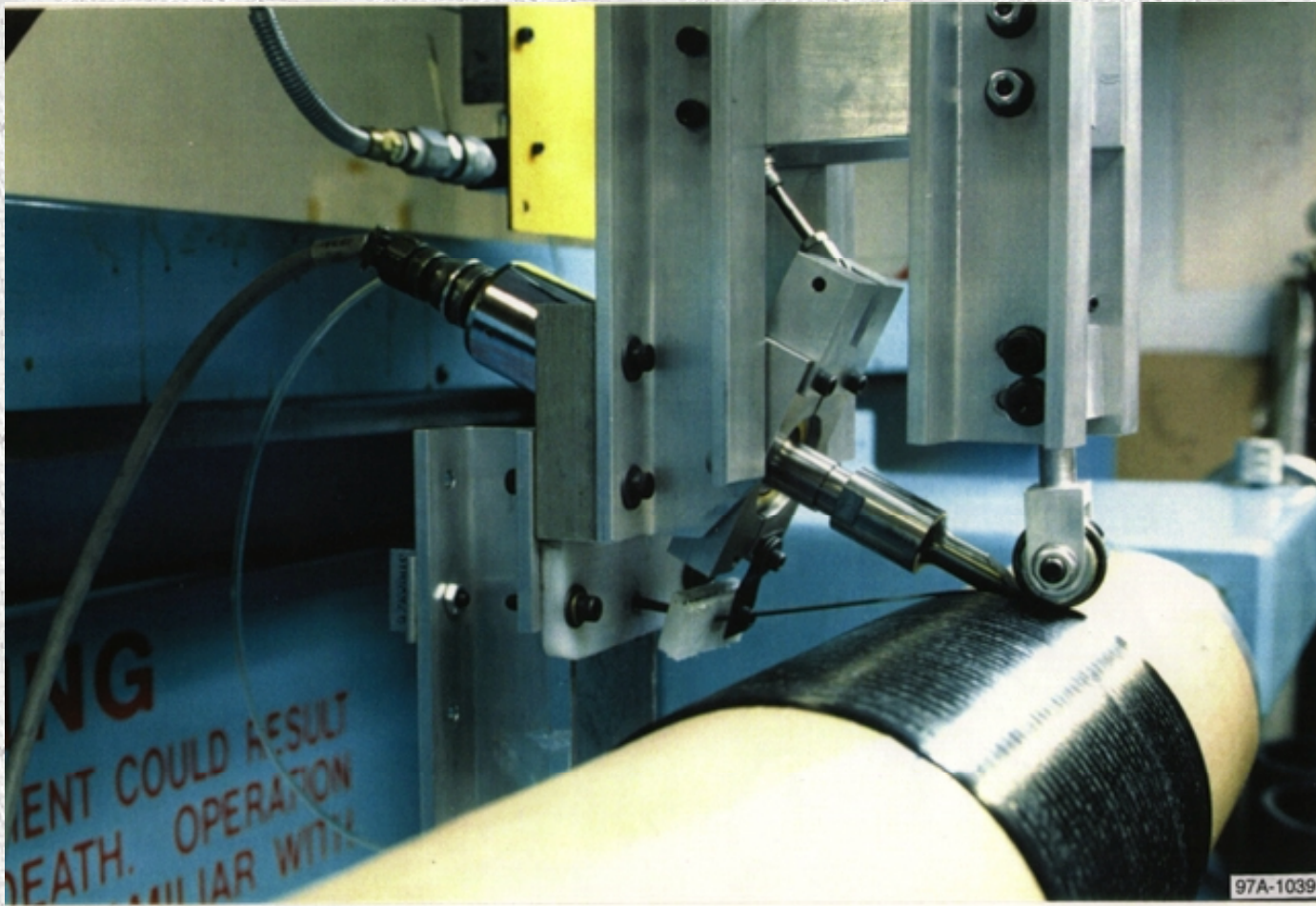


Ultrasonic Tape Lamination (UTL) Consolidation and Out-of-Autoclave Curing of Thick Composite Structures

