $z \in R$  to the unit disk and the point  $\zeta \in R$  to  $w = 0$ :

$$g(z|\zeta) = -\frac{1}{2\pi} \log |f(z, \zeta)|$$

# Summary

Interior shape factors in two-dimensions are the same as exterior shape factors

- 1 *Shape factors for conduction inside an object are equal to those for conduction through the material outside the object,*
  - a if the only heat sources and sinks are the isothermal boundary sections
  - b no net heat transfer to the exterior region far away
  - c interior and exterior conductivities must be uniform, but not equal

# Summary

Interior shape factors in two-dimensions are the same as exterior shape factors

- 1 *Shape factors for conduction inside an object are equal to those for conduction through the material outside the object,*
  - a if the only heat sources and sinks are the isothermal boundary sections
  - b no net heat transfer to the exterior region far away
  - c interior and exterior conductivities must be uniform, but not equal
- 2 This principle is established:
  - a For the unit disk using the Poisson integral formula
  - b For arbitrary shapes by conformally mapping to and from the unit disk
  - c And for arbitrary shapes using Green's functions (see paper for details)



# Summary

Interior shape factors in two-dimensions are the same as exterior shape factors

- 1 *Shape factors for conduction inside an object are equal to those for conduction through the material outside the object,*
  - a if the only heat sources and sinks are the isothermal boundary sections
  - b no net heat transfer to the exterior region far away
  - c interior and exterior conductivities must be uniform, but not equal
- 2 This principle is established:
  - a For the unit disk using the Poisson integral formula
  - b For arbitrary shapes by conformally mapping to and from the unit disk
  - c And for arbitrary shapes using Green's functions (see paper for details)
- 3 A simple geometrical proof shows that shape factors are invariant under conformal mapping (a mathy proof is in the paper)

# Summary

Interior shape factors in two-dimensions are the same as exterior shape factors

- 1 *Shape factors for conduction inside an object are equal to those for conduction through the material outside the object,*
  - a if the only heat sources and sinks are the isothermal boundary sections
  - b no net heat transfer to the exterior region far away
  - c interior and exterior conductivities must be uniform, but not equal
- 2 This principle is established:
  - a For the unit disk using the Poisson integral formula
  - b For arbitrary shapes by conformally mapping to and from the unit disk
  - c And for arbitrary shapes using Green's functions (see paper for details)
- 3 A simple geometrical proof shows that shape factors are invariant under conformal mapping (a mathy proof is in the paper)
- 4 The “Yin-Yang” shape factors with  $S = 1$ , described in 1981, have been explained as rotations of the unit disk prior to mapping.

# Thank you!

To read more, see this paper:

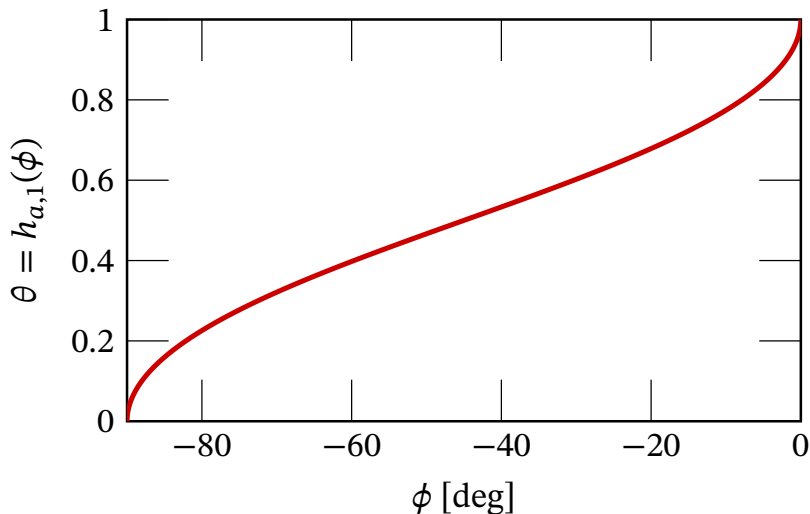
J. H. Lienhard V, “Exterior shape factors from interior shape factors,” *J. Heat Transfer*, **141**(6):061301, June 2019.