J. Player, W. Zukas and M. Roylance,
Foster-Miller, Inc.

D. Roylance, MIT

Ultrasonic Consolidation



Process Model

- Ultrasonic heating

$$\frac{dT}{dt} = \frac{Q}{\rho c}, \quad Q = f \cdot \pi E'' \varepsilon_0^2 + R_r \Delta H_r$$

- Dynamic modulus

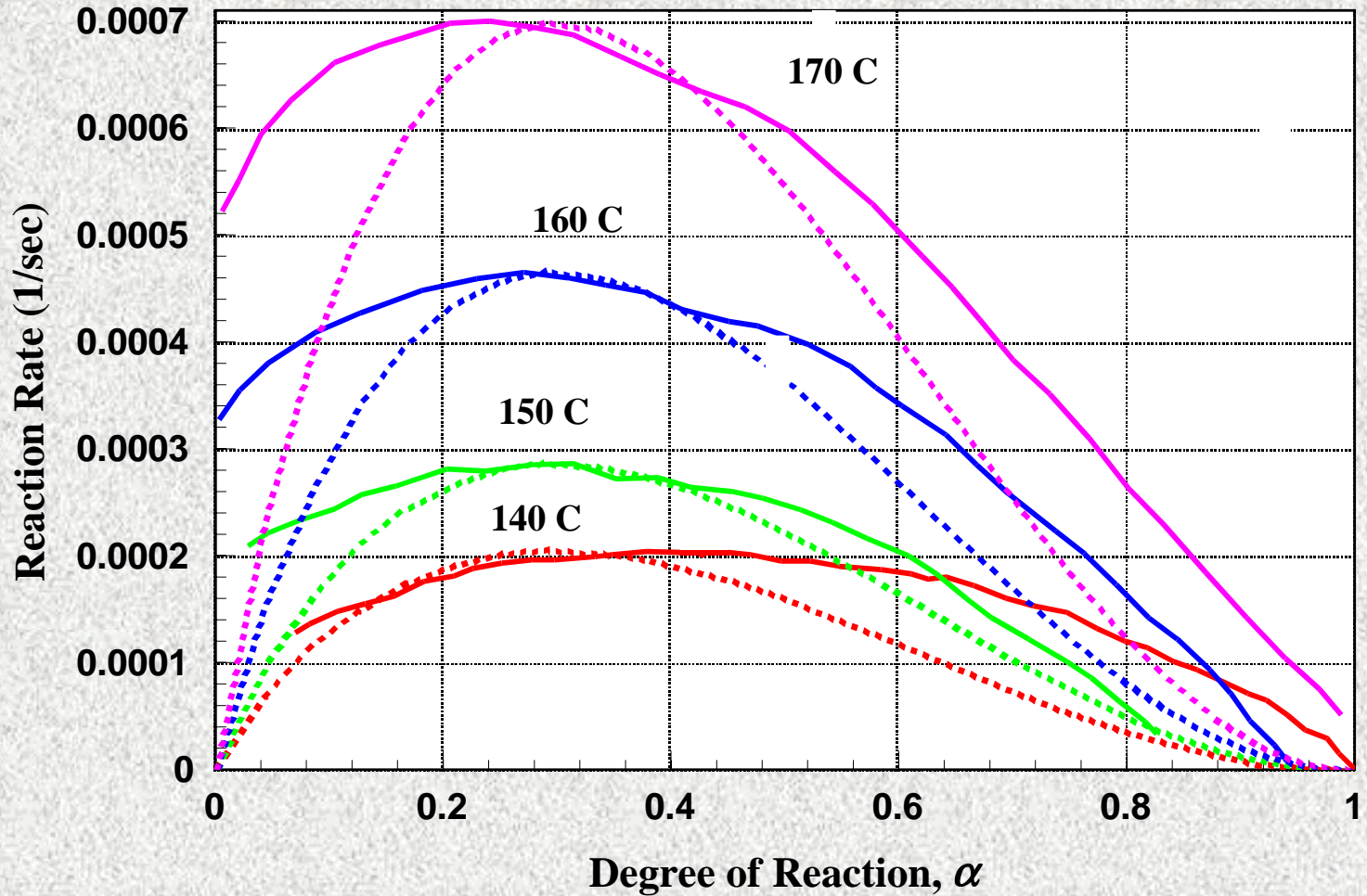
$$E' = k_0 + \sum_{j=1}^N \frac{k_j (\omega \tau_j)^2}{1 + (\omega \tau_j)^2}, \quad E'' = \sum_{j=1}^N \frac{k_j (\omega \tau_j)}{1 + (\omega \tau_j)^2}$$