OPEN ACCESS: <https://doi.org/10.1115/1.4042912>



# Supplementary slides

## Temperature distribution on 90° adiabatic edge of disk



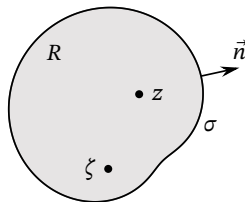
# Green's functions for an arbitrary 2D region, $R$

The Green's function  $g(z|\zeta)$  is the solution of:

$$-\nabla^2 g = \delta(\zeta - z)$$

$z$  and  $\zeta$  in  $R$

$g = 0$  for  $\zeta$  on  $\sigma$



Green's second identity

$$\int_R [g \nabla^2 \theta - \theta \nabla^2 g] dR_\zeta = \int_\sigma \left[ g \frac{\partial \theta}{\partial n_\zeta} - \theta \frac{\partial g}{\partial n_\zeta} \right] dl_\zeta$$

where subscript  $\zeta$  means differentiation/integration w.r.t.  $\zeta$ .

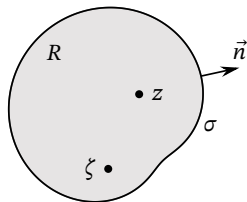
## Green's functions for an arbitrary 2D region, $R$

The Green's function  $g(z|\zeta)$  is the solution of:

$$-\nabla^2 g = \delta(\zeta - z)$$

$z$  and  $\zeta$  in  $R$

$g = 0$  for  $\zeta$  on  $\sigma$



Green's second identity

$$\int_R [g \nabla^2 \theta - \theta \nabla^2 g] dR_\zeta = \int_\sigma \left[ g \frac{\partial \theta}{\partial n_\zeta} - \theta \frac{\partial g}{\partial n_\zeta} \right] dl_\zeta$$

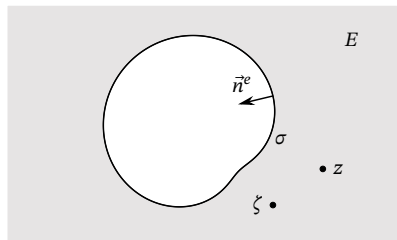
where subscript  $\zeta$  means differentiation/integration w.r.t.  $\zeta$ . Then:

$$\theta(z) = - \int_\sigma \frac{\partial g(z|\zeta)}{\partial n_\zeta} h(\zeta) dl_\zeta \equiv \int_\sigma I(z|\zeta) h(\zeta) dl_\zeta$$

The boundary influence function,  $I(z|\zeta)$ , is the temperature at  $z$  produced by a delta-function boundary temperature at  $\zeta$  (a unit-strength point source).

## Green's functions an arbitrary 2D exterior region, $E$

For the exterior region  $E$ , the outward normal direction,  $\vec{n}^e$ , is opposite  $\vec{n}$ . The rest is the same. (We also require  $g^e(z, \zeta)$  to give bounded solution for  $\theta^e$  as  $|z| \rightarrow \infty$ .)



$$\theta^e(z) = - \int_{\sigma} \frac{\partial g^e(z|\zeta)}{\partial n_{\zeta}^e} h(\zeta) dl_{\zeta} = \int_{\sigma} \frac{\partial g^e(z|\zeta)}{\partial n_{\zeta}} h(\zeta) dl_{\zeta}$$

Since the only temperature sources are on the boundary  $\sigma$ , the exterior solution is also given by the boundary influence function, respecting the change in normal direction:

$$\theta^e(z) = - \int_{\sigma} l(z|\zeta) h(\zeta) dl_{\zeta}$$



## Interior and exterior shape factors of $R$ are equal

Let the boundary  $\sigma$  be a chain four curves:  $\sigma_1$  isothermal at  $\theta = 0$ ;  $\sigma_2$  and  $\sigma_4$  adiabatic; and  **$\sigma_3$  isothermal at  $\theta = 1$** .