$$\tau_j = \tau_{0j} \exp\left(\frac{E^{\tau}}{R_g T}\right)$$

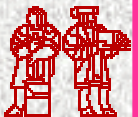
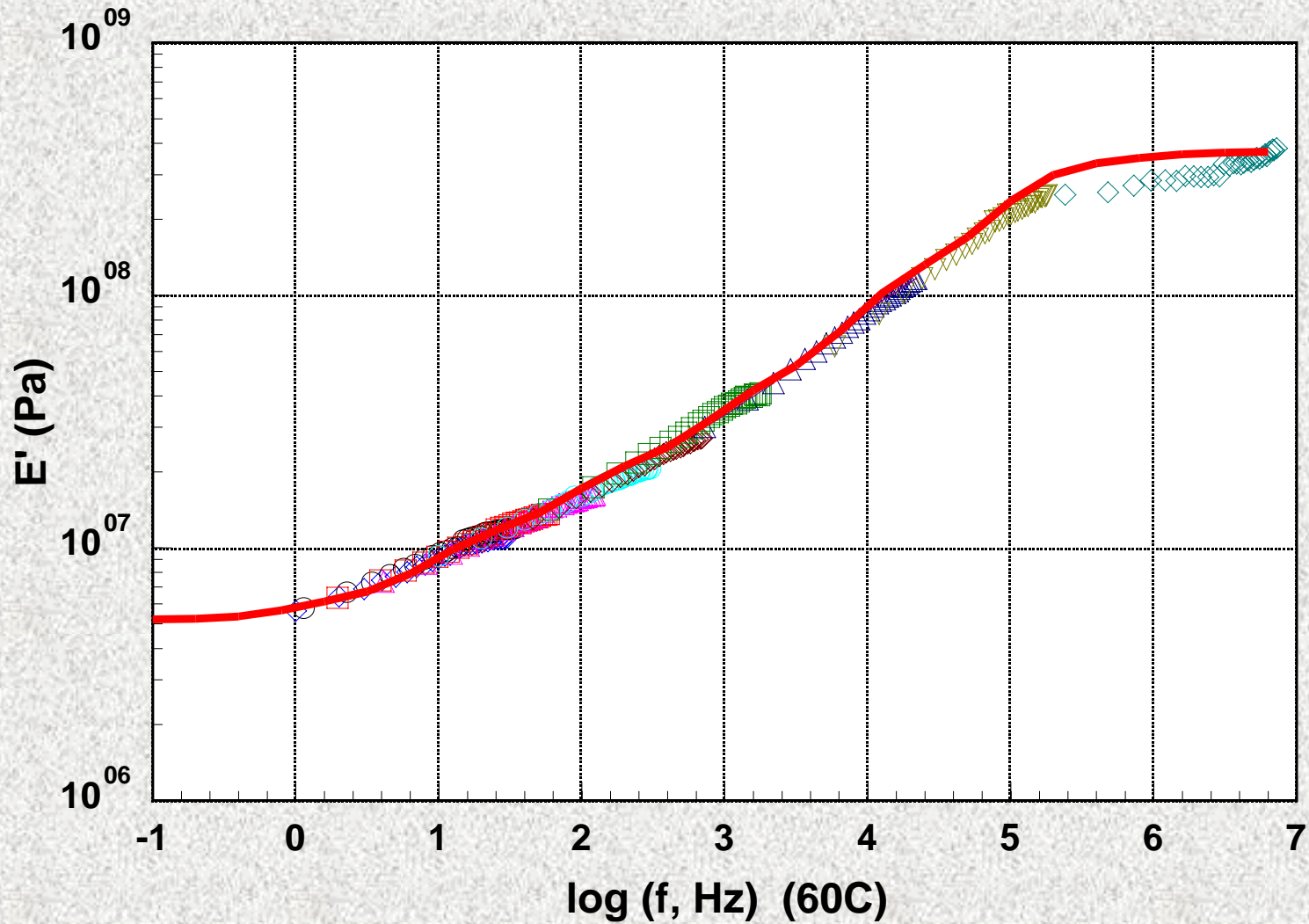
- Curing reaction

$$\frac{d\alpha}{dt} = k_0 \exp\left(\frac{-E^r}{R_g T}\right) \cdot \alpha^{m1} (1 - \alpha)^{m2}$$

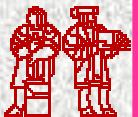
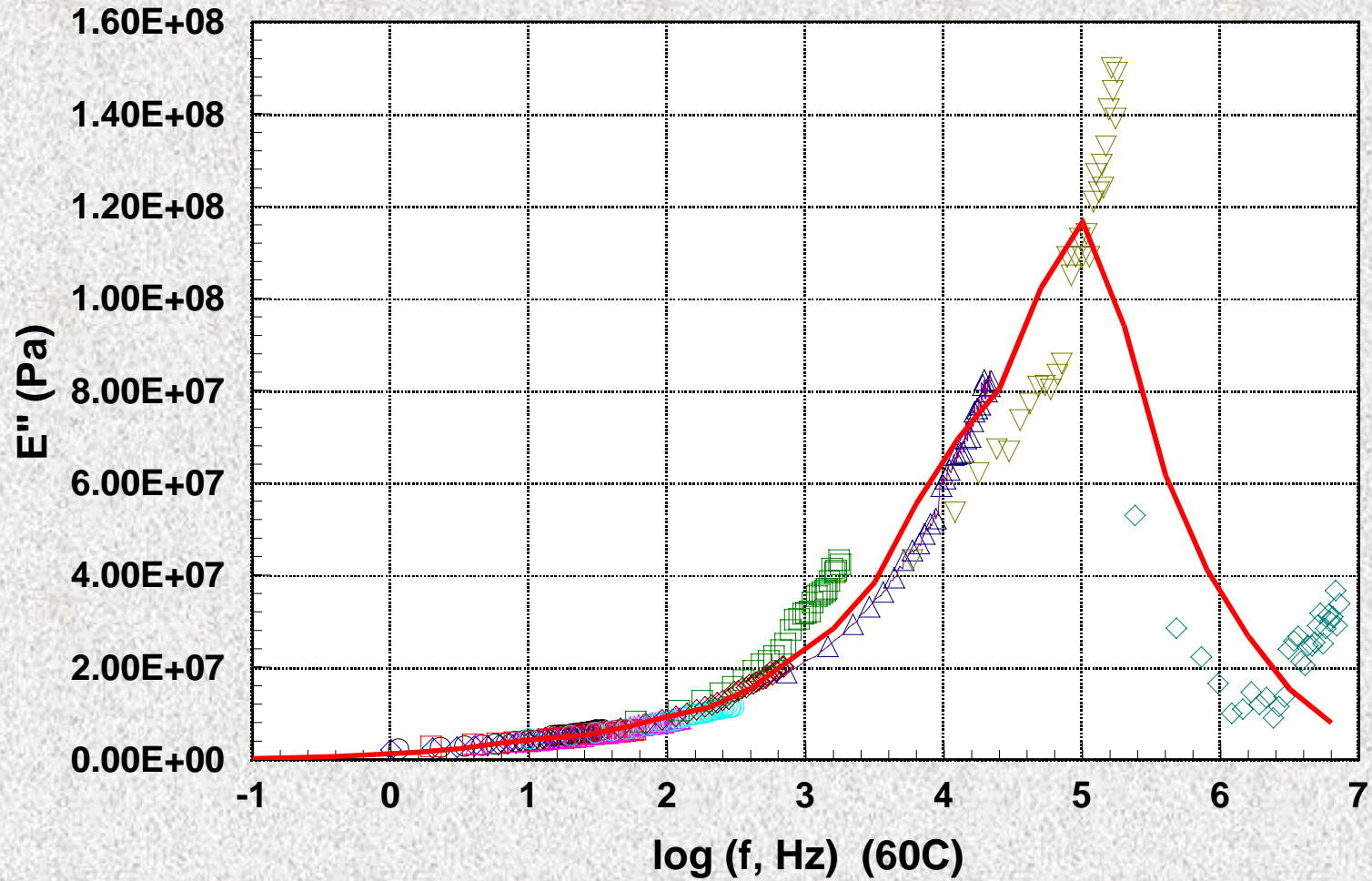
DSC Cure Scans and Model Fit