The shape factor for the interior is:

$$S^i = \int_{\sigma_3} \frac{\partial \theta}{\partial n_z} dl_z = - \int_{\sigma_3} \frac{\partial}{\partial n_z} \int_{\sigma} \frac{\partial g(z|\zeta)}{\partial n_{\zeta}} h(\zeta) dl_{\zeta} dl_z = + \int_{\sigma_3} \frac{\partial}{\partial n_z} \int_{\sigma} l(z|\zeta) h(\zeta) dl_{\zeta} dl_z$$

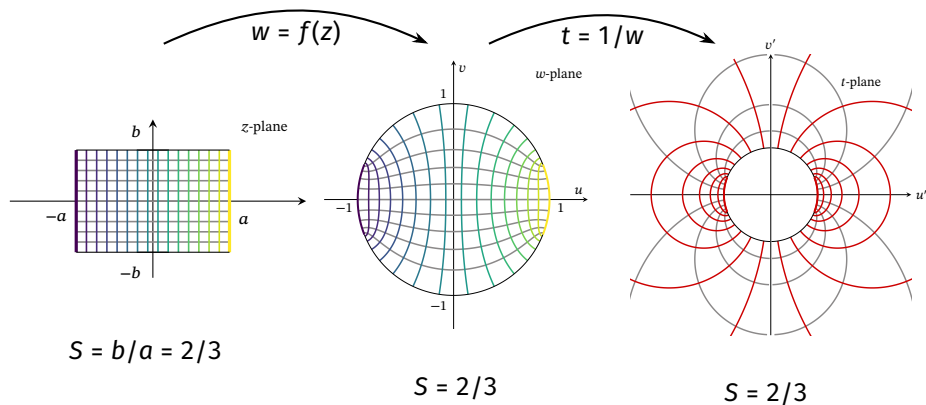
For the exterior, the normal direction is reversed

$$S^e = \int_{\sigma_3} \frac{\partial \theta^e}{\partial n_z^e} dl_z = - \int_{\sigma_3} \frac{\partial}{\partial n_z^e} \int_{\sigma} l(z|\zeta) h(\zeta) dl_{\zeta} dl_z = + \int_{\sigma_3} \frac{\partial}{\partial n_z} \int_{\sigma} l(z|\zeta) h(\zeta) dl_{\zeta} dl_z$$

Comparing eqn. (5) to eqn. (5), we see again that  **$S^e = S^i$** .

# Conformal mapping of rectangle to disk ( $a : b = 3 : 2$ )

$$w = f(z) = \frac{\operatorname{sn}(\lambda z | m) \operatorname{dn}(\lambda z | m)}{\operatorname{cn}(\lambda z | m)} \quad \text{for } \lambda = K/2a \text{ with } K(m) \text{ the real quarter period}$$



# Line integral of a normal derivative

The integral defining the shape factor is unchanged by a conformal map

Consider an integral in the mapped  $w$ -plane

$$\int_{\sigma} \frac{\partial T}{\partial n} dl = \int_{\sigma} \vec{n} \cdot \nabla T dl = \int_{\sigma} \nabla^{\perp} T \cdot d\vec{w}$$

in which the skew gradient is

$$\nabla^{\perp} T \equiv \begin{pmatrix} \partial T / \partial v \\ -\partial T / \partial u \end{pmatrix}$$

The transformation of  $d\vec{w}$  to the  $z$ -plane is

$$d\vec{w} = \begin{pmatrix} du \\ dv \end{pmatrix} = \underbrace{\begin{pmatrix} \partial u / \partial x & \partial u / \partial y \\ \partial v / \partial x & \partial v / \partial y \end{pmatrix}}_{=J_1} \begin{pmatrix} dx \\ dy \end{pmatrix} \quad (1)$$

With the Cauchy-Riemann conditions,

$$|J_1| = (\partial u / \partial x)^2 + (\partial u / \partial y)^2$$

$$J_1 = |J_1| \begin{pmatrix} \alpha & \beta \\ -\beta & \alpha \end{pmatrix}$$

where  $\alpha^2 + \beta^2 = 1$ .  $|J_1|$  is:

$$\left| \frac{\partial u}{\partial z} \right|^2 = \frac{\partial u}{\partial z} \overline{\frac{\partial u}{\partial z}} = \left( \frac{\partial u}{\partial x} \right)^2 + \left( \frac{\partial u}{\partial y} \right)^2$$