E' Master Curve and Model Fit



E'' Master Curve and Model Fit



Spreadsheet Model

Microsoft Excel - kinetic model (zukas).xls

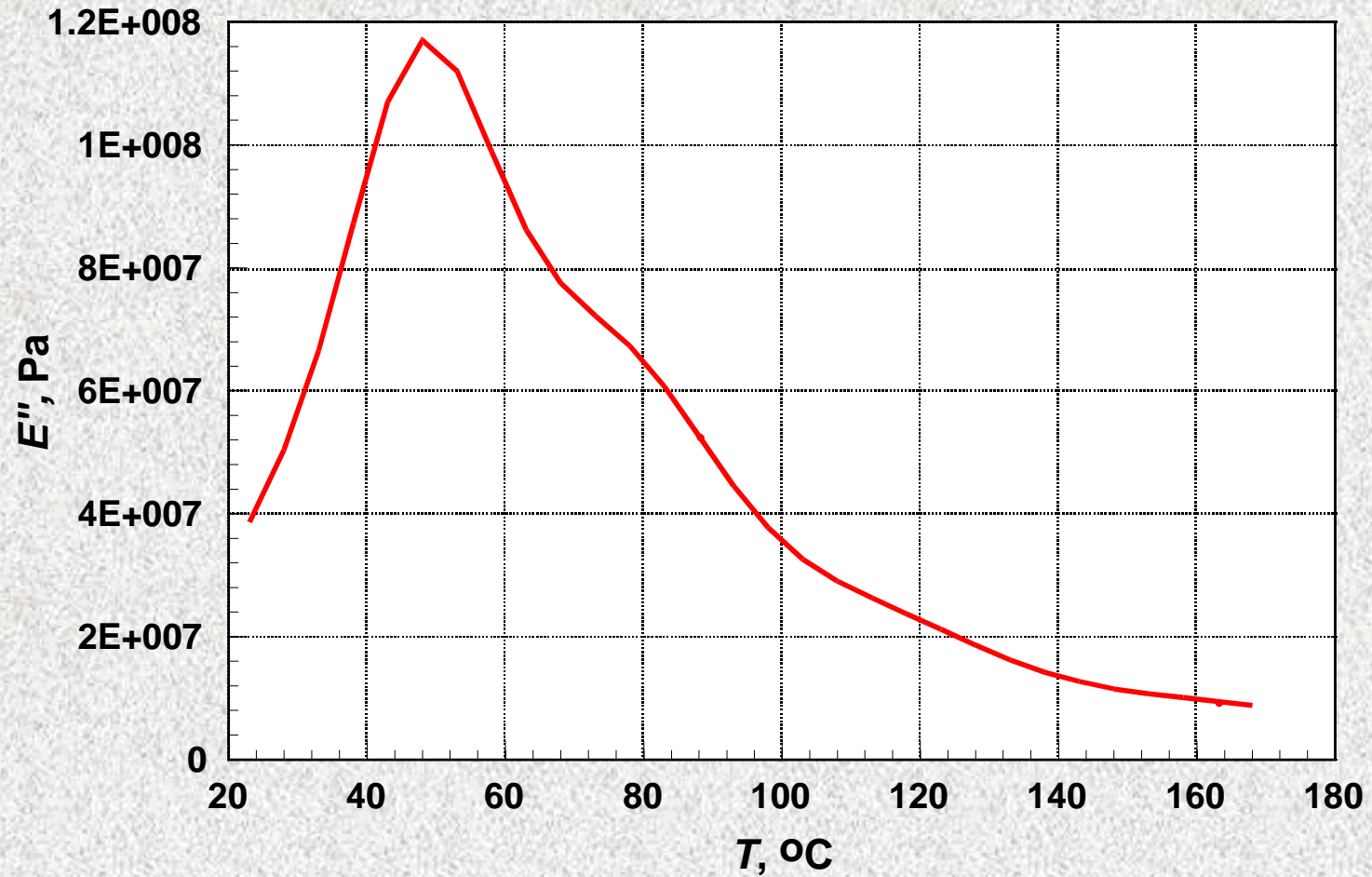
File Edit View Insert Format Tools Data Window Help

o13 = =k_4*Dp*t_4*EXP(Ev*120.3/(273+\$B13))/(1+(Dp*t_4*EXP(Ev*120.3/(273+\$B13)))^2)

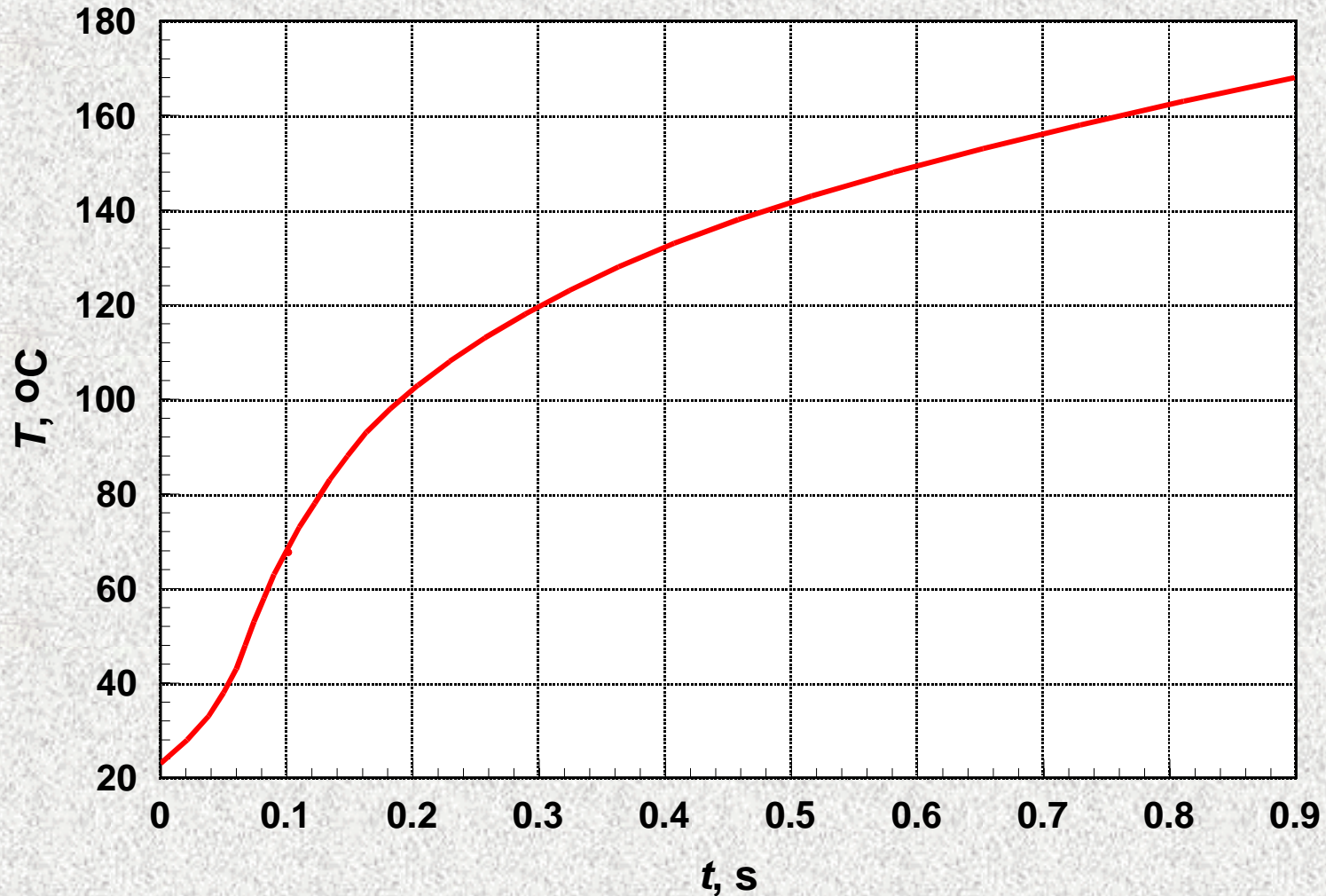
	A	B	C	D	E	F	G	H	I	J	
1	Ultrasonic cure, simple model, 8552 resin										
2	Dissipation from Zukas data, SLS model										
3	no spatial variation, heating from viscous dissipation and reaction										
4	exotherm, less convective cooling										
5											
6		Z(1/s)=	1.27E+05	E(J/mol)=	6.34E+04	n=	0.9				
7		T_a(C) =	100	H_r(J/g)=	483			G0(Pa)=	1.18E+08		
8		depth(mm)=	0.360	ampl(mm)=	0.005	f(Hz)=	4.00E+04	tau0(s)=	9.09E-16		
9		c(J/kg-K)=	2000	rho(kg/m^3)=	2000	w(rad/s)=	6.37E+03	Ev(kJ/mol)=	69.1		
10		h(J/m^2-K)=		E"(N/m^2)=	7.00E+04	strain=	0.014				
11											
12	t (s)	T (C)	α	alpha_dot	tau (s)	E" (Pa)	q_d (W/m³)	q_r (W/m³)	h (W/m²)	T_dot (C)	
13	0.000	23	0.010000	1.30E-08	1.42E-03	3.86E+07	9.37E+08	1.26E+01	0.00E+00	2.34E+02	
14	0.021	28	0.010000	2.00E-08	8.92E-04	5.04E+07	1.22E+09	1.93E+01	0.00E+00	3.05E+02	
15	0.038	33	0.010000	3.02E-08	5.68E-04	6.65E+07	1.61E+09	2.92E+01	0.00E+00	4.03E+02	
16	0.050	38	0.010000	4.51E-08	3.67E-04	8.72E+07	2.11E+09	4.36E+01	0.00E+00	5.28E+02	
17	0.060	43	0.010000	6.65E-08	2.41E-04	1.07E+08	2.60E+09	6.42E+01	0.00E+00	6.49E+02	

Sheet1 Sheet2 Sheet3

Temperature Dependence of E'' at 40MHz



Carbon/8552 composite, $\epsilon_0 = 1.4\%$, $f = 40$ kHz.