Similarly,

$$\begin{aligned} \nabla^{\perp} T &= \begin{pmatrix} \partial T / \partial v \\ -\partial T / \partial u \end{pmatrix} \\ &= \underbrace{\begin{pmatrix} \partial y / \partial v & -\partial x / \partial v \\ -\partial y / \partial u & \partial x / \partial u \end{pmatrix}}_{=J_2} \begin{pmatrix} \partial T / \partial y \\ -\partial T / \partial x \end{pmatrix} \quad (2) \\ &= |J_2| \begin{pmatrix} \alpha & \beta \\ -\beta & \alpha \end{pmatrix} \begin{pmatrix} \partial T / \partial y \\ -\partial T / \partial x \end{pmatrix} \end{aligned}$$

## Line integral of $\vec{n} \cdot \nabla T$ is unchanged by conformal mapping

$|J_2| = (\partial x / \partial u)^2 + (\partial y / \partial u)^2$  and

$$\left| \frac{\partial \vec{z}}{\partial u} \right|^2 = \frac{\partial \vec{z}}{\partial u} \frac{\partial \bar{\vec{z}}}{\partial u} = \left( \frac{\partial x}{\partial u} \right)^2 + \left( \frac{\partial y}{\partial u} \right)^2$$

Thus,  $|J_1| |J_2| = |\partial u / \partial \vec{z}|^2 |\partial \vec{z} / \partial u|^2 = 1$ .

For vectors  $\vec{a}$  and  $\vec{b}$  and matrices  $\mathbf{A}$  and  $\mathbf{B}$ ,

$$\begin{aligned} (\mathbf{A}\vec{a}) \cdot (\mathbf{B}\vec{b}) &= (\mathbf{A}\vec{a})^T (\mathbf{B}\vec{b}) \\ &= \vec{a}^T \mathbf{A}^T (\mathbf{B}\vec{b}) = \vec{a}^T (\mathbf{A}^T \mathbf{B}) \vec{b} \end{aligned}$$

Then, using eqns. (1) and (2),

$$\nabla^\perp T \cdot d\vec{w} = \begin{pmatrix} \partial T / \partial y \\ -\partial T / \partial x \end{pmatrix}^T J_2^T J_1 \begin{pmatrix} dx \\ dy \end{pmatrix}$$

Multiplication of the Jacobian matrices produces a considerable simplification:

$$\begin{aligned} J_2^T J_1 &= |J_2| |J_1| \begin{pmatrix} \alpha & -\beta \\ \beta & \alpha \end{pmatrix} \begin{pmatrix} \alpha & \beta \\ -\beta & \alpha \end{pmatrix} \\ &= |J_1| |J_2| \begin{pmatrix} \alpha^2 + \beta^2 & 0 \\ 0 & \alpha^2 + \beta^2 \end{pmatrix} \\ &= |J_1| |J_2| \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix} \\ &= \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix} \end{aligned}$$

Putting these pieces together, denoting the  $w$  and  $z$  planes by subscripts, we find that:

$$\int_{\sigma_w} \vec{n} \cdot \nabla_w T dl_w = \int_{\sigma_w} \nabla_w^\perp T \cdot d\vec{w} = \int_{\sigma_z} \nabla_z^\perp T \cdot d\vec{z} = \int_{\sigma_z} \vec{n} \cdot \nabla_z T dl_z$$

# Riemann mapping theorem in full

**Riemann mapping theorem:** for a plane simply-connected region  $R$  with boundary  $\sigma$  containing an interior point  $\zeta$ , there exists a function  $w = f(z, \zeta)$ , analytic on  $R$ , that conformally maps  $R$  one-to-one onto the unit disk in the  $w$ -plane, taking  $\sigma$  to the disk's circumference and  $\zeta$  to  $w = 0$ . When  $\zeta = 0$ , we will simply write  $w = f(z)$ . The mapping is unique to within an arbitrary rotation of the disk.