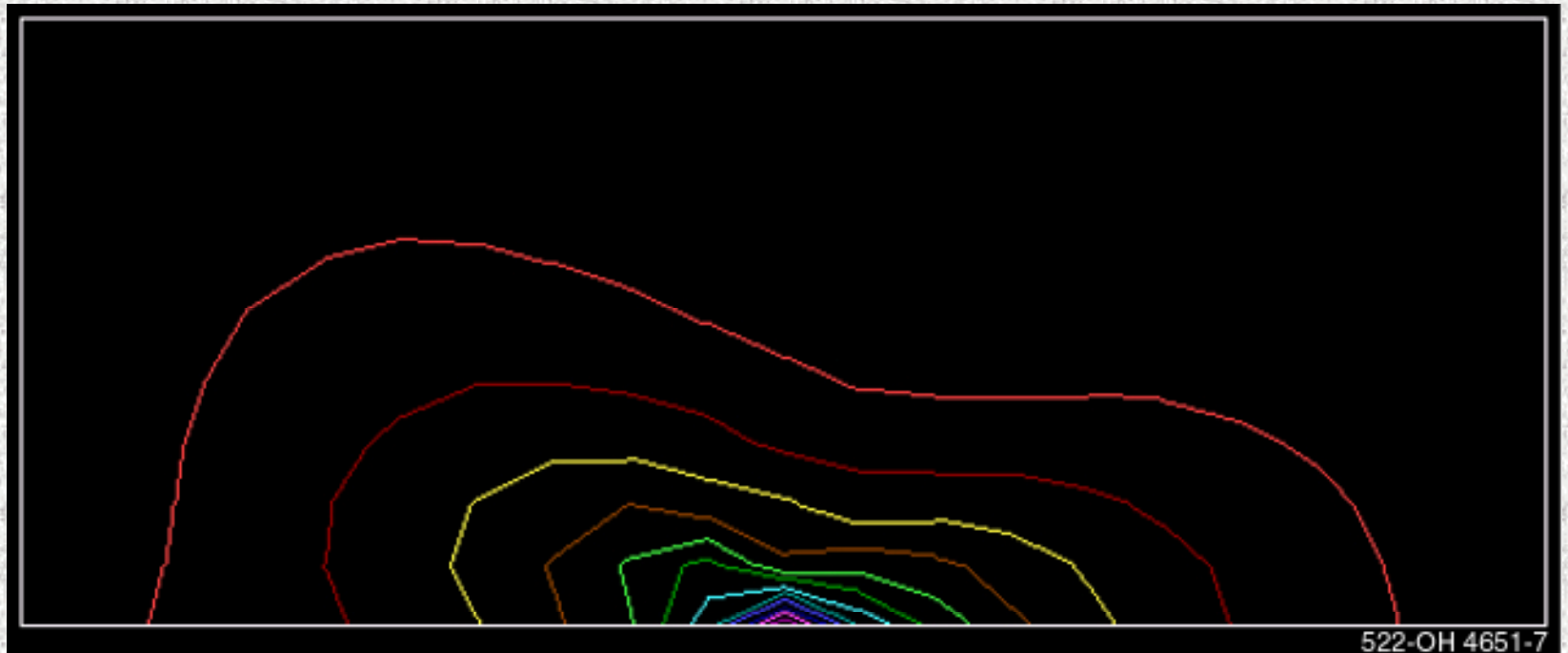
Finite Element Analysis (FEA)

$$\rho \left[\frac{\partial u}{\partial t} + u \nabla u \right] = -\nabla p + \nabla (\eta \nabla u)$$

$$\rho c \left[\frac{\partial T}{\partial t} + u \nabla T \right] = Q + \nabla (k \nabla T)$$

$$\left[\frac{\partial C}{\partial t} + u \nabla C \right] = R + \nabla (D \nabla C)$$

FEA - Displacement (u_x) Contours



FEA - Temperature Contours

